

LAMPIRAN

Perhitungan Perancangan Heat Exchanger

Shell side		Tube side	Temperatur :	
IDs	= 10 in	IDt	= 0,62 in	Th1 = 60°C 140°F
B	= 7	ODt	= ¾	Th2 = 36°C 96,8°F
Baffle space	= 6 in	BWG	= 16	Th1 = 24°C 43,2 °F
Passes	= 1	pitch	= triangular	Tc1 = 28°C 82,4°F
Pt	= 0,9375	passes	= 2	Tc2 = 36°C 96,8°F
C	=0,99(fig.2	C	=0,98(fig2	ΔTc = 8 °C 14,4 °
Kern)		Kern)		
de	=0,045833333 ft	Nt	= 12	

Shell

1. Heat Balance :

$$\Delta T_{LMTD} = \frac{\Delta T_1 - \Delta T_2}{\ln \Delta t_1 / \Delta t_2}$$

$$= \frac{43,2 - 14,4}{\ln \left(\frac{43,2}{14,4} \right)}$$

$$= 26,215 \text{ } ^\circ \text{F}$$

$$Q = 67900,423 \text{ Btu/jam}$$

$$Q_{\text{shell}} = W \times C(\text{Th1} - \text{Th2})$$

$$W_{\text{shell}} = Q / C(\text{Th1} - \text{Th2})$$

$$= 67900,423 / (0,99 \times 43,2 \text{ } ^\circ \text{F})$$

$$= 1587,646 \text{ lb/jam}$$

$$Q_{\text{tube}} = W \times C(\text{Th1} - \text{Th2})$$

$$W_{\text{tube}} = Q / C(\text{Th1} - \text{Th2})$$

$$= 67900,423 / (0,98 \times 14,4 \text{ } ^\circ \text{F})$$

$$= 4811,538 \text{ lb/jam}$$

2. $\Delta t =$

Hot Fluid		Cold Fluid	Differential
140	Higher Temp	82,4	57,6
96,8	Lower Temp	96,8	0
43,2	Differential	14,4	57,6

$$L = 1 \text{ m}$$

$$= 3,2808399 \text{ ft}$$

$$= 39,370079 \text{ in}$$

$$\text{LMTD} = 26,215^\circ\text{F}$$

$$R = \frac{43,2}{14,4}$$

$$= 3$$

$$S = \frac{14,4}{140 - 96,8}$$

$$= 0,333$$

$$F_t = 0,98 \text{ (Fig 18 Kern)}$$

$$\Delta t = F_t \times \Delta T_{\text{LMTD}}$$

$$= 0,98 \times 26,215^\circ\text{F}$$

$$= 25,691^\circ\text{F}$$

Shell

3. Hot Fluid; shell side, water

4. $A_s = ID \times C'B / 144Pt$

dengan $C' = Pt - OD$

$$= 0,9375 - \frac{3}{4}$$

$$= 0,188 \text{ in}$$

$$B = L/b$$

$$= \frac{39,370079 \text{ in}}{6 \text{ in}}$$

$$= 7$$

$A_s = ID \times C'B / 144Pt$

$$= 10 \text{ in} \times 0,188 \times (7 / 144) \times 0,9375$$

$$= 0,091 \text{ ft}^2$$

5. $G_s = W/a_s$

$$= 1587,646 \text{ lb/jam} / 0,091 \text{ ft}^2$$

$$= 17.446,66 \text{ lb/jam ft}^2$$

6. $T_a = (Th_1 + Th_2) / 2$

$$= (140^\circ\text{F} + 96,8^\circ\text{F}) / 2$$

$$= 118,4^\circ\text{F}$$

$$7. D_s = I_{Ds}/12$$

$$= 10 \text{ in} / 12$$

$$= 0,833 \text{ ft}$$

$$8. Res = (D_s \times G_s) / \mu$$

$$= (0,833 \text{ ft} \times 17.446,66 \text{ lb/jam ft}^2) / 0,8712 \text{ lb/jam ft}$$

$$= 16.681,667 \text{ (Turbulen)}$$

$$9. jH = 380 \text{ (fig 28 Kern)}$$

$$10. At_{Ta} = 118,4^\circ\text{F}$$

$$c = 1 \text{ Btu/lb } ^\circ\text{F}$$

$$k = 0.898 \text{ Btu/(jam)(ft}^2)(^\circ\text{F/ft)} \text{ (Tabel 4 Kern)}$$

$$(c\mu/k)^{(1/3)} = (0,99 \times 0,8712/0,898)^{(1/3)}$$

$$= 0,98664$$

$$11. h_o = jH \times k/d_e \times (c\mu/k)^{(1/3)}$$

$$= 380 \times 0,898 \text{ Btu/(jam)(ft}^2)(^\circ\text{F)} / (0,045833333 \text{ ft}) \times 0,98664$$

$$= 90552,580 \text{ Btu/jam ft}^{2^\circ\text{F}}$$

Tube

3. Cold Fluid; tube side, water

4. $a't = 0,302 \text{ in}^2$ (table 10 Kern)

$$at = Ntxa't / 144xn$$

$$= 12 \times (0,302 \text{ in}^2 / 144) \times 2$$

$$= 0,0503 \text{ ft}^2$$

$$5. \quad Gt = w/at$$

$$= 4811,538 \text{ lb/jam} / 0,0503 \text{ ft}^2$$

$$= 95.656,82 \text{ lb/jamft}^2$$

$$\text{vel, } v = Gt/3600_e$$

$$= 95.656,82 \text{ lb/jam} /$$

$$(3600 \times 62,5)$$

$$= 0,425 \text{ ft/sec}$$

$$6. \quad \text{At } t_a = (Tc_1 + Tc_2) / 2$$

$$= (82,4^\circ\text{F} + 96,8^\circ\text{F}) / 2$$

$$= 89,6^\circ\text{F}$$

$$\mu = ((0,95 \cdot 2,42) + (0,8 \cdot 2,42)) / 2$$

$$= 0,8712 \text{ lb/jamft}$$

$$= 2,118 \text{ lb/jamft (fig. 14)}$$

$$\mu = ((0,35 \cdot 2,42) + (0,37 \cdot 2,42)) / 2$$

$$= 0,8712 \text{ lb/jamft}$$

$$7. D = IDt/12$$

$$= 0,62/12$$

$$= 0,052 \text{ ft}$$

$$8. \text{Ret} = D \times Gt/\mu$$

$$= 0,052 \text{ ft} \times 95.656,82 \text{ lb/jamft}^2 / 2,118 \text{ lb/jamft}$$

$$= 2.348,5150 \text{ (laminar)}$$

$$9. h_i = 415 \text{ Btu/jam (ft}^2) (\text{°F}) \quad (\text{fig 25 kern})$$

$$10. h_{io} = h_i \times ID/OD$$

$$= 415 \text{ Btu/jam (ft}^2) (\text{°F}) \times (0,62 \text{ in} / \frac{3}{4})$$

$$= 343,067$$

$$12) \text{ Clean overall } (U_c) = h_{io} \times h_o / h_{io} + h_o$$

$$= (343,067 \times 90552,580) / (343,067 + 90552,580)$$

$$= 341,772 \text{ Btu/(jam)(ft}^2)(\text{°F})$$

13) Design overall coefficient U_D :

$U_D = 340 \text{ btu/jam ft}^2 \text{ °F}$ didapat dari tabel.8 Kern

$$U_D = \frac{Q}{A \Delta T}$$

$$340 \text{ btu/jam ft}^2 \text{ °F} = \frac{67900,423 \frac{\text{Btu}}{\text{jam}}}{A \cdot 26,215 \text{ °F}}$$

$$A = \frac{67900,423 \text{ Btu /jam}}{340 \text{ btu/jam ft}^2 \text{ °F} \cdot 26,215 \text{ °F}}$$

$$A = 7,618 \text{ ft}^2$$

$$\begin{aligned}
 14) \text{ Rd} &= U_c - U_D / U_c \times U_D \\
 &= (341,772 - 340) / (341,772 \times 340) \\
 &= 0,00002 \text{ (hr) (ft}^2\text{)(}^\circ\text{F) / Btu}
 \end{aligned}$$

Summary

90552,580	h outside	343,067
U _c	341,772	
U _D	340	
Rd Calculated	0.00002	
Rd Required	0.001	

Pressure Drop

Shell

$$1) \text{ Res} = 16.681,667$$

$$f = 0.001 \text{ ft/in}^2$$

$$2) \text{ No. of crosses, } N + 1 = 12L/B$$

$$= 12 \times 6,56167979$$

$$= 78,74$$

$$D_s = 10/12$$

$$= 0,833 \text{ ft}$$

$$3) \Delta P_s = (f \times G_s^2 \times D_s \times (N+1)) / (5,22 \times 10^{10} \times D_s \times \phi_s)$$

$$= ((0,001 \times (17.446,66 \text{ lb/jam ft}^2)^2 \times 0,833 \times 78,74)) / (5,22 \times 10^{10} \times 0,833 \times 1)$$

$$= 0,000 \text{ psi}$$

Tube

$$1) \text{ Ret} = 2.348,5150$$

$$= 0,00015 \text{ ft}^2 / \text{in}^2$$

$$2) \Delta P_t = (f \times G_t^2 \times L \times n) / (5,22 \times 10^{10} \times D_s \times \phi_t)$$

$$= ((0,00015 \times (95.656,82)^2 \times 1 \times 2) / (5,22 \times 10^{10} \times 0,052 \times 1))$$

$$= 0,001 \text{ psi}$$

$$3) G_t = 95.656,82 \text{ lb/jamft}^2$$

$$V^2/2G' = 0,03$$

$$4) \Delta P_r = 4 \text{ n/s } (V^2/2G')$$

$$= 4 \times (2/1) \times 0,03$$

$$= 0,24 \text{ psi}$$

$$\Delta P_T = \Delta P_t + \Delta P_r$$

$$= 0,001 + 0,24$$

$$= 0,241 \text{ psi}$$