

Heat Transfer in Engine

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Engine Heat Transfer

1. Impact of heat transfer on engine operation
2. Heat transfer environment
3. Energy flow in an engine
4. Engine heat transfer
 - Fundamentals
 - Spark-ignition engine heat transfer
 - Diesel engine heat transfer
5. Component temperature and heat flow

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Engine Heat Transfer

- Heat transfer is a parasitic process that contributes to a loss in fuel conversion efficiency
- The process is a “surface” effect
- Relative importance reduces with:
 - Larger engine displacement
 - Higher load

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Engine Heat Transfer: Impact

- **Efficiency and Power:** Heat transfer in the inlet decrease volumetric efficiency. In the cylinder, heat losses to the wall is a loss of availability.
- **Exhaust temperature:** Heat losses to exhaust influence the turbocharger performance. In- cylinder and exhaust system heat transfer has impact on catalyst light up.
- **Friction:** Heat transfer governs liner, piston/ ring, and oil temperatures. It also affects piston and bore distortion. All of these effects influence friction. Thermal loading determined fan, oil and water cooler capacities and pumping power.
- **Component design:** The operating temperatures of critical engine components affects their durability; e.g. via mechanical stress, lubricant behavior

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Engine Heat Transfer: Impact

- **Mixture preparation in SI engines:** Heat transfer to the fuel significantly affect fuel evaporation and cold start calibration
- **Cold start of diesel engines:** The compression ratio of diesel engines are often governed by cold start requirement
- **SI engine octane requirement:** Heat transfer influences inlet mixture temperature, chamber, cylinder head, liner, piston and valve temperatures, and therefore end-gas temperatures, which affect knock. Heat transfer also affects build up of in-cylinder deposit which affects knock.

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Engine heat transfer environment

- Gas temperature: $\sim 300 - 3000^\circ\text{K}$
- Heat flux to wall: $\dot{Q}/A < 0$ (during intake) to 10 MW/m^2
- Materials limit:
 - Cast iron $\sim 400^\circ\text{C}$
 - Aluminum $\sim 300^\circ\text{C}$
 - Liner (oil film) $\sim 200^\circ\text{C}$
- Hottest components
 - Spark plug $>$ Exhaust valve $>$ Piston crown $>$ Head
 - Liner is relatively cool because of limited exposure to burned gas
- Source
 - Hot burned gas
 - Radiation from particles in diesel engines

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Energy flow diagram for an IC engine

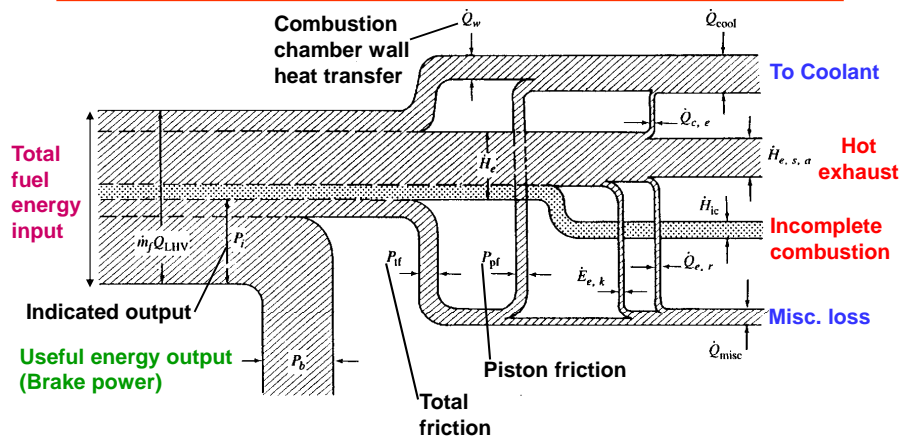


FIGURE 12-3

Energy flow diagram for IC engine. $(\dot{m}_f Q_{LHV})$ = fuel flow rate \times lower heating value, \dot{Q}_w = heat-transfer rate to combustion chamber wall, \dot{H}_e = exhaust gas enthalpy flux, \dot{P}_b = brake power, \dot{P}_{tf} = total friction power, \dot{P}_i = indicated power, \dot{P}_{pf} = piston friction power, \dot{Q}_{cool} = heat-rejection rate to coolant, $\dot{Q}_{e,r}$ = heat-transfer rate to coolant in exhaust ports, $\dot{H}_{e,s,a}$ = exhaust sensible enthalpy flux entering atmosphere, $\dot{H}_{e,ic}$ = exhaust chemical enthalpy flux due to incomplete combustion, $\dot{Q}_{e,r}$ = heat flux radiated from exhaust system, $\dot{E}_{e,k}$ = exhaust kinetic energy flux, \dot{Q}_{misc} = sum of remaining energy fluxes and transfers.

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Energy flow distribution for SI and Diesel

TABLE 12.1

Energy balance for automotive engines at maximum power

| | P_b | \dot{Q}_{cool} | \dot{Q}_{misc} | $\dot{H}_{e,lc}$ | $\dot{m}h_{e,s}$ |
|-----------|------------------------------------|------------------|------------------|------------------|------------------|
| | (percentage of fuel heating value) | | | | |
| SI engine | 25–28 | 17–26 | 3–10 | 2–5 | 34–45 |
| Diesel | 34–38 | 16–35 | 2–6 | 1–2 | 22–35 |

Sources: From Khovakh,³ Sitkei,⁴ and Burke *et al.*⁵

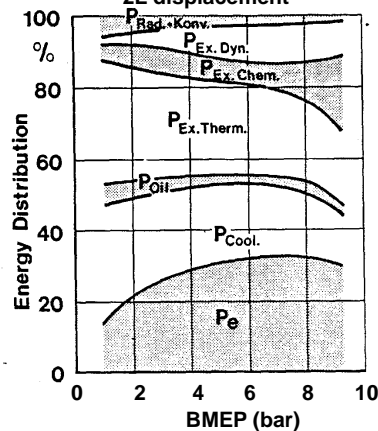
Update for modern engines:
SI engine in the low 30's
Diesel in the low 40's

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Energy distribution in SI engine

2000 rpm, water cooled SI engine
2L displacement



"Heat Balance of Modern Passenger Car SI Engines", Gruden, Kuper and Porsche, in *Heat and Mass Transfer in Gasoline and Diesel Engines*, ed. by Spalding and Afgan

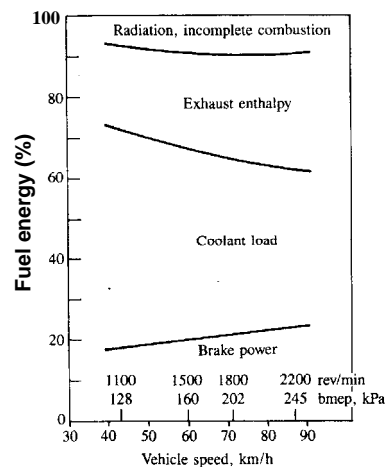
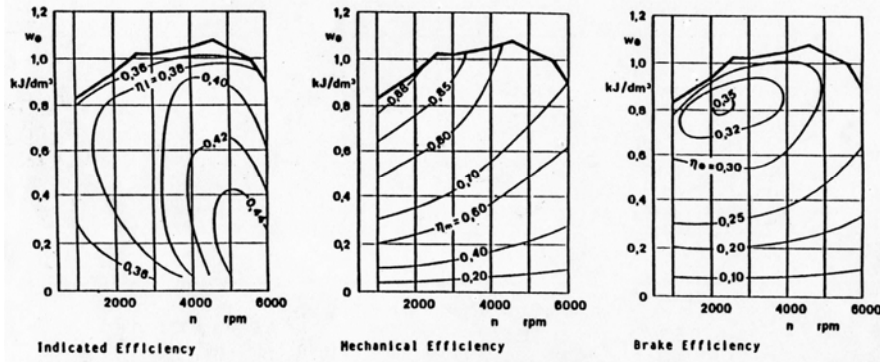


Fig. 12-4 SI engine energy distribution under road load condition, 6 cylinder engine; SAE Paper 770221, 1977

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Efficiency of Passenger Car SI Engines



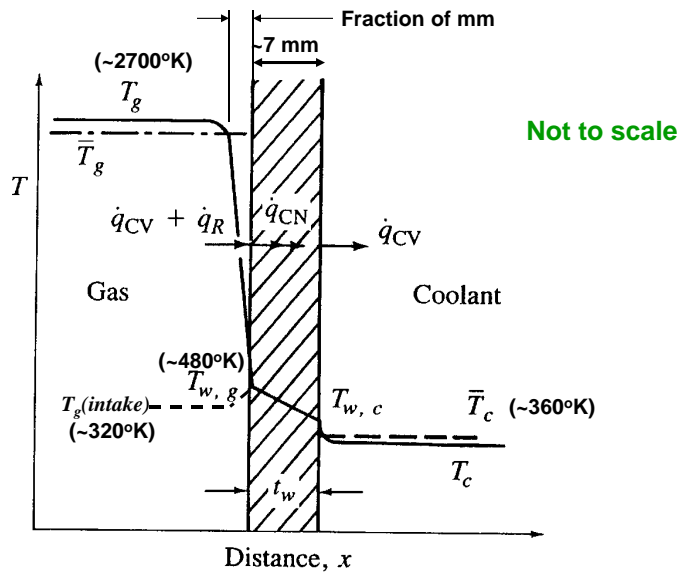
Source: D. Gruden, P.F., and F. Porsche AG. R & D Center Weissach, 1989.

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Heat transfer process in engines

- **Areas where heat transfer is important**
 - Intake system: manifold, port, valves
 - In-cylinder: cylinder head, piston, valves, liner
 - Exhaust system: valves, port, manifold, exhaust pipe
 - Coolant system: head, block, radiator
 - Oil system: head, piston, crank, oil cooler, sump
- **Information of interest**
 - Heat transfer per unit time (rate)
 - Heat transfer per cycle (often normalized by fuel heating value)
 - Variation with time and location of heat flux (heat transfer rate per unit area)

Schematic of temperature distribution and heat flow across the combustion chamber wall (Fig. 12-1)



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Combustion Chamber Heat Transfer

Turbulent convection: hot gas to wall

$$\dot{Q} = Ah_g(\bar{T}_g - T_{wg})$$

Conduction through wall

$$\dot{Q} = A \frac{\kappa}{t_w} (T_{wg} - T_{wc})$$

Turbulent convection: wall to coolant

$$\dot{Q} = Ah_c(T_{wc} - \bar{T}_c)$$

Overall heat transfer

$$\dot{Q} = Ah(\bar{T}_g - \bar{T}_c)$$

Overall thermal resistance: three resistance in series

$$\frac{1}{h} = \frac{1}{h_g} + \frac{t_w}{\kappa} + \frac{1}{h_c}$$

(κ_{alum} ~180 W/m-k
 $\kappa_{\text{cast iron}}$ ~ 60 W/m-k
 $\kappa_{\text{stainless steel}}$ ~18 W/m-k)

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Turbulent Convective Heat Transfer Correlation

Approach: Use Nusselt- Reynolds number correlations similar to those for turbulent pipe or flat plate flows.

e.g. In-cylinder:

$$\text{Nu} = \frac{hL}{\kappa} = a(\text{Re})^{0.8}$$

h = Heat transfer coefficient

L = Characteristic length (e.g. bore)

Re = Reynolds number, $\rho UL/\mu$

U = Characteristic gas velocity

κ = Gas thermal conductivity

μ = Gas viscosity

ρ = Gas density

a = Turbulent pipe flow correlation coefficient

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Radiative Heat Transfer

- Important in diesels due to presence of hot radiating particles (particulate matters) in the flame
- Radiation from hot gas relatively small

$$\dot{Q}_{\text{rad}} = \varepsilon \cdot \sigma \cdot T_{\text{particle}}^4$$

σ = Stefan Boltzman Constant ($5.67 \times 10^{-8} \text{ W/m}^2 \cdot \text{K}^4$)

ε = Emissivity

where

$$T_{\text{cyl. ave}} < T_{\text{particle}} < T_{\text{max burned gas}}$$

- Radiation spectrum peaks at λ_{max}
 $\lambda_{\text{max}} T = \text{constant}$ ($\lambda_{\text{max}} = 3 \mu\text{m}$ at 1000K)

Typically, in diesels: $\bar{Q}_{\text{rad}} \approx 0.2 \bar{Q}_{\text{total}}$ (cycle cum)

$\dot{Q}_{\text{rad, max}} \approx 0.4 \dot{Q}_{\text{total, max}}$ (peak value)

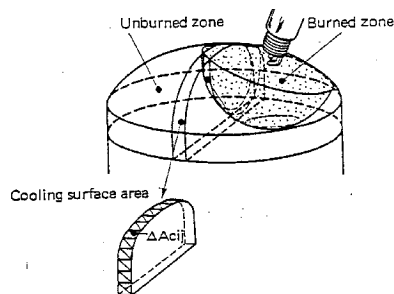
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IC Engine heat transfer

- Heat transfer mostly from hot burned gas
 - That from unburned gas is relatively small
 - Flame geometry and charge motion/turbulence level affects heat transfer rate
- Order of Magnitude
 - SI engine peak heat flux ~ 1-3 MW/m²
 - Diesel engine peak heat flux ~ 10 MW/m²
- For SI engine at part load, a reduction in heat losses by 10% results in an improvement in fuel consumption by 3%
 - Effect substantially less at high load

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SI Engine Heat Transfer



- Heat transfer dominated by that from the hot burned gas
- Burned gas wetted area determine by cylinder/ flame geometry
- Gas motion (swirl/ tumble) affects heat transfer coefficient

Heat transfer

Burned zone: sum over area "wetted" by burned gas

$$\dot{Q}_b = \sum_i A_{ci,b} h_b (T_b - T_{w,i})$$

Unburned zone: sum over area "wetted" by unburned gas

$$\dot{Q}_u = \sum_i A_{ci,u} h_u (T_u - T_{w,i})$$

Note: Burned zone heat flux >> unburned zone heat flux

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SI engine heat transfer environment

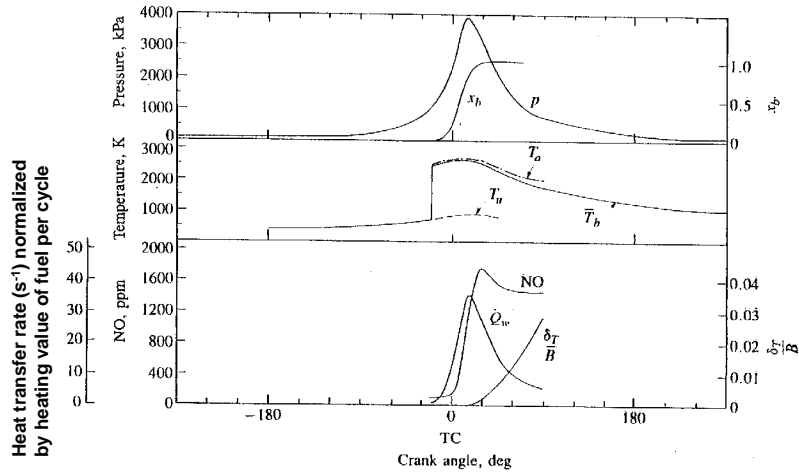
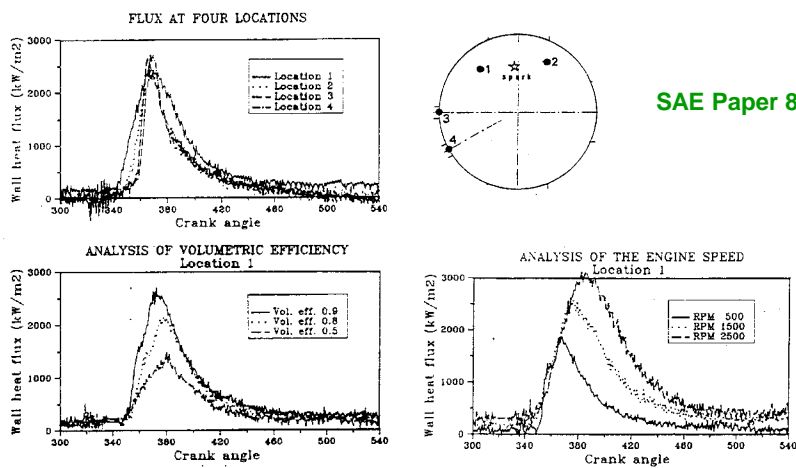


Fig. 14-9 5.7 L displacement, 8 cylinder engine at WOT, 2500 rpm; fuel equivalence ratio 1.1; GIMEP 918 kPa; specific fuel consumption 24 g/kW-hr.

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SI engine heat flux

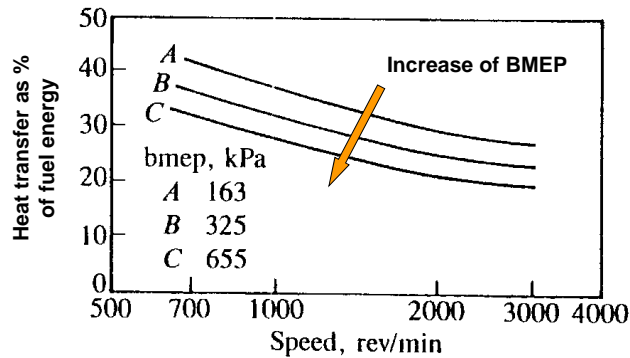


SAE Paper 880516

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Heat transfer scaling



Nu correlation: heat transfer rate $\propto \rho^{0.8} N^{0.8}$
Time available (per cycle) $\propto 1/N$
Fuel energy $\propto \rho$
BMEP $\propto \rho$

Fig. 12-25

Thus Heat Transfer/Fuel energy $\propto \text{BMEP}^{-0.2} N^{-0.2}$

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Diesel engine heat transfer

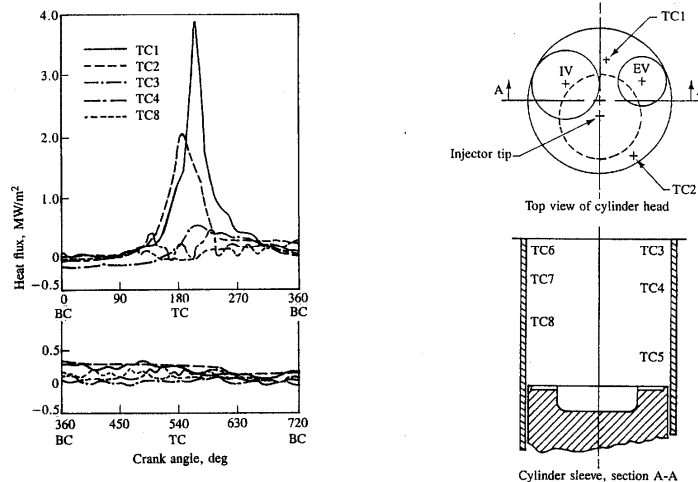


Fig. 12-13 Measured surface heat fluxes at different locations in cylinder head and liner of naturally aspirated 4-stroke DI diesel engine. Bore=stroke=114mm; 2000 rpm; overall fuel equivalence ratio = 0.45.

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Diesel engine radiative heat transfer

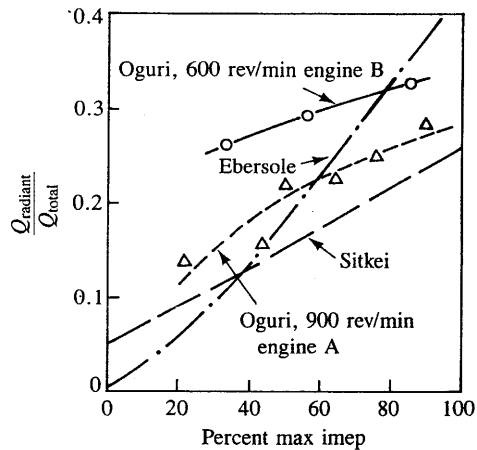


Fig. 12-15
Radiant heat flux as fraction of total heat flux over the load range of several different diesel engines

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Heat transfer effect on component temperatures Temperature distribution in head

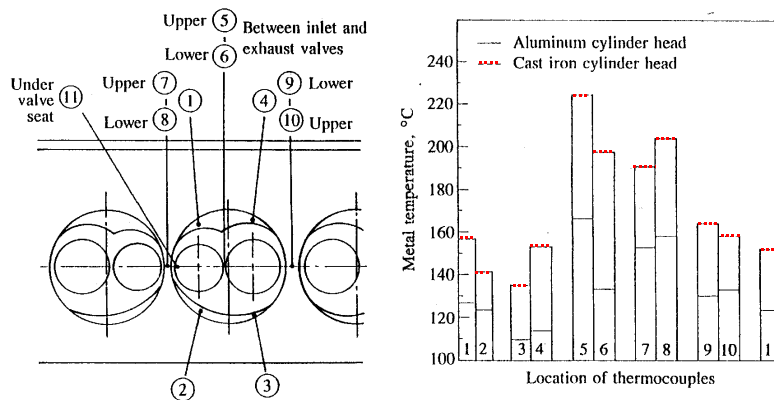


Fig. 12-20 Variation of cylinder head temperature with measurement location in SI engine operating at 2000 rpm, WOT, with coolant water at 95°C and 2 atmosphere.

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Heat transfer paths from piston

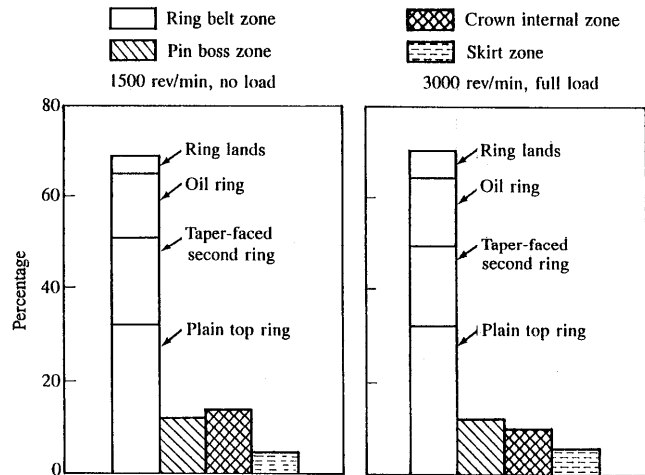


Fig. 12-4 Heat outflow from various zones of piston as percentage of heat flow in from combustion chamber. High-speed DI diesel engine, 125 mm bore, 110 mm stroke, CR=17

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Piston Temperature Distribution

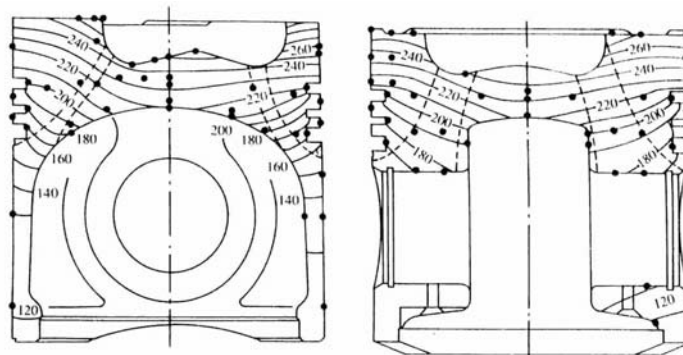


Figure 12-19

Isothermal contours (solid lines) and heat flow paths (dashed lines) determined from measured temperature distribution in piston of high speed DI diesel engine. Bore 125 mm, stroke 110 mm, $r_c=17$, 3000 rev/min, and full load

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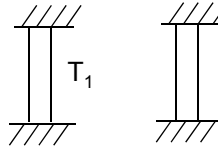
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Thermal stress

Simple 1D example : column constrained at ends

Stress-strain relationship

$$\epsilon_x = [\sigma_x - \nu(\sigma_y + \sigma_z)]/E + \alpha(T_2 - T_1)$$



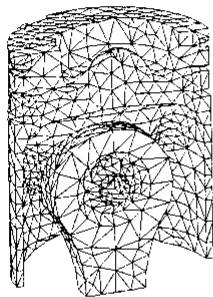
$T_2 > T_1$ induces compression stress

REAL APPLICATION - FINITE ELEMENT ANALYSIS

- Complicated 3D geometry
- Solution to heat flow to get temperature distribution
- Compatibility condition for each element

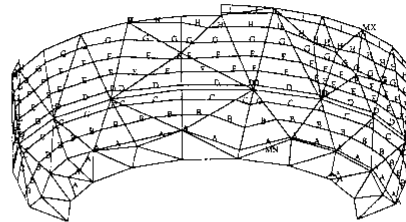
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Example of Thermal Stress Analysis: Piston Design



Power Cylinder Design Variables and Their Effects on Piston Combustion Bowl Edge Stresses
J. Castleman, SAE 932491

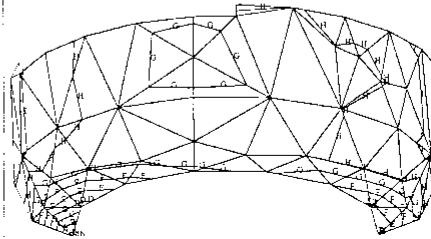
Heat Transfer Analysis



```

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MAX 0 1503
13.55.08
PLAT NO 3
POST1 378135
STEP 4969
ITER 1
TEMP
SMN =297.253
SMX =356.124
YV =1
ZY =0.4
DIST=1.419
XZ =-2.154825
YF =-0.708471
ZF =2.751
VDP =2
PRECISE HIDDEN
A =712.2
B =289.015
C =30.849
D =30.824
E =31.479
F =38.773
G =33.548
H =34.332
I =35.157
    
```

Thermal-Stress-Only Loading Structural Analysis



```

ANR75 4 441
MAX 0 1503
13.55.08
PLAT NO 5
POST1 378135
STEP 4969
ITER 1
TEMP
SMN =-8.8401
SMX =1.802
YV =1
ZY =0.4
DIST=1.419
XZ =-2.154825
YF =-0.708471
ZF =2.751
VDP =2
PRECISE HIDDEN
A =74.08
B =65.212
C =36.327
D =4.4322
E =38.527
F =39.631
G =20.756
H =11.611
I =3.345
    
```

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Heat Transfer Summary

1. Magnitude of heat transfer from the burned gas much greater than in any phase of cycle
2. Heat transfer is a significant performance loss and affects engine operation
 - Loss of available energy
 - Volumetric efficiency loss
 - Effect on knock in SI engine
 - Effect on mixture preparation in SI engine cold start
 - Effect on diesel engine cold start
3. Convective heat transfer depends on gas temperature, heat transfer coefficient, which depends on charge motion, and transfer area, which depends on flame/combustion chamber geometry
4. Radiative heat transfer is smaller than convective one, and it is only significant in diesel engines

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