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Influence of pore water pressure to seepage and stability of embankment dam (case study of Sermo Dam Yogyakarta, Indonesia)

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1 Introduction

Construction of the dam is needed so that water as a fundamental natural resource, can be long in the land before flowing back into the sea, as well as allow time to absorption the ground water. In order for the benefits to be sustainable, it needs to know the safety, especially when the dam operates. More than 70% dam in Indonesia is an embankment dam as stated by Soedibyo [1]. In this type of embankment dam, it should be taken into account in order to ensure its stability in retaining water.

One of the principal criteria for dam safety is safe against failure due to seepage [2]. Seepage through dam body and foundation can cause erosion. The transport of material through dam by seepage flow may result in fractures, which can reduce the capacity of dam. In addition, excessive seepage can cause reed erosion increasingly and potentially cause landslide until the dam collapse. Sudardja [3] stated that the seepage that occurred within embankment dam is affected by water level height.

In addition, with the change in water level can also affect the increase in pore water pressure. Pore water pressure can trigger embankment slope instability and deformation. Morton et al. [4] study on the high walls suggested that the increase in pore water pressure will lead to a reduction in stress, while decreasing pore water pressure will lead for an increasing in stress. When the

stress on land increases, it can increase strength of the ground to against instability resulting landslide on the slope. On the other way, if the stress on the ground is reduced, the more easily on slopes in landslide.

Deformation due to increased water levels studied on the Shuibuya Dam, China which is rockfill dam with impermeable layer of concrete in the upstream (Concrete Faced Rockfill Dam) [5]. Observation instrument for monitoring done at WS01 to WS11 which measures the deformation in the dam. Observations monitoring shows that when the water level increases, the settlement in dam also increases. In addition, the observation was also made by using Interferometric Synthetic Aperture Radar (InSAR), which has result that consistent with the result from the monitoring measurements. The combination of the results between monitoring in-situ and InSAR measurements indicate that the settlement is affected by gravity and the water level of reservoir at the dam, so that the largest settlement occurred at the peak of the dam.

The influence of dam water level with settlement is also given using a laboratory model of the embankment dam [6]. The study was conducted at three variations of the upstream slope of the dam, 1:1; 1:1.5; and 1:2. The result shows, when water level height increases, then the deformation is getting bigger. In addition, with the fill on the upstream slope steeper makes sliding on the downstream slope of the dam models more quickly occur.

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Based on these problems, it is necessary to study the seepage and stability analysis (in this case to be reviewed is settlement), to analyze the security of the dam caused by the influence of pore water pressure. Seepage and stability analyzes performed on operational condition so that it can be seen the influence of pore water pressure in these conditions. This study took place in the Sermo Dam located in the Hargowilis village, Kokap, Kulon Progo, Yogyakarta, Indonesia.

2 Research method

The research method is an important thing which is used as reference studies for research stage. In this study, the first stage is carried out based on the field data collection of water level from monitoring Peil Schaal and discharge of seepage monitoring V-Notch in the field at zero rainfall.

Sermo Dam modeling done by using PLAXIS in analyzing every operational conditions reviewed in the study. There are three cross sections on Sermo Dam, which are sta 12, sta 15, and sta 18, but in this study the cross section is reviewed in sta 15. Further analysis discharge of seepage, settlement, and the pore water pressure are based on modeling using PLAXIS and the explanation can be seen as follows.

2.1 Field data collection

Water levels are needed to determine the conditions used in this research analysis. In this study, determined the water level used is at the zero rainfall. Then graphed the relation between water level and discharge of seepage measurement with V-Notch, so it can be determined the discharge of seepage for each condition water levels is analyzed. Graph relation between water level and discharge of seepage can be seen in Figure 1, which uses 120 data field from 2000 to 2014 based on Departemen Pekerjaan Umum [7]. The graph's correlation value (R^2) is 0.666.

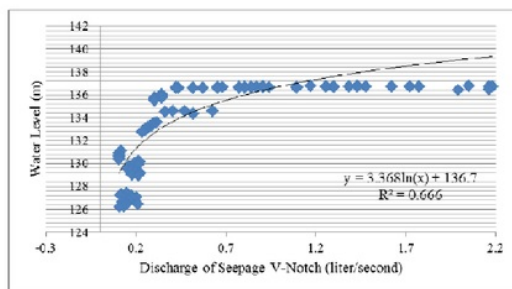


Fig. 1. Correlation between water level and discharge of seepage without rainfall condition

Water levels reviewed in this study analysis are 126.33 meters; 133.47 meters; 136.60 meters; and 136.71 meters. The selection of water level was adjusted to the availability of data piezometers in the field which is recorded every seven days. This is because before analysing this research study, then also do the data

validation checks between the value of pore water pressure monitoring with piezometers in the field and value of pore water pressure modeling simulation results using PLAXIS.

Based on the graph in Figure 1 and four water level that have been determined for analysing in this study, it can be obtained the new discharge of seepage V-Notch that can be seen in Table 1. Standard error of 120 data is 0.05, whereas the standard deviation is 0.537, so that can be determined the upper value limit and lower value limit of the new discharge of seepage. The upper value limit and lower value limit for the new discharge of seepage can be seen in Table 1.

Table 1. New discharge of seepage data through V-Notch

Water Level (m)	Discharge of Seepage V-Notch (liter/sec)	Uper Limit (liter/sec)	Lower Limit (liter/sec)
126.33	0.05	0.58	0.00
133.47	0.38	0.92	0.00
136.60	0.97	1.50	0.43
136.71	1.00	1.54	0.46

2.2 Modeling of Sermo Dam

Sermo Dam is included in zonal dam, consisting of permeable zone (shell), impermeable zone (core), and a filter zone (classification zone based on Sosrodarsono and Takeda [8]). Sermo Dam itself is a rockfill dam zonal types with clay core.

Figure 2 shows a cross-sectional Sermo Dam which is reviewed in this study, namely the sta 15. Figure 3 shows a cross section Sermo Dam on the sta 15 which is modeled using PLAXIS. It should be noted that at this Sermo Dam given chamber of 2.142 meters, from a height of 141.00 meters to 143.142 meters.

This study is conducted using modeling Mohr-Coulomb on PLAXIS, which is applying the finite element method by dividing the dam structure into small dots related with nodal (meshing). The finer meshing is done, then the result will be more accurate. In this study, using very fine type of meshing with 15-node. Very fine type of meshing produces about 1000 elements [9].

Parameters of material at the dam determined based on data from soil investigation by Caturbina Guna Persada [10] and field testing data from Departemen Pekerjaan Umum [11]. The data's parameters materials bedrock based on design data from Departemen Pekerjaan Umum [12].

Determining the value of permeability coefficient is from the result discharge of seepage measurements using PLAXIS modeling and calibrated with discharge of seepage from monitoring V-Notch in the field at water level 135.20 meters. The result in this discharge of seepage monitoring with V-Notch is 1.055 liters/second [7].

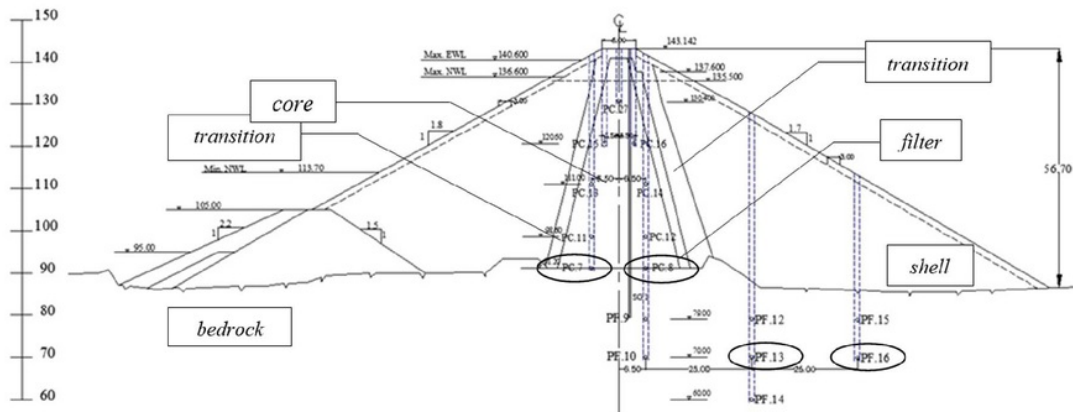


Fig. 2. Location of piezometer within the cross section of Sermo Dam [13]

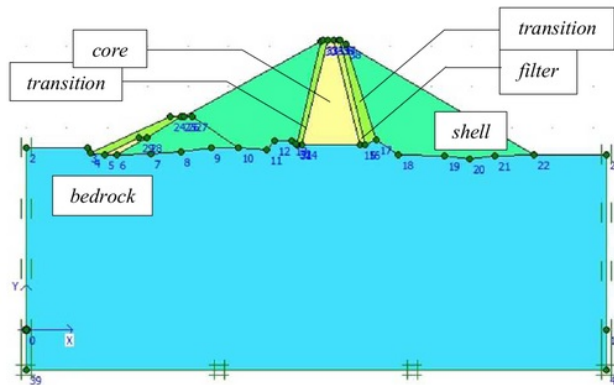


Fig. 3. PLAXIS modeling overview of Sermo Dam

Table 2. PLAXIS parameters of material used in the model of Sermo Dam

Zone of Dam	Parameter			
	$\gamma_{\text{saturated}}$ (kN/m ³)	$\gamma_{\text{unsaturated}}$ (kN/m ³)	Cohesion (c) (kN/m ²)	Angle of Friction (θ)
Core	18.74	15.41	8.3	32
Filter	21	18.5	0.001	35
Transition	21.7	21.6	0.001	35
Shell	21	20	0.001	43
Bedrock	21.82	20.12	680	55

Table 3. PLAXIS parameters of material used in the model of Sermo Dam

Zone of Dam	Parameter		
	Coefficient of Permeability (k) (m/day)	Young's Modulus (E) (kN/m ²)	Poisson (ν)
Core	2.32×10^{-4}	5500	0.45
Filter	134.10	6000	0.30
Transition	14.292	8000	0.30
Shell	12154.69	200000	0.35
Bedrock	6.00	210000	0.45

Calibration the parameters material is performed at three station locations within Sermo Dam, which are sta 12, sta 15, and sta 18, along 190 meters as the length of the peak of dam, so expect the results is obtained in accordance with the real situation on the field. Neither, the parameter values of Young's modulus and Poisson value figures on core zone, which are determined using back analysis method by calibration with settlement gauge. Thus parameter of materials values shown in Table 2.

2.3 Discharge of seepage analysis

Discharge of seepage calculation by analyzing the resultant discharge of the dam cross-section modeling using PLAXIS, which is calculated from the total discharge of seepage along 190 meters as the length of the dam. Discharge of seepage calculation results using modeling PLAXIS can be compared with measurements of the new discharge of seepage from V-Notch which has been calculated in Table 1, for each condition is analyzed.

Pore water pressure is measured at each stress point in PLAXIS modeling that has nearly same coordinates with the coordinates of the piezometer in field under review. Piezometer's reviewed in this study (see Figure

2) are on the upstream side of the PC-7 and PC-8 (core zone). Meanwhile, the downstream are in PF-13 and PF-16 (bedrock zone). Coordinates PC-7 and PC-8 are located at 143.85; 91.20 and 156.85; 91.20. While coordinate PF-13 and PF-16 are located at 181.85; 70.0 and 206.85; 70.0. In this study do a review of the settlement, as one aspect of stability. Analyse settlement is to look at the maximum settlement that occurred in the Sermo Dam using PLAXIS modeling.

3 Results and discussions

Based on the analysis performed, the results discharge of seepage using PLAXIS modeling in each waters levels are analyzed in this study shown in Table 3. From Table 3 it can be concluded that the higher water level then also higher the discharge of seepage. This is according to research that have been done before [3], which examined the effects of fluctuations in water level in the dam seepage using laboratory models. The stability in this study to evaluated is settlement. Large drop settlement can lead to instability of the dam. The relation of water level and the maximum settlement in the core zone is shown in Table 4.

Table 4. Discharge of seepage analysis on Sermo Dam using PLAXIS

Water Level (m)	Discharge of Seepage V-Notch (lt/sec) *	Uper Limit (lt/sec)	Lower Limit (lt/sec)	Discharge of Seepage Using PLAXIS (lt/sec)
126.33	0.05	0.58	0.00	0.58
133.47	0.38	0.92	0.00	0.69
136.60	0.97	1.50	0.43	0.71
136.71	1.00	1.54	0.46	0.83

* Based on Figure 1 and Table 1

Table 5. Maximum settlement on core zone of Sermo Dam using PLAXIS modeling

No	Water Level (m)	Maximum Settlement in the Core Zone (m)
1	126.33	1.10
2	133.47	1.14
3	136.60	1.16
4	136.71	1.16

Table 4 shows that in operational condition, the higher water level so does the settlement. This is relevant with research that have been done before [5], which examines monitoring settlement in Shuibuya Dam, China. The monitoring results show that when the water level increases, the settlement in dam will also increase. Additionally, there is also a study that studied the effect of fluctuations in water level in the dam deformation in laboratory model which is giving relevant conclusion [6].

According to the tolerable resulting discharge of seepage should not exceed 0.56 liters/minute/meter, for high dams greater than 40 meters [14]. The sta 15 of Sermo Dam which is analyzed in this study, has a height of 56.70 meters (Figure 2). Meanwhile, based on Table 3, the maximum discharge using PLAXIS is in the water level 136.71 meters with a discharge of 0.83 liters/sec or equal to 0.26 liters/minute/meter. The discharge value is smaller than 0.56 liters/minute/meter, so it is still less than the tolerable discharge requirements. Meanwhile, when seen from the settlement, the value of the maximum settlement result from numerical modeling using PLAXIS is 1.16 meters in water level of 136.71 meters (Table 4). The tolerance settlement at the end construction is 2% of dam height [15]. It is approaching with the value of settlement result from modeling using PLAXIS.

In this study, also given the relation between the water level and pore water pressure result using PLAXIS modeling. As already explained, that piezometers are reviewed on the upstream and downstream, they are PC-7, PC-8, PF-13, and PF-16 (Figure 2). The value of pore water pressure from PLAXIS modeling is obtainable by taking the stress point in PLAXIS which have similar or approaching coordinates (in x-axis and y-axis) with the coordinates in each piezometer that is reviewed. Relation between water level and pore water pressure in PC-7 and PC-8 modeling using PLAXIS can be seen in Table 5. Meanwhile Table 6 shown the relation between the water level and pore water pressure in PF-13 and PF-16.

Table 6. Relation between water level and pore water pressure on the PC-7 and PC-8 using PLAXIS

Water Level (m)	Pore Water Pressure			
	(PC-7)		(PC-8)	
126.33	34.57 kPa	126.32 m	16.83 kPa	126.67 m
133.47	41.20 kPa	133.46 m	33.32 kPa	130.97 m
136.60	54.30 kPa	135.59 m	45.88 kPa	132.25 m
136.71	66.19 kPa	136.50 m	61.13 kPa	135.25 m

Table 7. Relation between water level and pore water pressure on the PF-13 and PF-16 using PLAXIS

Water Level (m)	Pore Water Pressure			
	(PF-13)		(PF-16)	
126.33	6.79 kPa	88.46 m	4.30 kPa	86.67 m
133.47	9.50 kPa	87.66 m	9.47 kPa	85.59 m
136.60	14.26 kPa	87.01 m	10.54 kPa	85.28 m
136.71	16.17 kPa	86.97 m	11.54 kPa	85.37 m

Table 5 and Table 6 show that the higher water level, the higher the pore water pressure, and at a position downstream of the dam (bedrock zone in PF-13 and PF-16), the pore water pressure will be smaller than in upstream of the dam (core zone in PC-7 and PC-8). In addition, it can be concluded that when the water level increases, the pore water pressure will also increases. Increasing water level can cause an increase pore water

pressure, this is because the material is in the saturated condition resulting from the flow of water seepage into the body of the dam, as a consequence of the water level height. Saturated material will increase pore water pressure, especially with the long drainage because the material in the core of Sermo Dam is a cohesive soil (as a location of PC-7 and PC-8). So that, in PC-7 and PC-8 have value of pore water pressure greater than in the PF-13 and PF-16. From Figure 2, is known that PF-13 and PF-16 are located in the bedrock zone or foundation of the dam, which is composed of andesite breccia rocks making the material easier for draining water seepage.

The increase in pore water pressure that occurs may lead to increases the discharge of seepage, which can be seen in Table 3. The discharge of seepage could cause settlement that occurred also increased significantly (Table 4). Increasing the settlement occurred because of water seepage in the dam body causes the material changes in saturated condition. Then, the value of the materials will changed. So that, the stress will reduced. The stress reduction will impact on increasing the settlement and reducing the stability of dam in retaining water. This is also according to research conducted on a high wall [4], which is an increasing pore water pressure will lead to a reduction in stress, while decreasing pore water pressure will lead to an increasing in stress. When the stress increases, so that can increase the soil strength to against instability.

4 Conclusion

Based on the existing problem in this study is about the influence of pore water pressure on the seepage and stability with a case study on Sermo Dam, could be concluded as follows:

1. Analysis of the PLAXIS modeling shows that water levels affect the increase of pore water pressure. The higher the water level, the higher the pore water pressure. With the increase in pore water pressure, the discharge of seepage that occurs will also increase.
2. Increasing the pore water pressure due to change of water level height led to increased discharge of seepage and settlement. This is due to water seepage causes the materials become saturated and the value of materials will changed and the stress will reduced. Reduction of stress will impact on the instability of dam structure.

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