

# ANALYSIS OF ALSELMANI SIGNALIZED INTERSECTION IN BENGHAZI - LIBYA

## Thesis

Submitted as Partial Fulfilling of the Requirement for the Research Methodology Lecturer of Master of the Civil Engineering Diponegoro University

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#### ABSTRACT

Intersections play an important role in the road network, where traffic flows in different directions converge. Because of their influence each other, disturbance of pedestrians and bicycle to vehicles, and the lost of green time for beginning and clearance and so on.

The spectacular growth of vehicles, as of the most convenient mode of travel has brought in its wake problems of frustration, accidents, delays, queues, congestion and environmental degradation. This has generated a new branch of the circulation of knowledge, known as traffic management. The argument is gaining importance as vehicles whose population is increasing in recent years, and traffic problems become more alarming. In many situations of daily life, it addresses the problem of providing services to the requirements of random. Consider the simple case of drivers who arrive at a junction with traffic lights, if the arrival rate is high and the rate of supply is unable to cope, it is inevitable that increases in the queue. Delay occurred as a result. In fact, queuing and delays to traffic at intersections, especially at the traffic light is a common problem in dealing with urban traffic. In this perspective, it is necessary to apply appropriate management of traffic at critical intersections to minimize the effect of delays and queues for the global system of circulation. Thus, knowledge on methods of traffic management is essential. In the recent years vehicle ownership and traffic volume in links increase dramatically due to the continuous high speed growth, which cause traffic congestion of different level in Bengazi city.. The objective of this study is to evaluate the performance of intersection and make alternative solutions recommendation. The analysis is done by evaluating the performance of intersection, including the initial conditions of intersection by using Indonesian Highway Capacity Manual (IHCM 1997).so the traffic flow, Then saturation flow rates and delays of the intersection Finally, some countermeasures for enhancing the capacities of the intersection are proposed including channelization of the traffic flow in the intersection, drawing the traffic marking and line in the intersection, strengthen traffic safety education, improving traffic control method, regulation of pedestrians and bicycle flows at the signalized intersection and improving the safety facility and capacity at the signalized intersections and so on. The control was changed from two-phase to four-phase control during , leading to excessive queuing in the area. The calculations for four phase control shows the reason why, the Intersection flow ratio increases, and the degree of saturation becomes higher in all approaches during the studied peak hour. The reason to change from two-phase to four-phase control was probably that the there were many traffic accidents in the intersection. An alternative action would have been to increase the inter-green periods between the phases, and to keep two-phase control which obviously results in a much higher intersection capacity and better level of performance level. The advantage of changed to four phase: inevitably leads to an increase of the cycle time and of the ratio of time allocated to switching between phases (Intergreen). Although this may be beneficial from the traffic safety point of view, it normally means that the overall capacity of the intersection is decreased.

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## CHAPTER 1 INTRODUCTION

#### 1.1 Background

Intersections play an important role in the road network, where traffic flows in different directions converge. Because of their influence each other, disturbance of pedestrians and bicycle to vehicles, and the lost of green time for beginning and clearance and so on , the capacity of intersections is much lower than that of their approach links. Thus, the intersections usually are the bottleneck of the network, the popular and immediate source of the traffic jam and traffic accidents. Benghazi City is the second largest city of Libya contains a lot of Beaches monuments and places and in holiday times crowded roads in the city because a lot of people come to spend the holiday in Benghazi. And especially the city is costal , tourist city and also close to the Seaport .

The increasing numbers of motor vehicles in Libya, all kinds of private cars, private transport, taxis and trucks and heavy equipment an indication of the severity of congestion on major roads between main and interior cities, there is continual congestion, traffic congestion is frequently a problem through the weekdays. Both geographically and administratively, the network started to suffer from various traffic problems. More and more policies and regulations are being developed, particularly in the field of traffic and transport. The spectacular growth of vehicles, as of the most convenient mode of travel has brought in its wake problems of frustration, accidents, delays, queues, congestion and environmental degradation. This has generated a new branch of the circulation of knowledge, known as traffic management. The argument is gaining importance as vehicles whose population is increasing in recent years, and traffic problems become more alarming. In many situations of daily life, it addresses the problem of providing services to the requirements of random. Consider the simple case of drivers who arrive at a junction with traffic lights, if the arrival rate is high and the rate of supply is unable to cope, it is inevitable that increases in the queue. Delay occurred as a result. In fact, queuing and delays to traffic at intersections, especially at the traffic light is a common problem in dealing with urban traffic. In this perspective, it is necessary to apply appropriate management of traffic at critical intersections to minimize the effect of delays and queues for the global system of circulation. Thus, knowledge on methods of traffic management is essential. In the recent years vehicle ownership and traffic volume in links increase

dramatically due to the continuous high speed growth, which cause traffic congestion of different level in Benghazi city. Under this circumstance, velocity of vehicles drops largely and in the city the velocity in peak hour is even lower than 10 km/h. All of these already influence the normal performance of urban function, hamper the continuous and steady growth of the economy and affect residents' daily lives. It is also same for the developed country, the most. Traffic congestion happens at the intersection in Benghazi. First two main reasons causing the traffic congestion in Benghazi is as follows: there is an exclusive lane for right turn, right turn vehicle obscures the following vehicle and the capacity of the intersection is enough; Thus, it is significant to study the traffic flow characteristics at signalized intersections because the capacity of the intersection can be improved according to their Characteristics. Study on traffic flow characteristics at signalized intersections is one of most effective and immediate measure to enhance the capacity of road networks and relieve the congestion in the city. In this study, the traffic flow, Then saturation flow rates and delays of the intersection Finally, some countermeasures for enhancing the capacities of the intersection are proposed including channelization of the traffic flow in the intersection, drawing the traffic marking and line in the intersection, strengthen traffic safety education, improving traffic control method, regulation of pedestrians and bicycle flows at the signalized intersection and improving the safety facility and capacity at the signalized intersections and so on. The objective of the research is to evaluate the performance of intersection using the 1997 IHCM. The phases, cycle times, green times, amber and red lights for this intersection will be varied by existing traffic flow. The performance of this intersection will be expected to perform better, so the traffic jam such as delay and queuing could be reduced.

#### **1.2 Problem Statement**

As it was mentioned earlier in this chapter, the selected operating mode of traffic signal for a particular intersection is usually based on a measured or estimated peak traffic volume. This may provide efficient traffic flow during rush hours; however, operation during off-peak hours will be far from ideal. This happens because the main traffic parameter for signal design changes significantly. In most cases during the off-peak hours, the traffic volume decreases a lot and vehicle arrival patterns are random in nature. The conditions stated above make it hard or almost impossible to find a single optimal plan for signal timing. It can be even worse at an intersection where the traffic signal is coordinated

with another traffic signal at different intersections. That particular problem can be very obvious in Benghazi Because it is a tourist and costal town and there is commercial seaport that is why the traffic congestion is common. The lack of optimized traffic control during off-peak hours can cause different issues such as travel delay and increased gas consumption for travelers who may be stuck at traffic lights on empty roads. But, most importantly, these conditions may cause safety issues – being stuck at the traffic light at night a driver may be robbed or experience other serious safety and security issues. Modern traffic signal systems researches have already come with a solution for that problem introducing several types of traffic signal operations including pre-timed, fully actuated, semi-actuated and flashing signal operating patterns. Improvements in off-peak traffic signal control can be beneficial for drives making it possible to get to their final destination during off-peak hours much faster. Importance Alsellmani Street does not lie in being a carrier route only but one of the key facilities which are located in the north and south of the intersection where there is a huge number means these facilities and thus witnessing the early morning hours and afternoon hours busiest great to get to these facilities .The east side is linked to the coastal road that connects the city and suburbs who have most of the city's population follow in terms of labor and universities, who is also witnessing at its busiest great morning and afternoon (the end of working hours).



(Sorce: Atlas Book Of Benghazi(2010))



Figure 1.2 Alselmani Intersection

## 1.3 Objective Of Study

The objective of this study is to evaluate the performance of intersection and make alternative solutions recommendation. The analysis is done by evaluating the performance of intersection, including the initial conditions of intersection by using Indonesian Highway Capacity Manual (IHCM 1997).

#### 1.4 Scope Of Study

This study focuses on the estimation of delays and queue lengths that result from the adoption of a signal control strategy at an intersection, Traffic delays and queues are principal performance measures of intersections. In the evaluation of the adequacy of cycle length, the obtained minimum delay being the foremost goal of the traffic engineers.

#### 1.5 Organization Of Thesis

To facilitate reading and comprehension, the results of recent studies will need to be classified parts of the report follow a systematic study as follows:

#### A. CHAPTER I (Introduction)

Contains a description of the background research, the research aims and objectives, constraints and systematic problems of writing.

#### B. CHAPTER II (Review Books)

Contains a description of the basics of theories related to the trip of the traffic, the model and its characteristics, statistical methods, and previous studies of similar or similar has ever done.

#### C. CHAPTER III (Research Methodology)

Contains a description of the mindset of research, stages and procedures of research and analytical methods used.

#### D. CHAPTER IV (Data Analysis and Discussion)

This section contains a description of the data results of research on the trip model of traffic is accompanied by analysis and discussion of the nature and trends of the results of the study.

#### E. CHAPTER V (Conclusions and Recommendations)

This section contains a description of the conclusions can be drawn from the results of analysis of the results of research that has been done. Also presented suggestions for the application of research results in the field and to the possibility of further study.

# CHAPTER 2 LITERATURE REVIEW

#### 2.1 Signalized Intersection

As the number of vehicles in use increases in all developing countries the most severe congestion is being experienced in urban areas where the number of junctions severely restricts traffic flow. Urban Transport has many particular features in the form of journeys to work peak hour, congestion, traffic restrains measures, public transport priorities act. The usual solution to the problem of junction capacity has been either to make the area of the junction larger, or to adopt grade separation. The former is difficult to achieve in congested urban areas and the latter is extremely expensive. It is therefore important to investigate every possible means of increasing the capacity of the single level junction so that delays are reduced. Intersection is of the greatest importance in highway design because of their effect on the movements and safety of vehicular traffic flow. The actual place of intersection is determined by setting and design and the act of the intersection by the regulation and control of the traffic movement. Priority control of traffic at junction is one of the most widely used ways of resolving the conflict between merging and crossing vehicles. The universal adoption of the 'Give Way to traffic on the right' rule at roundabouts together with the use of 'Give Way' and 'Stop' control at junctions has considerably increased the number of occasions at which a driver has to merge or cross a major road traffic stream making use of gaps or lags in one or more conflicting stream. Normally traffic signal is introduced for one or more of the following reasons:

- To avoid blockage of an intersection by conflicting traffic stream, thus guaranteeing that a certain capacity can be maintained even during peak traffic conditions; (Proceedings of the Eastern Asia Society for Transportation Studies, Vol.4, October, 2003).
- To facilitate the crossing of major road by the vehicles and/or pedestrian from a minor road;
- To reduce the number of traffic accidents caused by collisions between vehicles in conflicting directions. Signalization by means of three-colored light (green, amber, red) is applied to separate of conflicting traffic movement in time. Three

basic mechanisms, which affect intersection operation and performance, should be well understood:

- Discharge headways at signalized intersections, and their relationship to lost times and saturation flow rates.
- > Factor affecting right turn at a signalized intersection.
- Uses of demand volume.

The capacity of a traffic signal controlled intersection is limited by the capacities of the individual approaches to the intersection. There are two types of factor, which affect the capacity of approach, roadway and environment factor and traffic and control factor. The roadway and environmental factor that controls the capacity of an approach are the physical layout of the approach, in particular its width, the road along which left or right turning vehicle has to travel, and the gradient of the approach and its exit from the intersection. The capacity of an approach is measured independently of traffic and control factors and is expressed as the saturation flow. Saturation flow is defined as the maximum flow, expressed as equivalent passenger cars that can cross the stop line of the approach when there is a continuous green signal indication and a continuous queue of vehicles on the approach. Delay is used to define the level of service at signalized intersections, since delay not only indicates the amount of lost travel time and fuel consumption; it is also a measure of the frustration and discomfort of motorists. Delay, depends on the red time, which in turn depend on the length of the cycle. Reasonable levels of service can therefore be obtained for short cycle length, even though the (v/c) ratio is as high as 0.9. The LOS criteria are given in term of the average stopped delay per vehicle during an analysis period of 15 min. Level of service C described that level of operation at which delay per vehicle ranges from 15.1 to 25 Sec. At level of service C, many vehicles go through the intersection without stopping, but a significant number of vehicles are stopped. In addition, not all vehicles at an approach clear the intersection during a few cycles (cycle failure). The higher delay may be due to the significant number of vehicles arriving during the red phases (poor progression) and or relative long cycle lengths. Level of service D described that level of operation at which delay per vehicle ranges from 25.1 to 40 Sec. At level of service D, vehicles are stopped at the intersection, resulting in the longer delay. The number of individual cycles failing is now noticeable. The longer delay at this level of service is due to a combination of two or more several factors that include long cycle length, high (v/c) ratios, and unfavorable progression.

Level of service E describes that level of operation at which the delay per vehicle ranges from 40.1 to 60 Sec. At level of service E, individual cycle's frequency fails. This long delay, which is usually taken as the limit of accepted delay, generally indicates high (v/c) ratios, long cycle lengths, and poor progression Level of service F describes that level of operation at which the delay per vehicle is greater than 60 sec. This long delay is usually unacceptable to most motorists. At level of service F the phenomenon know as over saturation usually occurs that is arrival flow rates are greater than the capacity of the intersection. Long delay can also occur as a result of poor progression and long cycle length. Note that this level of service can occur when approaches have high (V/C) ratios, which are less than 1.00, but also have many individual cycles failing. Area Traffic Control: where the traffic is controlled at junctions in street network that the output at one junction are related in some way to the inputs at adjacent junctions. The interaction between individual components of the system affects the overall network performance. Linked and coordinated signal plans are mainly applicable to the principal linear routes. Methods of controlling traffic in the network are referred to as area traffic control and may also include a control mode, which is traffic responsive. Area traffic control first became feasible with the introduction of the electronic computer. Further analysis can be carried out and modifications introduced which further refine the choices, and improve sensitivity and performance. In dynamic control systems the greatest difficulty lies in describing, in a logical and mathematical way, the behavior of traffic and the rapid computation of optimum control policies. An important part of the communication system is the link between the detector and the central computer and the return link conveying instructions to the signal. The data transmission system usually operates through out-stations, connected to the traffic signal controllers, and collecting data from the individual detectors. This information before or after local processing is relayed over cables, usually rented telephone pairs, to the central controller. Control instruction is transmitted in a reverse direction to the local controller via the out station. Each part of the system has a unique address, which can be interrogated by the central controller either for data retrieval and resetting or for instruction and control operation. It is usually necessary to monitor thus key points which have a critical effect on the control of the whole system and closed-circuit television is often provided for this purposed.

#### 2.2 Analysis Of Signalised Intersection By Using IHCM 1997

Indonesia Highway Capacity Manual is program for determination of signal timing, capacity and traffic performance (delay, queue length and proportion of stopping vehicles) for signalized intersection in urban and semi-urban areas. The traffic facilities capacity and traffic performance is primarily a function of geometric conditions and traffic demand. By means of the signal however, the planner can distribute capacity to different approaches through the green time allocated to each approach. In order to calculate capacity and traffic performance it is therefore necessary to first determine the signal phasing and timing, which is most appropriate for the studied condition. The methodology for analysis of signalized intersections described below is based on the following main principles:

#### a. Geometry:

The calculations are done separately for each approach. One intersection arm can consist of more than one approach, i.e. be divided into two or more subapproaches. This is the case if the right turning and/or left turning movements received green signal in different phases (s) than the straight thought traffic, or if they are physically divided by a traffic island in the approach. For each approach or sub-approach the effective width (We) is determined with consideration to the layout of the entry and the exit and distribution of turning movements.

#### b. Traffic flow:

The calculation is performed on an hourly basis for one or more periods, e.g. based on peak hour design flow for morning, noon and afternoon traffic conditions. The traffic flow for each movement (left turning, straight through and right turning are converted from vehicles per hour to passenger car units (pcu) per car units (pcu) per hour using the following passenger car equivalent (pce) for protected and for opposed approach types

| Vehicle Type      | Pce for approach type |         |  |  |  |
|-------------------|-----------------------|---------|--|--|--|
| veniere rype      | Protected             | Opposed |  |  |  |
| Light Veh . (L V) | 1.0                   | 1.0     |  |  |  |
| Heavy Veh.(HV)    | 1.3                   | 1.3     |  |  |  |
| Motorcycle(MC)    | 0.2                   | 0.4     |  |  |  |

#### c. Basic model

The amounts of traffic that can pass through a signal controlled intersection from a given approach depends on the green time available to the traffic and on the maximum flow of vehicles pass the stop line during the green period. When the signal changes to green vehicles take some second to start and accelerate to normal speed. After a few second the queue discharges at constant rate called **saturation flow (S)**.

The saturation flow is the flow, which would be obtained if there was a continuous queue of vehicles and they were passed at green time, or the saturation flow is the maximum departure rate, which can be achieved when there is a queue. The saturation flow is generally expressed in vehicles per hour green time. **Figure2.1** could be seen that the average rate of flow is lower during few minutes because vehicles are accelerating to normal running speed. The capacity (C) of an approach to a signalized intersection can be expressed as follows:

$$\mathbf{C} = \mathbf{S} \mathbf{x} \mathbf{g}/\mathbf{c} \tag{1}$$

Where:

C = Capacity (pcu/h)

- S = Saturation flow, i.e. mean discharge rate from a queue in the approach during green signal (pcu/hg = pcu per hour of green)
- g = Displayed Green Time
- c = Cycle time, i.e. duration of a complete sequence of signal changes(i.e. between two consecutive starts of green in the phase).



Figure 2.1 Basic model for saturation flow

#### **Purpose of the Intergreen Period**

- Warn discharging traffic that the phase is terminated. → Amber Period (for urban traffic signal in Indonesia is normally 3,0 sec).
- Certify that the last vehicle in the green phase which is being terminated receives adequate time to evacuate the conflict zone before the first advancing vehicle in the next phase enters the same area. → All-Red Period.

#### **All-Red Periods**

When there are no vehicles at an intersection, the controller can be programmed for "red rest" operation, displaying the red indication to all approaches. The controller will provide an immediate green indication to the first phase where vehicle demand is sensed. After the demand is serviced, and assuming no other demand occurs, the intersection will return to red indications on all approaches.

Red revert timing is used with red rest to ensure that unreasonably short red intervals do not occur. Without some amount of red revert timing (usually between 2 and 6 seconds), the green indication could very quickly, and unexpectedly, return to a phase that had just turned red. This might surprise a driver since, once a signal turns red, most drivers expect to wait a certain amount of time before receiving the green again. The saturation flow (S) can be expressed as a product between a base saturation flow (So) for a set of standard conditions, and adjustment factors (F) for deviation of the actual conditions from a set of pre-determined (ideal) conditions.

$$\mathbf{S} = \mathbf{S}_{\mathbf{Q}} \mathbf{x} \mathbf{F}_{\mathbf{CS}} \mathbf{x} \mathbf{F}_{\mathbf{SP}} \mathbf{x} \mathbf{F}_{\mathbf{G}} \mathbf{x} \mathbf{F}_{\mathbf{P}} \mathbf{x} \mathbf{F}_{\mathbf{RT}} \mathbf{x} \mathbf{F}_{\mathbf{LT}} \quad \text{pcu / hg}$$
(2)

Where:

- S = Saturation flow.
- So = Base saturation flow.
- F = Adjustment factors can be expressed as follows:

## The City size correction factor $F_{CS}$

| City population (M. inhabitants) | City size correction factor $F_{CS}$ |
|----------------------------------|--------------------------------------|
| > 3.0                            | 1.05                                 |
| 1.0-3.0                          | 1.00                                 |
| 0.3- 1.0                         | 0.94                                 |
| < 0.3                            | 0.83                                 |

Table 2:1 City size correction factor  $F_{CS}$ 

## The Side friction correction factor F SF

| Table | 2:2 | Adjustment | factor .f | for R | oad env | rironment | type | and | Side | fricti | on |
|-------|-----|------------|-----------|-------|---------|-----------|------|-----|------|--------|----|
|-------|-----|------------|-----------|-------|---------|-----------|------|-----|------|--------|----|

| Road        | Side friction | Phase type           | Ratio of unmotorised vehicles |              |              |              |              |              |  |
|-------------|---------------|----------------------|-------------------------------|--------------|--------------|--------------|--------------|--------------|--|
| environment | Side metion   | i nuse type          | 0.0                           | 0.05         | 0.10         | 0.15         | 0.20         | 0.25         |  |
| Commercial  | High          | Opposed<br>Protected | 0.93<br>0.93                  | 0.88<br>0.91 | 0.84<br>0.88 | 0.79<br>0.87 | 0.74<br>0.85 | 0.70<br>0.81 |  |

| Road        | Side friction         | Dhasa typa  | Ratio of unmotorised vehicles |      |      |      |      |      |  |
|-------------|-----------------------|-------------|-------------------------------|------|------|------|------|------|--|
| environment | Side metion           | I hase type | 0.0                           | 0.05 | 0.10 | 0.15 | 0.20 | 0.25 |  |
|             | Madium                | Opposed     | 0.94                          | 0.89 | 0.85 | 0.80 | 0.75 | 0.71 |  |
|             | Medium                | Protected   | 0.94                          | 0.92 | 0.89 | 0.88 | 0.86 | 0.82 |  |
|             | Ŧ                     | Opposed     | 0.95                          | 0.90 | 0.86 | 0.81 | 0.76 | 0.72 |  |
|             | Low                   | Protected   | 0.95                          | 0.93 | 0.90 | 0.89 | 0.87 | 0.72 |  |
|             |                       |             |                               |      |      |      |      | 0.83 |  |
|             | High<br>Medium<br>Low | Opposed     | 0.96                          | 0.91 | 0.86 | 0.81 | 0.78 | 0.72 |  |
|             |                       | Protected   | 0.96                          | 0.94 | 0.92 | 0.89 | 0.86 | 0.84 |  |
|             |                       | Opposed     | 0.97                          | 0.92 | 0.87 | 0.82 | 0.79 | 0.73 |  |
| Residential |                       | Protected   | 0.97                          | 0.95 | 0.93 | 0.90 | 0.87 | 0.85 |  |
|             |                       | Opposed     | 0.98                          | 0.93 | 0.88 | 0.83 | 0.80 | 0.74 |  |
|             |                       | Protected   | 0.98                          | 0.96 | 0.94 | 0.91 | 0.80 | 0.86 |  |
| Restricted  |                       | 0           | 1.00                          | 0.05 | 0.00 | 0.95 | 0.90 | 0.75 |  |
| Ac-cess(RA) | High/Medium/Low       | Opposed     | 1.00                          | 0.95 | 0.90 | 0.85 | 0.80 | 0.75 |  |
|             | _                     | Protected   | 1.00                          | 0.98 | 0.95 | 0.93 | 0.90 | 0.88 |  |
|             |                       |             |                               |      |      |      |      |      |  |

The Gradient correction factor  $F_{G}$ 



Figure 2:2 Correction factor for gradient  $F_{G}$ 

# The Right Turn correction factor FRT



Figure 2:3 Correction factor for right turns FRT. (o n l y applicable for

approach type P, two-way streets)

The Left turn correction factorFLT



Figure 2:4 Correction factorfor effect of left turn FLT

For protected approaches P (protected discharge) the base saturation flows So is determined as a function of the effective approach width (We):



So = 600 x We pcu/hg, (see Figure 2.5)

Figure 2.5 Base saturation flow for approach type P

For approach type 0 (opposed discharge),  $S_0$  is determined from Figure 2:6 (for approaches without separate left-turning lanes), and from Figure 2:7 (for approaches with separate left-turning lane) as a function of  $W_e$  QLT and QLTO



Figure 2:6 So for approaches type O without separate Left-turninglane



Figure 2.7 So for approach type O with separate Left-turning lane.

## d. Signal Timing

Signal Timing the signal timing for fixed-time control conditions is determined based on the Webster (1966) method for minimization of overall vehicle delay in the intersection. First the cycle time (c) is determined, and after that the length of green (g) in each phase (i).

$$c = (1,5 \text{ x LTI} + 5) / (1 - FRcrit)$$
 (4)

Where:

| c      | = | Signal cycle time (Sec)   |
|--------|---|---|
| LTI    | = | Lost time per cycle (Sec)   |
| FR     | = | Flow divided by saturation flow (Q/S)                               |
| FRcrit | = | The highest value of FR in all approaches being discharged in a     |
|        |   | signal phase  |
| FRcrit | = | Intersection flow ratio = sum of FRcrit for all phases in the cycle |

If the cycle time is shorter than this value there is a serious risk for over saturation of the intersection. Too long cycle time results in increased average delay of the traffic. If FRcrit is close to or greater than 1, the intersection is oversaturated and the formula will result in very high or negative cycle time values.

 $g = (c - LTI) \times FRcrit / (FRcrit)$ (5) Where:

g = Displayed green time in phase I (Sec)

The performance of a signalized intersection is generally much more sensitive to errors in the green time distribution than to a too long cycle time. Even a small deviation from the green ratio (g/c) determined from equation (4) and (5) above result in high increase of the average delay in the intersection.

#### e. Capacity and degree of saturation

The approach capacity (C) is obtained by multiplication of the saturation flow with the green ratio (g/c) for each approach; see equation (1) above. The degree of saturation (DS) is obtained as:

$$DS = Q/C = (Q x c) / (S x g)$$
 (6)

#### f.Traffic performance

Different measures of traffic performance can be determined based on the traffic flow (Q), degree of saturation (DS) and signal timing (c and g) as described below:

#### **Queue Length**

The average number of queuing puck at the beginning of green NQ is calculated as the number of pcu remain from the previous green phase NQ1 plus the number of pcu that arrive during the red phase (NQ2):

$$NQ = NQ1 + NQ2 \tag{7}$$

With

NQ1 = 0.25 x C x 
$$\left[ (DS-1) + \sqrt{((DS-1)2 + ((8x (DS-0.5))/C))} \right]$$
 (8)

If DS > 0.5, otherwise NQ 1 = 0

$$NQ2 = c \times \frac{1 - GR}{1 - GR \times DS} * \frac{Q}{3600}$$
(9)

Where:

- NQ1 = number of pcu that remain from the previous green phase
- NQ2 = number of pcu that arrive during the red phase
- DS = degree of saturation
- GR = green ratio
- = cycle time с
- С = capacity (pcu/h) = saturation flow times the green ratio (S x GR)
- Q = traffic flow in the approach (pcu/h).

For design purposes the manual includes provision for adjustment of this average value to a desired level of probability for overloading.

The resulting queue length QL is obtained by multiplication of NQ with the average area occupied per pcu (20 sqm) and division with the entry width.

7

$$QL = c x \frac{NQ_{MAX} x 20}{w_{ENTRY}}$$
(10)

Where:

NQ max = maximum number of queuing

Use Figure 2.5 below to adjust NQ with regard to the desired probability for overloading POL(%)



Figure 2.8 Calculation of no. of queuing pcu NQmax

#### **Stop Rate**

The stop rate (NS), i.e. the average number of stops per vehicle (including multiple stop in aqueue) before passing the intersection, is calculated as

$$NS = 0.9 * \frac{NQ}{Q * c} * 3600$$
(11)

Where: c is the cycle time (Sec)

Q the traffic flow (pcu/h) in the studied approach.

#### Number of stopped vehicles Nsv

$$Nsv = Q \times NS (pcu/h)$$
(12)

The proportion of stopped vehicles psv, i.e. the ratio of ratio of vehicles that have to stop because of the red signal before the intersection, is calculated as

$$psv = min (NS, 1)$$

Where: NS is the stop rate in the approach.

#### Delay

Delay D at an intersection can occur for two reasons:

- a. Traffic Delay (DT) due to traffic intersection with other movement in the junction
- **b.** Geometric Delay (DG) due to deceleration and acceleration when making a turn in the intersection and/or when being stopped by the red light.

The average delay for an approach j is calculated as:

$$Dj = DTj + DGj$$
(13)

Where:

Dj = Mean delay for approach j (sec/pcu)

DTj = Mean traffic delay for approach j (sec/pcu)

DGj = Mean geometric delay for approach j (sec/pcu)

The average traffic delay for an approach j can be determined from the following formula (based on Akcelik, 1988).

$$DT = c * A + \frac{NQ1*3600}{C}$$
(14)

Where:

DT = Mean traffic delay for approach j (sec/pcu)

c = Adjusted cycle time(sec)

$$A = \frac{0.5 * (1 - GR)^2}{(1 - GR X DS)}$$

GR = Green ratio (g/c)

- DS = Degree of Saturation
- NQ1 = Number of pcu that remain from the previous green phase
- C = Capacity (pcu/h)

Observe that the calculation result are not valid if the capacity of the intersection is influenced by "external" factors such as blocking of an exit due to downstream congestion, manual police control etc.

#### **Average Geometric Delay**

The average geometric delay for an approach j can be estimated as follows:

$$DGj = (1 - psv) x pt x 6 + (psv x 4)$$
 (15)

Where:

DGj = Mean geometric delay for approach j (sec/pcu)

psv = Proportion of stopped vehicle in the approach

pt = Proportion of turning vehicle in the approach

## CHAPTER 3 METHODOLOGY

#### 3.1 Study Outline

Figure 3.1 presents the flow chart of an overview of the study. The objective of this research is to improve transportation planning level techniques for the assessment of the traffic signal coordination system on congestion. Specifically, This study aimed to analyze traffic flow system in a study area location to get green that optimized signal timing in that network. Study scope cover survey implementation traffic such as volume calculation saturated flow road and rate have been classified in peak hour.



Fiugre 3.1 Flow Chart for The Study

#### 3.2 Selection Of Location:

Benghazi City contains a lot of Beaches monuments and places. In the holiday times the roads are in the city because a lot of people come to spend the holiday in Benghazi. And especially the city is costal, tourist city and also close to the Seaport. This study requires area where there are straight path with successive nodes. So the selection of the study area is based on the following criteria:

i. Roads with a variation of traffic volume.

- ii. Good access and safety for the enumerators and equipment during the data collection process.
- iii. Good overhead vantage points for video recording purposes.



Figure.3-2 Alselmani intersection in Benghazi city

#### 3.3 Data Collection

#### **3.3.1 Data Collection Equipment and Method:**

For data collection at signalized intersections we need two cameras and trumpeter that Record data simultaneously but because of there was not enough equipment we decided to collect data in different time but with consideration almost situation in time and place of installing cameras. So the peak hour traffic flow in intersection morning peak , noon off peak hour and afternoon peak hour recorded. The location of the cameras was influenced by logistics such as visibility, building, etc. During the survey below data was collected for the video recording method, the video camera was set up at each junction and intersections at a distance of approximately 1.8 meters above the ground level over-looking the intersection. An external time device was attached to the camera to provide a permanent record. Efforts were made to position the camera so that all the vehicles on the observed roadways could be observed. However, this was a compromise between satisfying this requirement and the camera resolution

#### **3.3.2 Data collection time:**

The times for data collection during the morning peak , off peak hours and afternoon peak hours. Data were collected during weekday's periods in the evening at peak and Off peak hours. Field research was at one day starting in early 8 December 2012 Saturday in morning the period of time between the hours of 7:00 am to 8:30 am, afternoon in the time period between 13:30 pm to15: 00 pm , evening in the time period between 14:15 pm to 17:45 pm.

#### 3.4 Problem Identification

Problems at an intersection are identified through a survey at congested signalized intersections, field investigations, and preliminary operational and safety analysis. To determine whether a problem exists, this information needs to be evaluated against defined goals or standards. A problem statement can be defined after a review of the established operational and safety criteria against the known characteristics of an intersection. In some cases, additional data may need to be collected to confirm that a problem exists

#### 3.5 Data And Performance Analysis

Calculations in this study to evaluate the performance of signalized intersections are using the rules set by IHCM 1997. The existing data consist of geometric, traffic flow, side friction condition, the phase, green time. The result of calculation consists of capacity, degree of saturation, average no. of stops, mean average intersection delay and Almost all of the intersections show lower performance. Figure 3.3 below is a flow chart of procedures for calculating the performance analysis.



Figure 3.3 Flow chart of the performance analysis of signal intersections

# CHAPTER IV ANALYSIS OF DATA AND RESULTS

## 4.1 Data geometric conditions of roads and intersections.

Data geometric condition of roads and intersections were obtained by direct measurement of the standard geometric parameters of road and intersection segments of roads and intersections affected by traffic expected.

# Table 4.1:Geometry, traffic arrangements and environmental conditions for intersection

| City Size              | 1.008700 million |       |      |      |  |  |  |  |  |
|------------------------|------------------|-------|------|------|--|--|--|--|--|
| Approach Code          | North            | South | East | West |  |  |  |  |  |
| Median Y/N             | Y                | Y     | Y    | Y    |  |  |  |  |  |
| Side Friction          | L                | L     | L    | L    |  |  |  |  |  |
| Road<br>Environment    | COM              | RES   | СОМ  | СОМ  |  |  |  |  |  |
| Gradient %             | 0                | 0     | 0    | 0    |  |  |  |  |  |
| Approach WA<br>(m)     | 8                | 8     | 9    | 9    |  |  |  |  |  |
| Entry WEntry<br>(m)    | 5                | 5     | 6    | 6    |  |  |  |  |  |
| RT on Red<br>WRTOR (m) | 3                | 3     | 3    | 3    |  |  |  |  |  |
| Wexit (m)              | 5                | 5     | 5    | 5    |  |  |  |  |  |



Figure 4.1 Geometric Condition Of Alselmani Intersection (Two Phase)
#### 4.2 Data setting phase to the signalized intersections(existing condition).

Data on the phase settings for the traffic signalized intersection is obtained by direct measurement of the phase duration of traffic lights at the existing intersections.

| Approach | Pha    | ase time   | No of phases    | Cycle Time      |
|----------|--------|------------|-----------------|-----------------|
| Code     | Green  | Intergreen | itto. of phuses | Cycle Thire     |
| North    | 22     | 4          | Phase (1)       | 54              |
| South    | 22     | 4          | T hase (1)      | 54              |
| East     | 24     | 4          |                 | 54              |
| West     | 24     | 4          | Phase (2)       | 54              |
|          | 22sec+ | Phas<br>4  | e (1)<br>24 sec | 2+2 sec         |
|          | 22sec+ | 4          | 24 sec          | 2+2 sec<br>A AR |
|          |        | Phas       | e (2)           |                 |
|          | 22sec  | 2 Sec 2    | Sec 24 se       | c + 4           |
|          |        |            |                 |                 |
|          |        | A AR       |                 |                 |
|          |        |            |                 |                 |

Table 4.2: Phase time, green, and cycle time for intersection

| Data          |                  |       |  |  |  |
|---------------|------------------|-------|--|--|--|
| Cycle T       | ime (sec)        | 54    |  |  |  |
| Green         | Гime (N)         | 22    |  |  |  |
| Green         | Time (S)         | 22    |  |  |  |
| Green         | Гime (E)         | 24    |  |  |  |
| Green 7       | Time (W)         | 24    |  |  |  |
| Intergr       | een (sec)        | 4     |  |  |  |
| Queue L       | ength (m)        | 87    |  |  |  |
| Average.no of | f stop (sec/pcu) | 1.03  |  |  |  |
|               | Ν                | 41.06 |  |  |  |
| Average Delay | S                | 18.30 |  |  |  |
| Sec/pcu       | Ε                | 34.92 |  |  |  |
|               | W                | 22.47 |  |  |  |
|               | Ν                | 1.24  |  |  |  |
| Stop Rate     | S                | 0.78  |  |  |  |
| Stop/pcu      | Ε                | 1.14  |  |  |  |
|               | W                | 0.90  |  |  |  |
| Average Inte  | rsection delay   | 64.30 |  |  |  |
| (sec.         | (pcu)            | 0.025 |  |  |  |
| n.            | IN C             | 0.925 |  |  |  |
| Degree        | <u> </u>         | 0.66  |  |  |  |
| Saturation    | E                | 0.92  |  |  |  |
|               | W                | 0.81  |  |  |  |

#### Table 4.3 The Results of existing condition (2 Phase)

#### 4.3 Data of volume traffic flow for the intersections.

Data volume of traffic crossing the road or obtained by surveying the traffic counting on roads and intersections. The implementation of a traffic count survey conducted on Saturday 8 December 2012 in morning the period of time between the hours of 7:00 am to 8:30 am, afternoon in the time period between 13:30 pm to15: 00 pm , evening in the time period between 14:15 pm to 17:45 pm.

|            |      |        | Light    | Heavy     | Motorcycles |       |  |
|------------|------|--------|----------|-----------|-------------|-------|--|
| Time       | Dire | ection | Vehicles | Vehicle   | (MC)        | Total |  |
|            |      |        | (LV)     | (HV)      |             |       |  |
|            |      | LT     | 91       | 74        | 3           |       |  |
|            | Ν    | ST     | 461      | 64        | 3           |       |  |
|            |      | RT     | 131      | 52        | 0           |       |  |
|            |      | LT     | 79       | 74        | 6           |       |  |
|            | S    | ST     | 205      | 93        | 1           |       |  |
| 7.00 8.00  |      | RT     | 67       | 60        | 2           | 2577  |  |
| 7.00 -8.00 |      | LT     | 153      | 114       | 7           | 5577  |  |
|            | Е    | ST     | 408      | 173       | 4           |       |  |
|            |      | RT     | 174      | 117       | 3           |       |  |
|            |      | LT     | 110      | 66        | 9           |       |  |
|            | W    | ST     | 391      | 145       | 12          |       |  |
|            |      | RT     | 135      | 81        | 9           |       |  |
|            |      | LT     | 103      | 70        | 5           |       |  |
|            | Ν    | ST     | 456      | 77        | 4           | 3681  |  |
|            |      | RT     | 142      | 44        | 0           |       |  |
|            |      | LT     | 89       | 68        | 5           |       |  |
|            | S    | ST     | 225      | 102       | 4           |       |  |
| 7.15 0.15  |      | RT     | 85       | 59        | 3           |       |  |
| /:15 -8:15 |      | LT     | 168      | 120       | 8           |       |  |
|            | Е    | ST     | 422      | 147       | 7           |       |  |
|            |      | RT     | 191      | 99        | 4           |       |  |
|            |      | LT     | 133      | 70        | 11          | 1     |  |
|            | W    | ST     | 402      | 125       | 8           |       |  |
|            |      | RT     | 137      | 82        | 6           |       |  |
|            |      | LT     | 109      | 68        | 5           |       |  |
|            | Ν    | ST     | 465      | <b>78</b> | 3           |       |  |
|            |      | RT     | 140      | 47        | 3           |       |  |
|            |      | LT     | 104      | 62        | 4           |       |  |
|            | S    | ST     | 236      | <b>99</b> | 4           |       |  |
|            |      | RT     | 88       | 55        | 3           | 3700  |  |
| /:30 -8:30 |      | LT     | 164      | 113       | 5           | 5780  |  |
|            | Е    | ST     | 443      | 150       | 5           |       |  |
|            |      | RT     | 202      | <b>98</b> | 4           |       |  |
|            |      | LT     | 145      | 84        | 10          |       |  |
|            | W    | ST     | 413      | 132       | 6           |       |  |
|            |      | RT     | 137      | 90        | 6           |       |  |

Tables 4.4 The peak hours and off-peak hours Morning Period 7:00 – 8:30 Am

| Time          | Direction |    | Light<br>Vehicles | Heavy<br>Vehicle | Motorcycles<br>(MC) | Total |
|---------------|-----------|----|-------------------|------------------|---------------------|-------|
|               |           | 1  | (LV)              | (HV)             |                     |       |
|               |           | LT | 107               | 77               | 6                   |       |
|               | Ν         | ST | 331               | 88               | 4                   |       |
|               |           | RT | 129               | 86               | 3                   |       |
|               |           | LT | 107               | 74               | 4                   |       |
|               | S         | ST | 368               | 84               | 1                   |       |
| 12.20 14.20   |           | RT | 124               | 100              | 4                   | 3750  |
| 15.50 - 14.50 |           | LT | 134               | <b>89</b>        | 4                   | 3750  |
|               | E         | ST | 382               | 180              | 6                   |       |
|               |           | RT | 130               | 107              | 11                  |       |
|               |           | LT | 158               | 58               | 10                  |       |
|               | W         | ST | 412               | 133              | 3                   |       |
|               |           | RT | 136               | <b>95</b>        | 5                   |       |
|               |           | LT | 113               | 82               | 3                   |       |
|               | Ν         | ST | 349               | 89               | 1                   |       |
|               |           | RT | 117               | 95               | 2                   |       |
|               |           | LT | 109               | 70               | 5                   |       |
|               | S         | ST | 385               | 75               | 2                   |       |
| 12 45 14 45   |           | RT | 122               | 101              | 1                   | 2620  |
| 13:45 -14:45  |           | LT | 136               | 77               | 2                   | 3630  |
|               | Е         | ST | 351               | 170              | 4                   |       |
|               |           | RT | 139               | 102              | 10                  |       |
|               |           | LT | 133               | 45               | 11                  |       |
|               | W         | ST | 398               | 120              | 3                   |       |
|               |           | RT | 126               | 79               | 3                   |       |
|               |           | LT | 111               | 94               | 5                   |       |
|               | Ν         | ST | 343               | 92               | 1                   |       |
|               |           | RT | 110               | 103              | 0                   |       |
|               |           | LT | 105               | 70               | 4                   |       |
|               | S         | ST | 351               | 83               | 4                   |       |
|               |           | RT | 120               | 84               | 1                   | 2522  |
| 14:00 - 15:00 |           | LT | 130               | 74               | 1                   | 3532  |
|               | Е         | ST | 369               | 157              | 3                   |       |
|               |           | RT | 146               | 116              | 7                   |       |
|               |           | LT | 122               | 45               | 9                   |       |
|               | W         | ST | 369               | 105              | 3                   |       |
|               |           | RT | 110               | 82               | 3                   |       |

Afternoon Period 13:30 – 15:00 Pm

| Time        | Direction |          | Light<br>Vehicles<br>(LV) | Heavy<br>Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|-------------|-----------|----------|---------------------------|--------------------------|---------------------|-------|
|             | N         | LT<br>ST | 97<br>274                 | 63<br>69                 | 6<br>5              |       |
|             |           | RT       | 88                        | 82                       | 3                   |       |
|             |           | LT       | 79                        | 65                       | 6                   |       |
|             | S         | ST       | 237                       | 98                       | 3                   |       |
| 16.15 17.15 |           | RT       | 80                        | 65                       | 2                   | 2742  |
| 10.13-17.13 |           | LT       | 80                        | 70                       | 6                   | 2742  |
|             | E         | ST       | 159                       | 63                       | 6                   |       |
|             |           | RT       | 105                       | 68                       | 6                   |       |
|             |           | LT       | 115                       | 56                       | 9                   |       |
|             | W         | ST       | 267                       | 126                      | 8                   |       |
|             |           | RT       | 145                       | 71                       | 10                  |       |
|             |           | LT       | 116                       | 70                       | 4                   |       |
|             | Ν         | ST       | 284                       | 74                       | 4                   | 2763  |
|             |           | RT       | 101                       | 82                       | 3                   |       |
|             |           | LT       | <b>89</b>                 | 67                       | 5                   |       |
|             | S         | ST       | 215                       | 97                       | 4                   |       |
| 16:30-17:30 |           | RT       | 88                        | 64                       | 3                   |       |
|             |           | LT       | 96                        | 82                       | 7                   |       |
|             | E         | ST       | 186                       | <b>79</b>                | 7                   |       |
|             |           | RT       | 127                       | 68                       | 7                   | l     |
|             |           | LT       | 106                       | 60                       | 11                  |       |
|             | W         | ST       | 228                       | 116                      | 7                   |       |
|             |           | RT       | 137                       | 62                       | 7                   |       |
|             |           | LT       | 104                       | 63                       | 6                   |       |
|             | Ν         | ST       | 248                       | 67                       | 4                   |       |
|             |           | RT       | 94                        | 78                       | 3                   |       |
|             |           | LT       | 104                       | 64                       | 4                   |       |
|             | S         | ST       | 165                       | 89                       | 4                   |       |
| 16.45 17.45 |           | RT       | 81                        | 55                       | 3                   | 2520  |
| 10:43-17:45 |           | LT       | 119                       | 91                       | 5                   | 2530  |
|             | Е         | ST       | 185                       | 92                       | 5                   |       |
|             |           | RT       | 145                       | 77                       | 7                   |       |
|             |           | LT       | 70                        | 56                       | 10                  |       |
|             | W         | ST       | 168                       | 86                       | 4                   |       |
|             |           | RT       | 117                       | 50                       | 7                   |       |

Evening Period : 16:15 – 17:45 Pm

Due to the similarity of data traffic volume were taken in the morning peak hour, and then multiply the volume of traffic into (0.75, 0.50, 0.25) to get a low traffic volume.

### 4.4 The Calculation Of Morning Peak Hour( 7:30 – 8:30)

- Phase time Cycle Time Approach Code No. of phases Green Intergreen 4 79 North 34 phase 1 34 79 South 4 79 East 37 4 Phase 2 79 West 37 4 Phase (1) 34Sec+4 37 Sec 2Sec 2 Sec A AR Phase (2) 34Sec 2Sec 2Sec 37 Sec + 4 AR А
- a. Very High Traffic Flow

| b. | High Traffic H | Flow (traffic | volume x 0.75) |
|----|----------------|---------------|----------------|
|----|----------------|---------------|----------------|



| c. | Low Traffic Flow | (traffic volume x 0,50) |
|----|------------------|-------------------------|
|----|------------------|-------------------------|





d. Very Low Traffic Flow (traffic volume x 0.25)

### Note:

The minimum green time based on (IHCM 1997) is 7 Sec so the cycle time for very low traffic flow become as:

| Approach Code | Pha   | ase time   | No. of phasos  | Cycle Time |
|---------------|-------|------------|----------------|------------|
| Approach Coue | Green | Intergreen | 110. of phases | Cycle Time |
| North         | 7     | 4          | nhasa 1        | 22         |
| South         | 7     | 4          | phase 1        | 22         |
| East          | 7     | 4          | Phase 2        | 22         |
| West          | 7     | 4          |                | 22         |
|               |       | Phase      | (1)            |            |
| 7Sec          | +4    |            | <b>7 Sec</b>   | 2Sec 2Sec  |
|               |       |            |                |            |
|               |       |            |                | A AR       |
|               |       |            |                |            |
|               |       | Phase      | (2)            |            |
|               |       | i nase     | (=)            |            |
| 78            | ec    | 2Sec 2Sec  | 7 Sec +        | - 4        |
|               |       |            |                |            |
|               |       | A AR       |                |            |
|               |       |            |                |            |
|               |       |            |                |            |

| Data                            |            |           | Traffi | c Condition | 1           |      |
|---------------------------------|------------|-----------|--------|-------------|-------------|------|
|                                 |            | Very High | High   | Low         | Very<br>Low |      |
| Cycle Time (sec)                |            | 79        | 38     | 27          | 20          | 22   |
| Green Time (N,                  | <b>S</b> ) | 34        | 14     | 9           | 6(min 7)    | 7    |
| Green Time (E,                  | W)         | 37        | 16     | 10          | 6(min 7)    | 7    |
| Intergreen (se                  | c)         | 4         | 4      | 4           | 4           | 4    |
| Queue Length (                  | <b>m</b> ) | 108       | 42     | 20          | 11          | 11   |
| Average.no of stop<br>(sec/pcu) |            | 0.81      | 0.81   | 0.68        | 0.68        | 0.68 |
|                                 | Ν          | 36.1      | 17.1   | 9.75        | 8.42        | 8.60 |
| Average Delay                   | S          | 22.5      | 12.45  | 9.32        | 8.31        | 8.50 |
| Sec/pcu                         | E          | 32.1      | 14.67  | 9.32        | 8.53        | 8.70 |
|                                 | W          | 25.12     | 14.73  | 9.1         | 8.46        | 8.60 |
|                                 | Ν          | 0.96      | 0.88   | 0.70        | 0.68        | 0.66 |
| Stop Rate                       | S          | 0.72      | 0.70   | 0.66        | 0.66        | 0.65 |
| Stop/pcu                        | Ε          | 0.92      | 0.81   | 0.68        | 0.68        | 0.68 |
|                                 | W          | 0.80      | 0.8    | 0.66        | 0.68        | 0.66 |
| Average Intersec                | tion       |           |        |             |             |      |
| delay                           |            | 29.47     | 14.89  | 9.4         | 8.45        | 8.61 |
| (sec/pcu)                       |            |           |        |             |             |      |
|                                 | Ν          | 0.87      | 0.71   | 0.46        | 0.25        | 0.23 |
| Degree                          | S          | 0.68      | 0.50   | 0.32        | 0.17        | 0.16 |
| Saturation                      | Ε          | 0.87      | 0.69   | 0.46        | 0.26        | 0.25 |
|                                 | W          | 0.77      | 0.67   | 0.42        | 0.24        | 0.23 |

 Table 4.5:
 The Results of Intersection (2 Phase)

#### **Changed signal phasing**

An alternative phasing scheme with separate phase for left-turning traffic might be appropriate. Introduction of separate phases for left- turning traffic may have to accompanied with widening measures as well.

Geometric Condition Of Alselmani Intersection (Four Phase type 1)



Figure 4.2 Geometric Condition Of Alselmani Intersection (Four Phase)

#### The Sequence Diagram For Four Phase



## 1. Very High Trffic Flow

#### 3. Low Trffic Flow



#### Table 4.6 The Results of Intersection (4 Phase)

#### Type(1)

| Data                            |            | Traffic Condition |       |       |               |       |  |  |
|---------------------------------|------------|-------------------|-------|-------|---------------|-------|--|--|
|                                 |            | Very High         | High  | Low   | Very Low      |       |  |  |
| Cycle Time (sec)                |            | 153               | 77    | 51    | 36            | 44    |  |  |
| Green Time (N                   | <b>V</b> ) | 35                | 16    | 9     | 5(min=7)      | 7     |  |  |
| Green Time (S                   | 5)         | 25                | 11    | 7     | $4(\min = 7)$ | 7     |  |  |
| Green Time (I                   | E)         | 41                | 18    | 10    | 6(min=7)      | 7     |  |  |
| Green Time (V                   | V)         | 35                | 16    | 9     | 5(min=7)      | 7     |  |  |
| Intergreen (se                  | c)         | 4                 | 4     | 4     | 4             | 4     |  |  |
| Queue Length (                  | m)         | 173               | 67    | 31    | 16            | 17    |  |  |
| Average.no of stop<br>(sec/pcu) |            | 0.95              | 0.93  | 0.86  | 0.81          | 0.81  |  |  |
|                                 | Ν          | 73.29             | 38.62 | 23.96 | 17.61         | 19.88 |  |  |
| Average Delay                   | S          | 85.5              | 43.91 | 24.91 | 18.35         | 19.59 |  |  |
| Sec/pcu                         | Ε          | 66.96             | 37.30 | 23.82 | 16.59         | 20.07 |  |  |
|                                 | W          | 61.52             | 36.34 | 24.00 | 17.63         | 19.84 |  |  |
|                                 | Ν          | 0.96              | 0.94  | 0.86  | 0.82          | 0.80  |  |  |
| Stop Rate                       | S          | 1.00              | 0.98  | 0.87  | 0.83          | 0.79  |  |  |
| Stop/pcu                        | Ε          | 0.93              | 0.91  | 0.87  | 0.79          | 0.81  |  |  |
|                                 | W          | 0.93              | 0.91  | 0.86  | 0.82          | 0.79  |  |  |
| Average Intersec                | tion       |                   |       |       |               |       |  |  |
| delay                           |            | 70.25             | 38.52 | 24.10 | 17.42         | 19.88 |  |  |
| (sec/pcu)                       |            |                   |       |       |               |       |  |  |
|                                 | Ν          | 0.90              | 0.77  | 0.60  | 0.38          | 0.33  |  |  |
| Degree                          | S          | 0.91              | 0.80  | 0.56  | 0.34          | 0.24  |  |  |
| Saturation                      | E          | 0.90              | 0.80  | 0.64  | 0.31          | 0.38  |  |  |
|                                 | W          | 0.91              | 0.77  | 0.61  | 0.38          | 0.33  |  |  |

#### Comment:

Form the results that the Intersection Flow Ratio IFR = 0.808, leading

to a calculated cycle time for minimum delay of 153 sec. The existing timing can therefore be expected to lead to long queues. finally the level of performance with the new signal timing. As can be seen, the intersection is still heavily congested with queue-lengths in the order of 173 m, average proportion of stopped vehicles 0.93, and average delay 70.25 sec.

Geometric Condition Of Alselmani Intersection (Four Phase type 2)



## Figure 4.3 Geometric Condition Of Alselmani Intersection (Four Phase)

## Table 4.7 The Results of Intersection ( 4 Phase)

### Type(2)

| Data                                   |              | Traffic Condition |       |       |          |  |  |
|--|--------------|-------------------|-------|-------|----------|--|--|
| Data                                   |              | Very High         | High  | Low   | Very Low |  |  |
| Cycle Time (se                         | ec)          | 175               | 78    | 53    | 45       |  |  |
| Green Time (N                          | <b>V</b> )   | 51                | 20    | 11    | 7        |  |  |
| Green Time (S                          | 5)           | 22                | 9     | 7     | 7        |  |  |
| Green Time (I                          | E)           | 57                | 22    | 12    | 8        |  |  |
| Green Time (V                          | <b>V</b> )   | 29                | 11    | 7     | 7        |  |  |
| Intergreen (se                         | c)           | 4                 | 4     | 4     | 4        |  |  |
| Queue Length (                         | ( <b>m</b> ) | 264               | 87    | 44    | 23       |  |  |
| Average.no of s<br>(sec/pcu)           | top          | 0.95              | 0.92  | 0.85  | 0.85     |  |  |
|  | Ν            | 135.35            | 53.90 | 24.93 | 19.76    |  |  |
| Average Delay                          | S            | 106.85            | 47.03 | 24.7  | 20.67    |  |  |
| Sec/pcu                                | Ε            | 118.65            | 56.09 | 28.02 | 19.97    |  |  |
|  | W            | 85.38             | 42.85 | 24.94 | 19.81    |  |  |
|  | Ν            | 1.20              | 1.12  | 0.88  | 0.81     |  |  |
| Stop Rate                              | S            | 1.05              | 1.03  | 0.886 | 0.79     |  |  |
| Stop/pcu                               | Ε            | 1.12              | 1.15  | 0.92  | 0.80     |  |  |
|  | W            | 0.94              | 0.98  | 0.83  | 0.79     |  |  |
| Average Intersec<br>delay<br>(sec/pcu) | tion         | 81                | 37.46 | 24.2  | 19.2     |  |  |
|  | Ν            | 0.91              | 0.78  | 0.64  | 0.43     |  |  |
| Degree                                 | S            | 0.83              | 0.68  | 0.43  | 0.28     |  |  |
| Saturation                             | Ε            | 0.925             | 0.81  | 0.67  | 0.42     |  |  |
|  | W            | 0.81              | 0.70  | 0.58  | 0.37     |  |  |

#### **Comments:**

The control was changed from two-phase to four-phase control during , leading to excessive queuing in the area. The calculations for four phase control shows the reason why, the Intersection flow ratio increases , and the degree of saturation becomes higher in all approaches during the studied peak hour. The reason to change from two-phase to four-phase control was probably that the there were many traffic accidents in the intersection. An alternative action would have been to increase the inter-green periods between the phases, and to keep two-phase control which obviously results in a much higher intersection capacity and better level of performance level.

The advantage of changed to four phase: inevitably leads to an increase of the cycle time and of the ratio of time allocated to switching between phases (Intergreen). Although this may be beneficial from the traffic safety point of view, it normally means that the overall capacity of the intersection is decreased.

# CHAPTER V CONCLUSION AND RECOMMENDATIONS

#### 5.1 Conclusion

All of the data inserted and analyzed by using IHCM. The result of calculation consists of a number of phases, cycle length, green time, average intersection delay and average no. of stops. The intersections show the low performance in existing data case by the highest numbers in average intersection delay and average no. of stops.

The performance of the intersections will be expected to perform better by changing the phases from two phase to four phase which were calculated using IHCM for Alselmani intersection, so the change from two phase control to four phase control gave an increase of the cycle time and of the ratio of time allocated to switching between phases (Intergreen). Although this may be beneficial from the traffic safety point of view, it normally means that the overall capacity of the intersection is decreased.

#### 5.2 Suggestion And Recommendation

- a. Implementation of traffic management such as improved geometric (without widening the means) and movement arrangements need to be done because it will provide significant performance improvements at the intersection signalized intersection and intersection-existing
- b. It is recommended the study area is extended to conclude for more intersections and network in order to observe the role of a coordination system for traffic performance on network to avoid the many problems such as congestion.
- c. The last recommendation is to change from private transportation to public transportation to get rid of congestion and blocking traffic on the roads.

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## APPENDIX A

### This appendix includes the Survey traffic data flow at the Intersection

### 1. North

## a. Morning period

| Time        | Direction | Light<br>Vehicles<br>(LV) | Heavy<br>Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|-------------|-----------|---------------------------|--------------------------|---------------------|-------|
|             | LT        | 18                        | 20                       | 0                   | 38    |
| 7:00 -7:15  | ST        | 112                       | 11                       | 1                   | 124   |
|             | RT        | 32                        | 19                       | 0                   | 51    |
|             | LT        | 21                        | 12                       | 2                   | 35    |
| 7:15 -7:30  | ST        | 119                       | 19                       | 2                   | 140   |
|             | RT        | 29                        | 10                       | 0                   | 39    |
|             | LT        | 26                        | 22                       | 1                   | 49    |
| 7:30 -7:45  | ST        | 104                       | 15                       | 0                   | 119   |
|             | RT        | 31                        | 15                       | 0                   | 46    |
|             | LT        | 26                        | 20                       | 1                   | 47    |
| 7:45 -8:00  | ST        | 126                       | 19                       | 0                   | 145   |
|             | RT        | 39                        | 8                        | 0                   | 47    |
|             | LT        | 30                        | 16                       | 1                   | 47    |
| 8:00 - 8:15 | ST        | 116                       | 24                       | 2                   | 142   |
|             | RT        | 43                        | 11                       | 0                   | 54    |
|             | LT        | 27                        | 10                       | 1                   | 38    |
| 8:15 -8:30  | ST        | 119                       | 20                       | 1                   | 140   |
|             | RT        | 27                        | 13                       | 3                   | 43    |

### b. Afternoon period

| Time          | Direction | Light<br>Vehicles<br>(LV) | Heavy<br>Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|---------------|-----------|---------------------------|--------------------------|---------------------|-------|
|               | LT        | 24                        | 12                       | 3                   | 39    |
| 13:30 - 13:45 | ST        | 80                        | 16                       | 3                   | 99    |
|               | RT        | 39                        | 20                       | 1                   | 60    |
|               | LT        | 26                        | 17                       | 0                   | 43    |
| 13:45 -14:00  | ST        | 95                        | 21                       | 0                   | 116   |
|               | RT        | 31                        | 17                       | 0                   | 48    |
|               | LT        | 34                        | 20                       | 2                   | 56    |
| 14:00 - 14:15 | ST        | 83                        | 20                       | 0                   | 103   |
|               | RT        | 32                        | 26                       | 0                   | 58    |
|               | LT        | 23                        | 28                       | 1                   | 52    |
| 14:15 -14:30  | ST        | 73                        | 31                       | 1                   | 105   |
|               | RT        | 27                        | 23                       | 2                   | 52    |
|               | LT        | 30                        | 17                       | 0                   | 47    |
| 14:30 -14:45  | ST        | 98                        | 17                       | 0                   | 115   |
|               | RT        | 27                        | 29                       | 0                   | 56    |
|               | LT        | 24                        | 29                       | 2                   | 55    |
| 14:45-15:00   | ST        | 89                        | 24                       | 0                   | 116   |
|               | RT        | 24                        | 25                       | 0                   | 49    |

### **Evening Period**

| Time          | Direction | Light<br>Vehicles<br>(LV) | Heavy<br>Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|---------------|-----------|---------------------------|--------------------------|---------------------|-------|
|               | LT        | 14                        | 10                       | 3                   | 27    |
| 16:15 - 16:30 | ST        | 43                        | 12                       | 2                   | 57    |
|               | RT        | 14                        | 16                       | 1                   | 31    |
|               | LT        | 36                        | 16                       | 0                   | 52    |
| 16:30 -16:45  | ST        | 77                        | 21                       | 1                   | 99    |
|               | RT        | 31                        | 17                       | 0                   | 48    |
|               | LT        | 24                        | 20                       | 2                   | 46    |
| 16:45 - 17:00 | ST        | 92                        | 25                       | 1                   | 118   |
|               | RT        | 26                        | 26                       | 0                   | 52    |
|               | LT        | 23                        | 17                       | 1                   | 41    |
| 17:00 -17:15  | ST        | 62                        | 11                       | 1                   | 74    |
|               | RT        | 17                        | 23                       | 2                   | 42    |
|               | LT        | 33                        | 17                       | 1                   | 51    |
| 17:15 -17:30  | ST        | 53                        | 17                       | 1                   | 71    |
|               | RT        | 27                        | 16                       | 1                   | 44    |
|               | LT        | 24                        | 9                        | 2                   | 35    |
| 17:30- 17:45  | ST        | 41                        | 14                       | 1                   | 56    |
|               | RT        | 24                        | 13                       | 0                   | 37    |

#### 2. South

## a. Morning period

| Time        | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|-------------|-----------|------------------------|-----------------------|---------------------|-------|
|             | LT        | 15                     | 19                    | 2                   | 36    |
| 7:00 -7:15  | ST        | 42                     | 20                    | 0                   | 62    |
|             | RT        | 14                     | 13                    | 1                   | 28    |
|             | LT        | 19                     | 19                    | 1                   | 39    |
| 7:15 -7:30  | ST        | 50                     | 24                    | 0                   | 74    |
|             | RT        | 13                     | 16                    | 0                   | 29    |
|             | LT        | 19                     | 20                    | 3                   | 42    |
| 7:30 -7:45  | ST        | 52                     | 22                    | 1                   | 75    |
|             | RT        | 14                     | 15                    | 1                   | 30    |
|             | LT        | 26                     | 16                    | 0                   | 52    |
| 7:45 -8:00  | ST        | 61                     | 27                    | 2                   | 80    |
|             | RT        | 26                     | 16                    | 0                   | 42    |
|             | LT        | 25                     | 13                    | 1                   | 39    |
| 8:00 - 8:15 | ST        | 62                     | 29                    | 1                   | 92    |
|             | RT        | 32                     | 12                    | 2                   | 46    |
|             | LT        | 34                     | 13                    | 0                   | 47    |
| 8:15 -8:30  | ST        | 61                     | 21                    | 0                   | 82    |
|             | RT        | 16                     | 12                    | 0                   | 28    |

## b. Afternoon period

| Time          | Direction | Light Vehicles | Heavy Vehicle | Motorcycles | Total |
|---------------|-----------|----------------|---------------|-------------|-------|
| Time          | Direction | (LV)           | (HV)          | (MC)        | Total |
|               | LT        | 22             | 20            | 0           | 42    |
| 13:30 - 13:45 | ST        | 90             | 32            | 0           | 122   |
|               | RT        | 35             | 17            | 3           | 55    |
|               | LT        | 32             | 18            | 1           | 51    |
| 13:45 -14:00  | ST        | 106            | 15            | 0           | 121   |
|               | RT        | 35             | 34            | 0           | 69    |
|               | LT        | 25             | 18            | 2           | 45    |
| 14:00 - 14:15 | ST        | 89             | 15            | 1           | 105   |
|               | RT        | 22             | 34            | 1           | 57    |
|               | LT        | 28             | 18            | 1           | 47    |
| 14:15 -14:30  | ST        | 83             | 22            | 0           | 105   |
|               | RT        | 32             | 15            | 0           | 47    |
|               | LT        | 24             | 16            | 1           | 41    |
| 14:30 -14:45  | ST        | 107            | 23            | 1           | 131   |
|               | RT        | 33             | 18            | 0           | 51    |
|               | LT        | 28             | 18            | 0           | 46    |
| 14:45-15:00   | ST        | 72             | 23            | 2           | 97    |
|               | RT        | 33             | 17            | 0           | 50    |

## c. Evening Period

| Time         | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|--------------|-----------|------------------------|-----------------------|---------------------|-------|
|              | LT        | 15                     | 11                    | 2                   | 28    |
| 16:15 -16:30 | ST        | 52                     | 20                    | 0                   | 72    |
|              | RT        | 14                     | 13                    | 1                   | 28    |
|              | LT        | 19                     | 16                    | 1                   | 36    |
| 16:30 -16:45 | ST        | 71                     | 29                    | 0                   | 100   |
|              | RT        | 23                     | 21                    | 0                   | 44    |
|              | LT        | 19                     | 12                    | 3                   | 34    |
| 16:45 -17:00 | ST        | 53                     | 22                    | 1                   | 76    |
|              | RT        | 14                     | 15                    | 1                   | 30    |
|              | LT        | 26                     | 26                    | 0                   | 52    |
| 17:00 -17:15 | ST        | 61                     | 27                    | 2                   | 90    |
|              | RT        | 29                     | 16                    | 0                   | 45    |
|              | LT        | 25                     | 13                    | 1                   | 39    |
| 17:15 -17:30 | ST        | 30                     | 19                    | 1                   | 50    |
|              | RT        | 22                     | 12                    | 2                   | 36    |
|              | LT        | 34                     | 13                    | 0                   | 47    |
| 17:30 -17:45 | ST        | 21                     | 21                    | 0                   | 42    |
|              | RT        | 16                     | 12                    | 0                   | 28    |

#### 3. East:

### a. Morning period

| Time        | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|-------------|-----------|------------------------|-----------------------|---------------------|-------|
|             | LT        | 30                     | 21                    | 1                   | 52    |
| 7:00 -7:15  | ST        | 102                    | 60                    | 1                   | 163   |
|             | RT        | 29                     | 29                    | 0                   | 58    |
|             | LT        | 39                     | 25                    | 4                   | 68    |
| 7:15 -7:30  | ST        | 100                    | 35                    | 2                   | 137   |
|             | RT        | 32                     | 27                    | 0                   | 59    |
|             | LT        | 42                     | 36                    | 2                   | 80    |
| 7:30 -7:45  | ST        | 96                     | 39                    | 1                   | 136   |
|             | RT        | 52                     | 33                    | 1                   | 86    |
|             | LT        | 42                     | 32                    | 0                   | 74    |
| 7:45 -8:00  | ST        | 110                    | 39                    | 3                   | 152   |
|             | RT        | 61                     | 28                    | 2                   | 91    |
|             | LT        | 45                     | 27                    | 2                   | 74    |
| 8:00 - 8:15 | ST        | 116                    | 34                    | 1                   | 151   |
|             | RT        | 46                     | 11                    | 1                   | 58    |
|             | LT        | 35                     | 18                    | 1                   | 54    |
| 8:15 -8:30  | ST        | 121                    | 38                    | 0                   | 159   |
|             | RT        | 43                     | 26                    | 0                   | 69    |

## b. Afternoon period

| Time          | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|---------------|-----------|------------------------|-----------------------|---------------------|-------|
|               | LT        | 28                     | 30                    | 2                   | 60    |
| 13:30 - 13:45 | ST        | 119                    | 39                    | 2                   | 160   |
|               | RT        | 30                     | 32                    | 1                   | 63    |
|               | LT        | 42                     | 18                    | 1                   | 61    |
| 13:45 -14:00  | ST        | 89                     | 49                    | 1                   | 139   |
|               | RT        | 33                     | 26                    | 3                   | 62    |
|               | LT        | 25                     | 16                    | 0                   | 41    |
| 14:00 - 14:15 | ST        | 101                    | 52                    | 2                   | 155   |
|               | RT        | 30                     | 31                    | 4                   | 72    |
|               | LT        | 39                     | 25                    | 1                   | 65    |
| 14:15 -14:30  | ST        | 73                     | 40                    | 1                   | 114   |
|               | RT        | 37                     | 18                    | 3                   | 58    |
|               | LT        | 30                     | 18                    | 0                   | 48    |
| 14:30 -14:45  | ST        | 88                     | 29                    | 0                   | 117   |
|               | RT        | 39                     | 27                    | 0                   | 66    |
|               | LT        | 36                     | 15                    | 0                   | 51    |
| 14:45-15:00   | ST        | 107                    | 36                    | 0                   | 143   |
|               | RT        | 40                     | 40                    | 0                   | 80    |

### c. Evening Period

| Time         | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|--------------|-----------|------------------------|-----------------------|---------------------|-------|
|              | LT        | 19                     | 15                    | 1                   | 35    |
| 16:15 -16:30 | ST        | 30                     | 18                    | 0                   | 48    |
|              | RT        | 21                     | 11                    | 0                   | 32    |
|              | LT        | 17                     | 9                     | 3                   | 29    |
| 16:30 -16:45 | ST        | 47                     | 15                    | 2                   | 64    |
|              | RT        | 18                     | 17                    | 0                   | 35    |
|              | LT        | 22                     | 26                    | 2                   | 50    |
| 16:45 -17:00 | ST        | 36                     | 11                    | 1                   | 48    |
|              | RT        | 30                     | 22                    | 4                   | 56    |
|              | LT        | 22                     | 20                    | 0                   | 42    |
| 17:00 -17:15 | ST        | 46                     | 19                    | 3                   | 68    |
|              | RT        | 36                     | 18                    | 2                   | 56    |
|              | LT        | 35                     | 27                    | 2                   | 64    |
| 17:15 -17:30 | ST        | 57                     | 34                    | 1                   | 92    |
|              | RT        | 43                     | 11                    | 1                   | 55    |
|              | LT        | 40                     | 18                    | 1                   | 59    |
| 17:30 -17:45 | ST        | 46                     | 28                    | 0                   | 74    |
|              | RT        | 36                     | 26                    | 0                   | 62    |

### 4. West

### a. Morning period

| Time        | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|-------------|-----------|------------------------|-----------------------|---------------------|-------|
|             | LT        | 24                     | 10                    | 1                   | 35    |
| 7:00 -7:15  | ST        | 98                     | 49                    | 4                   | 151   |
|             | RT        | 26                     | 20                    | 3                   | 49    |
|             | LT        | 28                     | 13                    | 2                   | 43    |
| 7:15 -7:30  | ST        | 102                    | 30                    | 2                   | 134   |
|             | RT        | 39                     | 23                    | 2                   | 64    |
|             | LT        | 30                     | 13                    | 1                   | 44    |
| 7:30 -7:45  | ST        | 88                     | 30                    | 4                   | 122   |
|             | RT        | 46                     | 24                    | 2                   | 72    |
|             | LT        | 28                     | 30                    | 5                   | 63    |
| 7:45 -8:00  | ST        | 103                    | 36                    | 2                   | 141   |
|             | RT        | 24                     | 14                    | 2                   | 40    |
|             | LT        | 47                     | 14                    | 3                   | 64    |
| 8:00 - 8:15 | ST        | 109                    | 29                    | 0                   | 138   |
|             | RT        | 28                     | 21                    | 0                   | 49    |
|             | LT        | 40                     | 27                    | 1                   | 68    |
| 8:15 -8:30  | ST        | 113                    | 37                    | 0                   | 150   |
|             | RT        | 39                     | 31                    | 2                   | 72    |

### b. Afternoon period

| Time          | Direction | Light Vehicles<br>(LV) | Heavy Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|---------------|-----------|------------------------|-----------------------|---------------------|-------|
|               | LT        | 43                     | 24                    | 4                   | 71    |
| 13:30 - 13:45 | ST        | 92                     | 40                    | 2                   | 134   |
|               | RT        | 35                     | 35                    | 3                   | 73    |
|               | LT        | 40                     | 11                    | 3                   | 54    |
| 13:45 -14:00  | ST        | 129                    | 45                    | 0                   | 174   |
|               | RT        | 42                     | 22                    | 2                   | 68    |
|               | LT        | 45                     | 14                    | 1                   | 60    |
| 14:00 - 14:15 | ST        | 101                    | 35                    | 1                   | 137   |
|               | RT        | 32                     | 23                    | 0                   | 55    |
|               | LT        | 30                     | 9                     | 2                   | 41    |
| 14:15 -14:30  | ST        | 90                     | 13                    | 0                   | 103   |
|               | RT        | 27                     | 15                    | 0                   | 42    |
|               | LT        | 18                     | 11                    | 5                   | 34    |
| 14:30 -14:45  | ST        | 78                     | 27                    | 2                   | 107   |
|               | RT        | 25                     | 19                    | 1                   | 45    |
|               | LT        | 29                     | 11                    | 1                   | 41    |
| 14:45-15:00   | ST        | 100                    | 30                    | 0                   | 130   |
|               | RT        | 26                     | 25                    | 2                   | 53    |

## **Evening Period**

| Time         | Direction | Light<br>Vehicles<br>(LV) | Heavy<br>Vehicle<br>(HV) | Motorcycles<br>(MC) | Total |
|--------------|-----------|---------------------------|--------------------------|---------------------|-------|
|              | LT        | 26                        | 10                       | 1                   | 37    |
| 16:15 -16:30 | ST        | 68                        | 29                       | 1                   | 98    |
|              | RT        | 36                        | 20                       | 3                   | 59    |
|              | LT        | 48                        | 13                       | 2                   | 63    |
| 16:30 -16:45 | ST        | 85                        | 41                       | 3                   | 129   |
|              | RT        | 39                        | 23                       | 2                   | 64    |
|              | LT        | 30                        | 13                       | 1                   | 44    |
| 16:45 -17:00 | ST        | 68                        | 30                       | 2                   | 100   |
|              | RT        | 46                        | 14                       | 2                   | 62    |
|              | LT        | 11                        | 20                       | 5                   | 36    |
| 17:00 -17:15 | ST        | 46                        | 26                       | 2                   | 74    |
|              | RT        | 24                        | 14                       | 3                   | 41    |
|              | LT        | 17                        | 14                       | 3                   | 34    |
| 17:15 -17:30 | ST        | 29                        | 19                       | 0                   | 48    |
|              | RT        | 28                        | 11                       | 0                   | 39    |
|              | LT        | 12                        | 9                        | 1                   | 22    |
| 17:30 -17:45 | ST        | 25                        | 11                       | 0                   | 36    |
|              | RT        | 19                        | 11                       | 2                   | 32    |

#### APPENDIX B

#### Form USIG

This appendix includes the signalized calculation

|           |         |          |              | -         | TRAFFIC FL  | OW MOTO   | RISED VEH  | ICLES (MV)     |                 |                 |
|-----------|---------|----------|--------------|-----------|-------------|-----------|------------|----------------|-----------------|-----------------|
|           |         | Light Ve | hicles (LV)  | Heavy Ve  | hicles (HV) | Motorcy   | cles (MC)  | Total          | F               | Ratio           |
| Annr agda | Dir     | pce prot | tected = 1.0 | pce prote | ected = 1.3 | pce prote | cted = 0.2 | Motor vehicles |                 | of              |
| Appr code | Dir.    | pce opp  | osed = 1.0   | pce oppo  | osed = 1.3  | pce oppo  | sed = 0.4  | MV             | tu              | ırning          |
|           |         | veh/h    | pcu/h        | veh/h     | pcu/h       | veh/h     | pcu/h      | pcu/h          | р <sub>LT</sub> | р <sub>кт</sub> |
|           |         |          | Орр          |           | Орр         |           | Орр        | Орр            | Eq.(13)         | Eq.(14)         |
| (1)       | (2)     | (3)      | (4)          | (5)       | (6)         | (7)       | (8)        | (9)            | (10)            | (11)            |
| Ν         | LT/LTOR | 109      | 109          | 68        | 88          | 5         | 2          | 199            | 0.21            |                 |
|           | ST      | 465      | 465          | 78        | 101         | 3         | 1          | 567            |                 |                 |
|           | RT      | 140      | 140          | 47        | 61          | 3         | 1          | 202            |                 | 0.21            |
|           | TOTAL   |          |              |           |             |           |            | 968            |                 |                 |
| S         | LT/LTOR | 104      | 104          | 62        | 81          | 4         | 2          | 187            | 0.26            |                 |
|           | ST      | 236      | 236          | 99        | 129         | 4         | 2          | 367            |                 |                 |
|           | RT      | 88       | 88           | 55        | 72          | 3         | 1          | 161            |                 | 0.23            |
|           | TOTAL   |          |              |           |             |           |            | 715            |                 |                 |
| E         | LT/LTOR | 164      | 164          | 113       | 147         | 5         | 2          | 313            | 0.24            |                 |
|           | ST      | 443      | 443          | 150       | 195         | 5         | 2          | 640            |                 |                 |
|           | RT      | 202      | 202          | 98        | 127         | 4         | 2          | 331            |                 | 0.26            |
|           | TOTAL   |          |              |           |             |           |            | 1284           |                 |                 |
| W         | LT/LTOR | 145      | 145          | 84        | 109         | 10        | 4          | 258            | 0.23            |                 |
|           | ST      | 413      | 413          | 132       | 172         | 6         | 2          | 587            |                 |                 |
|           | RT      | 137      | 137          | 90        | 117         | 6         | 2          | 256            |                 | 0.23            |
|           | TOTAL   |          |              |           |             |           |            | 1101           |                 |                 |

# Calculations Of Existing Condition

**Traffic Flow Distribution** 



Phase(2)







| Appr | Green       | Appr |        | Ratio     |                 | RT-flov         | w pcu/h Eff                    |       |            | Saturation flow pcu/h |          |                |         |          |                | Flow  | Phase      | Green   | Capacity   | Degree |
|------|-------------|------|--------|-----------|-----------------|-----------------|--------------------------------|-------|------------|-----------------------|----------|----------------|---------|----------|----------------|-------|------------|---------|------------|--------|
| Code | In          | type |        | of turnir | ng              | Own             | Oppos                          | width | Base       | ŀ                     | Adjustm  | ent facto      | rs      | Adjusted | Flow           | ratio | Ratio      | Time    | pcu/h      | Of     |
|      | Phase       |      |        | vehicle   | S               | dir             | Dir                            | (m)   | Value      | All appr type         |          |                | Value   | pcu/h    | FR             |       | Sec        | S x g/c | Saturation |        |
|      | No          |      |        |           |                 |                 |                                |       | pcu/h      | City                  | Side     | Gradient       | Parking | pcu/h    |                |       |            |         | _          |        |
|      |             |      |        |           |                 |                 |                                |       | -          | size                  | friction |                | _       |          |                |       |            |         |            |        |
|      |             |      | P LTOR | P LT      | P <sub>RT</sub> | Q <sub>LT</sub> | Q LTO                          | We    | S₀         | Fcs                   | $F_{SF}$ | F <sub>G</sub> | $F_{P}$ | S        | Q              | Q/S   | PR=        | g       | С          | Q/C    |
|      |             |      |        |           |                 |                 |                                |       | Fig. 2.3   |                       |          |                |         |          |                |       | FRcrit/IFR |         |            |        |
|      |             |      |        |           |                 |                 |                                |       | Fig. 2.4   |                       |          |                |         | _ (2)    |                |       |            | _ /_>   |            |        |
|      |             |      |        |           |                 |                 |                                |       |            |                       |          |                |         | Eq.(2)   |                |       |            | Eq.(5)  |            |        |
| (1)  | (2)         | (3)  | (4)    | (5)       | (6)             | (7)             | (8)                            | (9)   | (10)       | (11)                  | (12)     | (13)           | (14)    | (15)     | (16)           | (17)  | (18)       | (19)    | (20)       | (21)   |
| Ν    | 1           | 0    |        | 0.21      | 0.21            | 199             | 187                            | 5     | 2140       | 1.00                  | 0.95     | 1.00           | 1.00    | 2033     | 766            | 0.38  | 0.48       | 22      | 828        | 0.925  |
| S    | 1           | 0    |        | 0.26      | 0.23            | 187             | 199                            | 5     | 2120       | 1.00                  | 0.98     | 1.00           | 1.00    | 2078     | 554            | 0.27  |            | 22      | 847        | 0.66   |
| E    | 2           | 0    |        | 0.24      | 0.26            | 313             | 258                            | 6     | 2460       | 1.00                  | 0.95     | 1.00           | 1.00    | 2337     | 953            | 0.41  | 0.52       | 24      | 1039       | 0.92   |
| W    | 2           | 0    |        | 0.23      | 0.23            | 258             | 313                            | 6     | 2460       | 1.00                  | 0.95     | 1.00           | 1.00    | 2337     | 845            | 0.37  |            | 24      | 1039       | 0.81   |
|      |             |      |        |           |                 |                 |                                |       |            |                       |          |                |         |          |                |       |            |         |            |        |
|      |             |      |        |           |                 |                 |                                |       |            |                       |          |                |         |          |                |       |            |         |            |        |
| To   | tal lost ti | me   |        | Unadju    | stment of       | cycle tim       | ne C <sub>US</sub> (sec) Eq.(2 |       |            |                       |          |                |         |          | IFR=           |       |            |         |            |        |
| LTI  | (sec) 8     | Sec  |        | Adjustr   | nent cyc        | le time         |                                | C (s  | sec) Eq.(3 | 54                    |          |                |         | ĺ        | <b>FR</b> CRIT |       |            |         |            |        |

| Approach           | Traffic | Capacity          | Degree of  | Green | No              | . of queuing | yvehicles (po | cu)               | Queue         | Stop      | No. of                                      |                                 | De                 | Delay           Average         Average<br>delay           Seometric<br>delay         sec/pcu           DG         DT+DG           Eq.(15)         (13)+(14)           (14)         (15)           4.66         41.06           3.42         18.30           4.34         34.92           3.74         22.47           D         Total: |          |
|--------------------|---------|-------------------|------------|-------|-----------------|--------------|---------------|-------------------|---------------|-----------|---|---------------------------------|--------------------|---|----------|
| Code               | flow    | pcu/h             | Saturation | Ratio |                 |              |               |                   | length        | rate      | Stops                                       | Average                         | Average            | Average<br>delay  | Total    |
|                    | pcu/h   |                   | DS         | GR    | NQ <sub>1</sub> | $NQ_2$       | Total         | NQ <sub>MAX</sub> | (m)           | stops/pcu | pcu/h                                       | Traffic<br>delay                | Geometric<br>delay | sec/pcu   | Delay    |
|                    |         |                   | =          | =     |                 |              | $NQ_1 + NQ_2$ |                   |               |           |   | sec/pcu                         | sec/pcu            | D =   | Pcu.sec  |
|                    | Q       | С                 | Q/C        | g/c   |                 |              | NQ            |                   | QL            | NS        | N <sub>SV</sub>                             | DT                              | DG                 | DT+DG   | DхQ      |
|                    |         |                   |            |       | Eq.(8)          | Eq.(9)       | Eq.(7)        | Fig.2.5           | Eq.(10)       | Eq.(11)   | Eq.(12)                                     | Eq.(14)                         | Eq.(15)            | (13)+(14)   | (2)+(15) |
| (1)                | (2)     | (3)               | (4)        | (5)   | (6)             | (7)          | (8)           | (9)               | (10)          | (11)      | (12)  | (13)                            | (14)               | (15)  | (16)     |
| N                  | 766     | 828               | 0.925      | 0.41  | 4.89            | 10.92        | 15.81         | 21.5              | 86            | 1.24      | 950   | 36.40                           | 4.66               | 41.06   | 31452    |
| S                  | 554     | 847               | 0.66       | 0.41  | 0.47            | 6.60         | 7.07          | 12                | 48            | 0.78      | 424   | 14.88                           | 3.42               | 18.30   | 9955     |
| E                  | 953     | 1039              | 0.92       | 0.44  | 4.72            | 13.45        | 18.17         | 26                | 87            | 1.14      | 1086  | 30.58                           | 4.34               | 34.92   | 33279    |
| W                  | 845     | 1039              | 0.81       | 0.44  | 1.61            | 11.03        | 12.64         | 19                | 63            | 0.90      | 761   | 18.73                           | 3.74               | 22.47   | 18987    |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
|                    |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
| ROTR (all)         |         |                   |            |       |                 |              |               |                   |               |           |   |                                 |                    |   |          |
| Flow adi. Qadi :   |         | Total: 3221 Total |            |       |                 |              |               |                   |               | 167317    |   |                                 |                    |   |          |
|                    |         | 1                 |            |       |                 |              |               | i otal.           |               |           |   | Average Intersection Delay (sec |                    |   |          |
| I otal flow Qtot : | 3118    |                   |            |       |                 |              |               | Averag            | ge no. of sto | ops/pcu   | 1.03 Average intersection belay (sec / pcu) |                                 |                    |   |          |

## **Calculations Of Two Phase**

#### 1. Very High Traffic Flow

|           |          |           |             |           | TRAFFIC F   | LOW MOTOR         | RISED VEHIC | LES (MV)       |                 |                        |  |
|-----------|----------|-----------|-------------|-----------|-------------|-------------------|-------------|----------------|-----------------|------------------------|--|
|           |          | Light Ver | nicles (LV) | Heavy Ve  | hicles (HV) | Motorcyc          | cles (MC)   | Total          |                 | Ratio                  |  |
| Appr.code | Dir      | pce prote | ected = 1.0 | pce prote | ected = 1.3 | pce prote         | cted = 0.2  | Motor vehicles | of              |                        |  |
| Appi code | DII.     | pce oppo  | osed = 1.0  | pce oppo  | osed = 1.3  | pce opposed = 0.4 |             | MV             | turning         |                        |  |
|           |          | veh/h     | pcu/h       | veh/h     | pcu/h       | veh/h             | pcu/h       | pcu/h          | р <sub>LT</sub> | <b>р</b> <sub>RT</sub> |  |
|           |          |           | Орр         |           | Орр         |                   | Орр         | Орр            | Eq.(13)         | Eq.(14)                |  |
| (1)       | (2)      | (3)       | (4)         | (5)       | (6)         | (7)               | (8)         | (9)            | (10)            | (11)                   |  |
| N         | LT/LTOR  | 109       | 109         | 68        | 88          | 5                 | 2           | 199            | 0.21            |                        |  |
|           | ST       | 465       | 465         | 78        | 101         | 3                 | 1           | 567            |                 |                        |  |
|           | RT       | 140       | 140         | 47        | 61          | 3                 | 1           | 202            |                 | 0.21                   |  |
|           | TOTAL    |           |             |           |             |                   |             | 968            |                 |                        |  |
| S         | LT/LTOR  | 104       | 104         | 62        | 81          | 4                 | 2           | 187            | 0.26            |                        |  |
|           | ST       | 236       | 236         | 99        | 129         | 4                 | 2           | 367            |                 |                        |  |
|           | RT       | 88        | 88          | 55        | 72          | 3                 | 1           | 161            |                 | 0.23                   |  |
|           | TOTAL    |           |             |           |             |                   |             | 715            |                 |                        |  |
| E         | LT/LTOR  | 164       | 164         | 113       | 147         | 5                 | 2           | 313            | 0.24            |                        |  |
|           | ST       | 443       | 443         | 150       | 195         | 5                 | 2           | 640            |                 |                        |  |
|           | RT       | 202       | 202         | 98        | 127         | 4                 | 2           | 331            |                 | 0.26                   |  |
|           | TOTAL    |           |             |           |             |                   |             | 1284           |                 |                        |  |
| W         | LT/LTOR  | 145       | 145         | 84        | 109         | 10                | 4           | 258            | 0.23            |                        |  |
|           | ST       | 413       | 413         | 132       | 172         | 6                 | 2           | 587            |                 |                        |  |
|           | RT       | 137       | 137         | 90        | 117         | 6                 | 2           | 256            |                 | 0.23                   |  |
|           | TOTAL    |           |             |           |             |                   |             | 1101           |                 |                        |  |
|           | <u> </u> |           |             |           |             | • 1               | DI(2)       |                |                 |                        |  |

**Traffic Flow Distribution** 

Phase (1)

Phase(2)





| Appr  | Green      | Appr |        | Ratio           |                 | RT-flo          | w pcu/h          | Eff   |                   | S                                  | aturatio | n flow pc | u/h     |          | Traffic             | Flow  | Phase      | Green  | Capacity | Degree     |
|-------|------------|------|--------|-----------------|-----------------|-----------------|------------------|-------|-------------------|------------------------------------|----------|-----------|---------|----------|---------------------|-------|------------|--------|----------|------------|
| Code  | In         | type | c      | of turnir       | ng              | Own             | Oppos            | Width | Base              | ŀ                                  | Adjustm  | ent facto | `S      | Adjusted | Flow                | Ratio | Ratio      | Time   | pcu/h    | Ōf         |
|       | Phase      |      |        | vehicle         | S               | Dir             | Dir              | (m)   | Value             |                                    | All ap   | pr type   |         | Value    | pcu/h               | FR    |            | Sec    | S x g/c  | Saturation |
|       | No         |      |        |                 |                 |                 |                  |       | pcu/h             | Jh City Side GradientParking pcu/h |          |           |         | pcu/h    |                     |       |            |        | •        |            |
|       |            |      |        |                 |                 |                 |                  |       |                   | size friction                      |          |           |         |          |                     |       |            |        |          |            |
|       |            |      | P LTOR | P <sub>LT</sub> | P <sub>RT</sub> | Q <sub>LT</sub> | Q <sub>LTO</sub> | We    | S₀                | $F_{CS}$                           | $F_{SF}$ | $F_G$     | $F_{P}$ | S        | Q                   | Q/S   | PR=        | g      | С        | Q/C        |
|       |            |      |        |                 |                 |                 |                  |       | Fig. 2.3          |                                    |          |           |         |          |                     |       | FRcrit/IFR |        |          |            |
|       |            |      |        |                 |                 |                 |                  |       | гı <u>у</u> . 2.4 |                                    |          |           |         | Eq.(2)   |                     |       |            | Eq.(5) |          |            |
| (1)   | (2)        | (3)  | (4)    | (5)             | (6)             | (7)             | (8)              | (9)   | (10)              | (11)                               | (12)     | (13)      | (14)    | (15)     | (16)                | (17)  | (18)       | (19)   | (20)     | (21)       |
| Ν     | 1          | 0    |        | 0.21            | 0.21            | 199             | 187              | 5     | 2140              | 1.00                               | 0.95     | 1.00      | 1.00    | 2033     | 766                 | 0.38  | 0.48       | 35     | 878      | 0.87       |
| S     | 1          | 0    |        | 0.26            | 0.23            | 187             | 199              | 5     | 2120              | 1.00                               | 0.98     | 1.00      | 1.00    | 2078     | 554                 | 0.27  |            | 35     | 898      | 0.62       |
| Е     | 2          | 0    |        | 0.24            | 0.26            | 313             | 258              | 6     | 2460              | 1.00                               | 0.95     | 1.00      | 1.00    | 2337     | 953                 | 0.41  | 0.52       | 38     | 1096     | 0.87       |
| W     | 2          | 0    |        | 0.23            | 0.23            | 258             | 313              | 6     | 2460              | 1.00                               | 0.95     | 1.00      | 1.00    | 2337     | 845                 | 0.37  |            | 38     | 1096     | 0.77       |
|       |            |      |        |                 |                 |                 |                  |       |                   |                                    |          |           |         |          |                     |       |            |        |          |            |
|       |            |      |        |                 |                 |                 |                  |       |                   |                                    |          |           |         |          |                     |       |            |        |          |            |
| Tot   | al lost ti | me   |        | Una             | djustme         | nt cycle        | e time           | CUS   | s (sec)           | 81                                 |          |           |         |          | IFR=                | 0 70  |            |        |          |            |
| LTI ( | sec) 8     | Sec  |        | Adju            | stment          | cycle tir       | ne               | С     | (sec)             | 81                                 |          |           |         |          | ∑FR <sub>CRIT</sub> | 0.19  |            |        |          |            |

| Approach         | Traffic | Capacity | Degree of  | Green | No.             | of queui        | ng vehicles   | (pcu)             | Queue   | Stop      | No. of          |                                      | De              | lay              |          |
|------------------|---------|----------|------------|-------|-----------------|-----------------|---------------|-------------------|---------|-----------|-----------------|--------------------------------------|-----------------|------------------|----------|
| Code             | flow    | pcu/h    | Saturation | Ratio |                 |                 |               |                   | length  | rate      | Stops           | Average                              | Average         | Average<br>delay | Total    |
|                  | pcu/h   |          | DS         | GR    | NQ <sub>1</sub> | NQ <sub>2</sub> | Total         | NQ <sub>MAX</sub> | (m)     | stops/pcu | pcu/h           | Traffic<br>delay                     | Geometric delay | sec/pcu          | Delay    |
|                  |         |          | =          | =     |                 |                 | $NQ_1 + NQ_2$ |                   |         |           |                 | sec/pcu                              | sec/pcu         | D =              | Pcu.sec  |
|                  | Q       | С        | Q/C        | g/c   |                 |                 | NQ            |                   | QL      | NS        | N <sub>SV</sub> | DT                                   | DG              | DT+DG            | DxQ      |
|                  |         |          |            | -     | Eq.(8)          | Eq.(9)          | Eq.(7)        | Fig.2.5           | Eq.(10) | Eq.(11)   | Eq.(12)         | Eq.(14)                              | Eq.(15)         | (13)+(14)        | (2)+(15) |
| (1)              | (2)     | (3)      | (4)        | (5)   | (6)             | (7)             | (8)           | (9)               | (10)    | (11)      | (12)            | (13)                                 | (14)            | (15)             | (16)     |
| Ν                | 766     | 878      | 0.87       | 0.43  | 2.72            | 15.7            | 18.42         | 27                | 108     | 0.96      | 735             | 32.2                                 | 3.89            | 36.09            | 27645    |
| S                | 554     | 898      | 0.62       | 0.43  | 0.32            | 9.7             | 10.02         | 16                | 64      | 0.72      | 399             | 19.22                                | 3.27            | 22.49            | 12459    |
| E                | 953     | 1096     | 0.87       | 0.47  | 2.74            | 19.22           | 21.96         | 32                | 107     | 0.92      | 877             | 28.25                                | 3.80            | 32.05            | 30544    |
| W                | 845     | 1096     | 0.77       | 0.47  | 1.16            | 15.8            | 16.96         | 26                | 87      | 0.80      | 676             | 21.64                                | 3.48            | 25.12            | 21226    |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
|                  |         |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
| ROTR (all)       | 950     |          |            |       |                 |                 |               |                   |         |           |                 |                                      |                 |                  |          |
| Flow adj. Qadj : |         |          |            |       |                 |                 |               |                   | Total:  |           | 2687            |                                      |                 | Total:           | 91874    |
| Total flow Qtot  | 3118    | Average  |            |       |                 |                 |               |                   |         | tops/pcu  | 0.86            | Average intersection delay (sec/pcu) |                 |                  | 29.47    |

#### 2. High Traffic Flow

| Appr code | Dir.    | Total<br>Motor<br>vehicles<br>MV | Ratio<br>of<br>turning |                 |  |  |  |  |
|-----------|---------|----------------------------------|------------------------|-----------------|--|--|--|--|
|           |         | pcu/h                            | р <sub>LT</sub>        | р <sub>кт</sub> |  |  |  |  |
|           |         | Орр                              | Eq.(13)                | Eq.(14)         |  |  |  |  |
| (1)       | (2)     | (9)                              | (10)                   | (11)            |  |  |  |  |
| N         | LT/LTOR | 149                              | 0.21                   |                 |  |  |  |  |
|           | ST      | 425                              |                        |                 |  |  |  |  |
|           | RT      | 152                              |                        | 0.21            |  |  |  |  |
|           | TOTAL   | 726                              |                        |                 |  |  |  |  |
| S         | LT/LTOR | 140                              | 0.26                   |                 |  |  |  |  |
|           | ST      | 275                              |                        |                 |  |  |  |  |
|           | RT      | 121                              |                        | 0.23            |  |  |  |  |
|           | TOTAL   | 536                              |                        |                 |  |  |  |  |
| Ε         | LT/LTOR | 235                              | 0.24                   |                 |  |  |  |  |
|           | ST      | 480                              |                        |                 |  |  |  |  |
|           | RT      | 248                              |                        | 0.26            |  |  |  |  |
|           | TOTAL   | 963                              |                        |                 |  |  |  |  |
| W         | LT/LTOR | 194                              | 0.23                   |                 |  |  |  |  |
|           | ST      | 440                              |                        |                 |  |  |  |  |
|           | RT      | 192                              |                        | 0.23            |  |  |  |  |
|           | TOTAL   | 826                              |                        |                 |  |  |  |  |



RT-flow pcu/h Eff Saturation flow pcu/h Flow Phase Green Capacity Degree Appr Green Appr Ratio Traffic Adjustment factors Code In type of turning Own Oppos Width Base Adjusted Flow ratio Ratio Time pcu/h Of Phase vehicles FR PR = Sec S x g/c saturation (m) All appr type pcu/h dir Dir Value Value City Side GradientParking FRcrit No pcu/h pcu/h size friction P LTOR P LT P<sub>RT</sub> Q<sub>LTO</sub> We Fcs  $F_{SF}$  $F_{G}$  $F_{P}$ S Q Q/S IFR С Q/C Q<sub>LT</sub> S<sub>o</sub> g (9) (1) (2) (3) (4) (5) (6) (7) (8) (10) (11) (12) (13) (14) (15) (16) (17) (18) (19) (20) (21) 2320 0.95 812 Ν 1 0 0.21 0.21 149 140 5 1.00 1.00 1.00 2204 574 0.26 0.47 14 0.71 S 0.26 0.23 140 149 2300 1.00 0.98 1.00 1.00 2254 415 0.18 14 830 0.50 0 5 1 0.95 Е 2 0 0.24 0.26 235 194 6 2580 1.00 1.00 1.00 2451 715 0.29 0.53 16 1032 0.69 W 0.23 0.23 2350 194 235 1.00 0.95 1.00 1.00 2233 634 0.28 16 940 0.67 2 0 6

**Traffic Flow Distribution** 

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| Total lost time      | Э           | Unad     | justment cyc | le time |                 | Cus (                       | sec)               | 38              |                   |   |           | IFR     | = 0.55           |                 |                  |          |
|----------------------|-------------|----------|--------------|---------|-----------------|-----------------------------|--------------------|-----------------|-------------------|---|-----------|---------|------------------|-----------------|------------------|----------|
| LTI (sec) 8 S        | ec          | Adjus    | tment cycle  | tim     |                 | С (                         | sec)               | 38              |                   |   |           | ∑FRc    | RIT              |                 |                  |          |
|                      | <b>–</b> (C |          |              |         |                 | · ·                         |                    |                 | \<br>\            |   |           |         |                  |                 |                  |          |
| Approach             | Iraffic     | Capacity | Degree of    | Green   | N0.             | No. of queuing vehicles (po |                    |                 | ocu)              | Queue                                   | Stop      | No. of  | Delay            |                 |                  | 1        |
| Code                 | Flow        | pcu/h    | Saturation   | ratio   |                 |                             |                    |                 |                   | length                                  | rate      | Stops   | Average          | Average         | Average<br>delay | Total    |
|                      | pcu/h       |          | DS           | GR      | NQ <sub>1</sub> | NQ <sub>2</sub>             | Tota               | al              | NQ <sub>MAX</sub> | (m)                                     | stops/pcu | pcu/h   | Traffic<br>delay | Geometric delay | sec/pcu          | Delay    |
|                      |             |          | =            | =       |                 |                             | NQ <sub>1</sub> +N | VQ <sub>2</sub> |                   |   |           |         | sec/pcu          | sec/pcu         | D =              | Pcu.sec  |
|                      | Q           | С        | Q/C          | g/c     |                 |                             | NQ                 | 2               |                   | QL                                      | NS        | Nsv     | DT               | DĠ              | DT+DG            | DxQ      |
|                      |             |          |              | _       | Eq.(8)          | Eq.(9)                      | Eq.(7              | 7)              | Fig.2:5           | Eq.(10)                                 | Eq.(11)   | Eq.(12) | Eq.(14)          | Eq.(15s)        | (13)+(14)        | (2)+(15) |
| (1)                  | (2)         | (3)      | (4)          | (5)     | (6)             | (7)                         | (8)                |                 | (9)               | (10)                                    | (11)      | (12)    | (13)             | (14)            | (15)             | (16)     |
| Ν                    | 574         | 812      | 0.71         | 0.37    | 0.72            | 0502                        | 5.92               | 2               | 10.6              | 42                                      | 0.88      | 505     | 13.4             | 3.67            | 17.1             | 9815     |
| S                    | 415         | 830      | 0.50         | 0.37    | 0               | 3.4                         | 3.4                |                 | 7                 | 28                                      | 0.70      | 291     | 9.25             | 3.2             | 12.45            | 5167     |
| E                    | 715         | 1032     | 0.69         | 0.42    | 0.61            | 6.2                         | 6.8                | 1               | 11.7              | 39                                      | 0.81      | 579     | 11.13            | 3.54            | 14.67            | 10489    |
| W                    | 634         | 940      | 0.67         | 0.42    | 0.61            | 5.4                         | 6.01               | 1               | 10                | 33                                      | 0.81      | 514     | 11.23            | 3.5             | 14.73            | 9339     |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
|                      |             |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
| ROTR (all)           | 713         |          |              |         |                 |                             |                    |                 |                   |   |           |         |                  |                 |                  |          |
| Flow adj. Qadj :     |             |          |              |         |                 |                             |                    |                 |                   | Total:                                  |           | 1889    |                  |                 | Total:           | 34810    |
| Total flow Qtot 2338 |             |          |              |         |                 | Average no. of stops/pcu    |                    |                 | 0.81              | Average intersection delay<br>(sec/pcu) |           |         | 14.89            |                 |                  |          |
#### 3. Low Traffic Flow

| Appr code | Dir.    | Total<br>Motor<br>vehicles<br>MV |                 | Ratio<br>of<br>turning |
|-----------|---------|----------------------------------|-----------------|------------------------|
|           |         | pcu/h                            | р <sub>LT</sub> | р <sub>кт</sub>        |
|           |         | Орр                              | Eq.(13)         | Eq.(14)                |
| (1)       | (2)     | (9)                              | (10)            | (11)                   |
| Ν         | LT/LTOR | 100                              | 0.21            |                        |
|           | ST      | 284                              |                 |                        |
|           | RT      | 101                              |                 | 0.21                   |
|           | TOTAL   | 485                              |                 |                        |
| S         | LT/LTOR | 94                               | 0.26            |                        |
|           | ST      | 184                              |                 |                        |
|           | RT      | 81                               |                 | 0.23                   |
|           | TOTAL   | 359                              |                 |                        |
| E         | LT/LTOR | 157                              | 0.24            |                        |
|           | ST      | 320                              |                 |                        |
|           | RT      | 166                              |                 | 0.26                   |
|           | TOTAL   | 643                              |                 |                        |
| W         | LT/LTOR | 129                              | 0.23            |                        |
|           | ST      | 294                              |                 |                        |
|           | RT      | 128                              |                 | 0.23                   |
|           | TOTAL   | 551                              |                 |                        |



RT-flow pcu/h Eff Saturation flow pcu/h Traffic Flow Phase Green Capacity Degree Appr Green Appr Ratio Code Type of turning Own Oppos Width Adjustment factors Adjusted Ratio pcu/h Base Flow ratio Time Of In PR = FR Phase vehicles dir Dir (m) Value All appr type Value Sec S x g/c saturation pcu/h Side Gradient Parking pcu/h City pcu/h FRcrit no Friction size P<sub>LTOR</sub> P<sub>LT</sub>  $Q_{LT}$  $\mathsf{F}_\mathsf{G}$  $F_{P}$ Q/S P<sub>RT</sub>  $Q_{LTO}$  $W_{e}$ S₀ F<sub>cs</sub>  $\mathsf{F}_{\mathsf{SF}}$ S Q IFR G С Q/C Т (12) (1) (2) (3) (4) (5) (6) (7) (8) (9) (10) (11) (13) (14) (15) (16) (17) (18) (19) (20) (21) 0.21 0.21 100 5 2510 1.00 0.95 1.00 1.00 2385 384 0.16 0.47 826 Ν 1 0 94 9 0.46 0.26 0.23 S 0 94 100 5 2500 1.00 0.98 1.00 1.00 2450 278 0.11 9 848 0.33 1 0.26 157 2850 2708 477 0.53 10 1042 Е 0.24 129 1.00 0.95 1.00 1.00 0.18 0.46 2 0 6 W 2 0 023 0.23 129 157 6 2760 1.00 0.95 1.00 1.00 2622 423 0.16 10 1008 0.42

| Total lost time   |             | Una      | djustment cy | cle time |                 | C <sub>US</sub> (see | c) 26                            |                   |             |           | IFR=   | = 0.34        |                      |                       |          |
|-------------------|-------------|----------|--------------|----------|-----------------|----------------------|----------------------------------|-------------------|-------------|-----------|--------|---------------|----------------------|-----------------------|----------|
| LTI (sec) 8 Se    | С           | Adju     | stment cycle | time     |                 | C (se                | ec) 27                           |                   |             |           | ∑FRc   | RIT           |                      |                       |          |
|                   | <b>T</b> (C |          |              |          |                 |                      |                                  | ( )               |             | 0         |        |               |                      |                       |          |
| Approach          | Iraffic     | Capacity | Degree of    | Green    | NC              | o. of que            | uing venici                      | es (pcu)          | Queue       | Stop      | NO. Of |               | D                    | elay                  | 1        |
| Code              | Flow        | pcu/h    | Saturation   | ratio    |                 |                      |                                  |                   | length      | rate      | Stops  | Average       | Average              | Average<br>delay      | Total    |
|                   | pcu/h       |          | DS           | GR       | $\mathbf{NQ}_1$ | $NQ_2$               | Total                            | NQ <sub>MAX</sub> | (m)         | stops/pcu | pcu/h  | Traffic delay | Geometric delay      | sec/pcu               | Delay    |
|                   |             |          | =            | =        |                 |                      | NQ <sub>1</sub> +NQ <sub>2</sub> |                   |             |           |        | sec/pcu       | sec/pcu              | D =                   | Pcu.sec  |
|                   | Q           | С        | Q/C          | g/c      |                 |                      | NQ                               |                   | QL          | NS        | Nsv    | DT            | DĠ                   | DT+DG                 | DxQ      |
|                   |             |          |              | -        |                 |                      |                                  |                   |             |           |        |               |                      | (13)+(14)             | (2)+(15) |
| (1)               | (2)         | (3)      | (4)          | (5)      | (6)             | (7)                  | (8)                              | (9)               | (10)        | (11)      | (12)   | (13)          | (14)                 | (15)                  | (16)     |
| Ν                 | 384         | 826      | 0.46         | 0.35     | 0               | 2.15                 | 2.15                             | 5                 | 20          | 0.70      | 269    | 6.55          | 3.20                 | 9.75                  | 3744     |
| S                 | 278         | 848      | 0.33         | 0.35     | 0               | 1.47                 | 1.47                             | 3.5               | 14          | 0.66      | 184    | 6.21          | 3.11                 | 9.32                  | 2591     |
| E                 | 477         | 1042     | 0.46         | 0.38     | 0               | 2.60                 | 2.60                             | 6                 | 20          | 0.68      | 324    | 6.1           | 3.22                 | 9.32                  | 4446     |
| W                 | 423         | 1008     | 0.42         | 0.38     | 0               | 2.25                 | 2.25                             | 5.8               | 19          | 0.66      | 279    | 5.95          | 3.11                 | 9.10                  | 3849     |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
|                   |             |          |              |          |                 |                      |                                  |                   |             |           |        |               |                      |                       |          |
| ROTR (all)        | 476         |          |              |          |                 |                      |                                  |                   | <u> </u>    |           | 1050   |               |                      |                       |          |
| Flow adj. Qadj :  |             |          |              |          |                 |                      |                                  |                   | Total:      |           | 1056   | 1.            |                      | Total:                | 14630    |
| Total flow Qtot : | 1562        |          |              |          |                 |                      |                                  | Averag            | e no. of si | tops/pcu  | 0.68   | Ave           | rage interse<br>(sec | ction delay<br>c/pcu) | 9.40     |

### 4. Very Low Traffic Flow

| Appr code | Dir.    | Total<br>Motor vehicles<br>MV | ti      | Ratio<br>of<br>urning |
|-----------|---------|-------------------------------|---------|-----------------------|
|           |         | pcu/h                         | р       | р <sub>кт</sub>       |
|           |         | Орр                           | Eq.(13) | Eq.(14)               |
| (1)       | (2)     | (9)                           | (10)    | (11)                  |
| N         | LT/LTOR | 50                            | 0.21    |                       |
|           | ST      | 142                           |         |                       |
|           | RT      | 51                            |         | 0.21                  |
|           | TOTAL   | 243                           |         |                       |
| S         | LT/LTOR | 47                            | 0.26    |                       |
|           | ST      | 92                            |         |                       |
|           | RT      | 40                            |         | 0.23                  |
|           | TOTAL   | 179                           |         |                       |
| E         | LT/LTOR | 78                            | 0.24    |                       |
|           | ST      | 160                           |         |                       |
|           | RT      | 83                            |         | 0.26                  |
|           | TOTAL   | 321                           |         |                       |
| W         | LT/LTOR | 65                            | 0.23    |                       |
|           | ST      | 147                           |         |                       |
|           | RT      | 64                            |         | 0.23                  |
|           | TOTAL   | 276                           |         |                       |



| Appr  | Green     | Appr |        | Ratio     |                 | RT-flo    | w pcu/h          | Eff   |                | S               | aturatio | n flow pcu | u/h     |          | Traffic | Flow  | Phase  | Green | Capacity | Degree     |
|-------|-----------|------|--------|-----------|-----------------|-----------|------------------|-------|----------------|-----------------|----------|------------|---------|----------|---------|-------|--------|-------|----------|------------|
| Code  | e In      | type |        | of turnir | ng              | Own       | Oppos            | width | Base           | I               | Adjustm  | ent factor | S       | Adjusted | Flow    | ratio | Ratio  | Time  | pcu/h    | Of         |
|       | Phase     |      |        | vehicle   | S               | Dir       | Dir              | (m)   | Value          |                 | All ap   | pr type    |         | Value    | pcu/h   | FR    | PR =   | Sec   | S x g/c  | saturation |
|       | No        |      |        |           |                 |           |                  |       | pcu/h          | City            | Side     | Gradient   | Parking | pcu/h    | -       |       | FRcrit |       |          |            |
|       |           |      |        |           |                 |           |                  |       | -              | size            | Friction |            | -       |          |         |       |        |       |          |            |
|       |           |      | P LTOR | P LT      | P <sub>RT</sub> | Q LT      | Q <sub>LTO</sub> | We    | S <sub>o</sub> | F <sub>cs</sub> | $F_{SF}$ | $F_{G}$    | FP      | S        | Q       | Q/S   | IFR    | g     | С        | Q/C        |
|       |           |      |        |           |                 |           |                  |       |                |                 |          |            |         |          |         |       |        | •     |          |            |
|       |           |      |        |           |                 |           |                  |       |                |                 |          |            |         |          |         |       |        |       |          |            |
|       |           |      |        |           |                 |           |                  |       |                |                 |          |            |         |          |         |       |        |       |          |            |
| (1)   | (2)       | (3)  | (4)    | (5)       | (6)             | (7)       | (8)              | (9)   | (10)           | (11)            | (12)     | (13)       | (14)    | (15)     | (16)    | (17)  | (18)   | (19)  | (20)     | (21)       |
| Ν     | 1         | 0    |        | 0.21      | 0.21            | 50        | 47               | 5     | 2720           | 1.00            | 0.95     | 1.00       | 1.00    | 2584     | 192     | 0.074 | 0.49   | 6     | 775      | 0.25       |
| S     | 1         | 0    |        | 0.26      | 0.23            | 47        | 50               | 5     | 2710           | 1.00            | 0.98     | 1.00       | 1.00    | 2656     | 139     | 0.052 |        | 6     | 797      | 0.17       |
| E     | 2         | 0    |        | 0.24      | 0.26            | 78        | 65               | 6     | 3200           | 1.00            | 0.95     | 1.00       | 1.00    | 3040     | 238     | 0.078 | 0.51   | 6     | 912      | 0.26       |
| W     | 2         | 0    |        | 0.23      | 0.23            | 65        | 78               | 6     | 3100           | 1.00            | 0.95     | 1.00       | 1.00    | 2945     | 212     | 0.072 |        | 6     | 884      | 0.24       |
|       |           |      |        |           |                 |           |                  |       |                |                 |          |            |         |          |         |       |        |       |          |            |
| Total | lost time |      |        | Unadju    | stment o        | cycle tim | е                | С     | Us (sec)       | 20              |          |            |         |          | IFR=    | 0.152 |        |       |          |            |

| LTI (sec) 8 S        | ec      | Adjus    | tment cycle              | e time |     | С (             | sec) 20       | )     |             |             | ΣF     | R <sub>CRIT</sub> |                      |                       |          |
|----------------------|---------|----------|--------------------------|--------|-----|-----------------|---------------|-------|-------------|-------------|--------|-------------------|----------------------|-----------------------|----------|
| Approach             | Traffic | Capacity | Degree of                | Green  | No  | o. of queuin    | g vehicles (  | pcu)  | Queue       | Stop        | No. of | Delay             |                      |                       |          |
| Code                 | flow    | pcu/h    | Saturation               | Ratio  |     |                 |               |       | length      | rate        | Stops  | Average           | Average              | Average delay         | Total    |
|                      | pcu/h   |          | DS                       | GR     | NQ1 | NQ <sub>2</sub> | Total         | NQMAX | (m)         | stops/pcu   | pcu/h  | Traffic delay     | Geometric<br>delay   | sec/pcu               | Delay    |
|                      |         |          | =                        | =      |     |                 | $NQ_1 + NQ_2$ |       |             |             |        | sec/pcu           | sec/pcu              | D =                   | Pcu.sec  |
|                      | Q       | С        | Q/C                      | g/c    |     |                 | NQ            |       | QL          | NS          | Nsv    | DT                | DG                   | DT+DG                 | DxQ      |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      | (13)+(14)             | (2)+(15) |
| (1)                  | (2)     | (3)      | (4)                      | (5)    | (6) | (7)             | (8)           | (9)   | (10)        | (11)        | (12)   | (13)              | (14)                 | (15)                  | (16)     |
| N                    | 192     | 775      | 0.25                     | 0.30   | 0   | 0.81            | 0.81          | 2.8   | 11          | 0.68        | 131    | 5.3               | 3.12                 | 8.42                  | 1617     |
| S                    | 139     | 797      | 0.17                     | 0.30   | 0   | 0.57            | 0.57          | 2     | 8           | 0.66        | 92     | 5.2               | 3.11                 | 8.31                  | 1155     |
| E                    | 238     | 912      | 0.26                     | 0.30   | 0   | 1.00            | 1.00          | 3     | 10          | 0.68        | 162    | 5.31              | 3.22                 | 8.53                  | 2030     |
| W                    | 212     | 884      | 0.24                     | 0.30   | 0   | 0.89            | 0.89          | 2.9   | 10          | 0.68        | 144    | 5.3               | 3.16                 | 8.46                  | 1794     |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
|                      |         |          |                          |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
| RUIR (all)           | 238     |          |                          |        |     |                 |               |       |             | <u> </u>    |        |                   |                      |                       | 0500     |
| Flow adj. Qadj :     |         |          | l otal: 529   Otal: 6596 |        |     |                 |               |       |             |             |        |                   |                      |                       |          |
| Total flow Qtot<br>: | 781     |          |                          |        |     |                 |               | Ave   | erage no. o | f stops/pcu | 0.68   | Ave               | rage interse<br>(sec | ection delay<br>/pcu) | 8.45     |

# The Calculations Of Four Phase (Type 1)

### 1. Very High Traffic Flow

|           |         |           |               |           | TRAFFIC     | FLOW MOT   | ORISED VEH | IICLES (MV)    |                 |                 |
|-----------|---------|-----------|---------------|-----------|-------------|------------|------------|----------------|-----------------|-----------------|
|           |         | Light Veh | nicles (LV)   | Heavy Ve  | hicles (HV) | Motorcycle | es (MC)    | Total          |                 | Patio           |
|           |         | pce prote | ected = $1.0$ | pce prote | cted = 1.3  | pce protec | ted = 0.2  | Motor          |                 | of              |
| Appr code | Dir.    | рсе орро  | sed = 1.0     | pce oppo  | sed = 1.3   | pce oppos  | ed = 0.4   | vehicles<br>MV | t               | urning          |
|           |         | veh/h     | pcu/h         | veh/h     | pcu/h       | veh/h      | pcu/h      | pcu/h          | р <sub>LT</sub> | р <sub>кт</sub> |
|           |         |           | Орр           |           | Орр         |            | Орр        | Орр            | Eq.(13)         | Eq.(14)         |
| (1)       | (2)     | (3)       | (4)           | (5)       | (6)         | (7)        | (8)        | (9)            | (10)            | (11)            |
| N         | LT/LTOR | 109       | 109           | 68        | 88          | 5          | 2          | 199            | 0.21            |                 |
|           | ST      | 465       | 465           | 78        | 101         | 3          | 1          | 567            |                 |                 |
|           | RT      | 140       | 140           | 47        | 61          | 3          | 1          | 202            |                 | 0.21            |
|           | TOTAL   |           |               |           |             |            |            | 968            |                 |                 |
| S         | LT/LTOR | 104       | 104           | 62        | 81          | 4          | 2          | 187            | 0.26            |                 |
|           | ST      | 236       | 236           | 99        | 129         | 4          | 2          | 367            |                 |                 |
|           | RT      | 88        | 88            | 55        | 72          | 3          | 1          | 161            |                 | 0.23            |
|           | TOTAL   |           |               |           |             |            |            | 715            |                 |                 |
| E         | LT/LTOR | 164       | 164           | 113       | 147         | 5          | 2          | 313            | 0.24            |                 |
|           | ST      | 443       | 443           | 150       | 195         | 5          | 2          | 640            |                 |                 |
|           | RT      | 202       | 202           | 98        | 127         | 4          | 2          | 331            |                 | 0.26            |
|           | TOTAL   |           |               |           |             |            |            | 1284           |                 |                 |
| W         | LT/LTOR | 145       | 145           | 84        | 109         | 10         | 4          | 258            | 0.23            |                 |
|           | ST      | 413       | 413           | 132       | 172         | 6          | 2          | 587            |                 |                 |
|           | RT      | 137       | 137           | 90        | 117         | 6          | 2          | 256            |                 | 0.23            |
|           | TOTAL   |           |               |           |             |            |            | 1101           |                 |                 |



| Appr      | Green        | Appr |      | Ratio    | )       | Eff         |            |      |          | Sat        | uration f | low pcı | ı/h            |          | Traffic             | Flow  | Phase  | Green | Capacity | Degree     |
|-----------|--------------|------|------|----------|---------|-------------|------------|------|----------|------------|-----------|---------|----------------|----------|---------------------|-------|--------|-------|----------|------------|
| Code      | In           | type | (    | of turni | ng      | width       | Base       |      |          | Adjustment | factors   |         |                | Adjusted | Flow                | ratio | Ratio  | Time  | pcu/h    | Of         |
|           | Phase        |      |      | vehicle  | es      | (m)         | Value      |      | All a    | ppr type   |           | Only    | type p         | Value    | pcu/h               | FR    | PR =   | Sec   | S x g/c  | Saturation |
|           | no           |      |      |          |         |             | pcu/h      | City | Side     | Gradient   | Parking   | Right   | Lift           | pcu/h    |                     |       | FRcrit |       |          |            |
|           |              |      |      |          |         |             |            | size | Friction |            |           | Turns   | Turns          |          |                     |       |        |       |          |            |
|           |              |      | Ρ    | D        | Dat     | ۱۸/         | c          | Faa  | For      | Fa         | Fa        | Ent     | E              | c        | 0                   | 0/9   | IED    | 0     | C        | OVC        |
|           |              |      | LTOR | 1 LI     | IRI     | vve         | 0.         | 1.05 | 1 SF     | IG         | IP        | IRI     | 1 []           | 0        | Q                   | Q/0   |        | 9     | U        | Q/U        |
|           |              |      |      |          |         |             |            |      |          |            |           |         |                |          |                     |       |        |       |          |            |
|           |              |      |      |          |         |             |            |      |          |            |           |         |                |          |                     |       |        |       |          |            |
| (1)       | (0)          |      |      | (-)      |         | <i>(</i> _) |            | (0)  | (10)     | (1.1)      | (10)      | (10)    | <i>(</i> , , , |          | (4.0)               |       | (10)   | (10)  | (0.0)    | (0.1)      |
| (1)       | (2)          | (3)  | (4)  | (5)      | (6)     | (/)         | (8)        | (9)  | (10)     | (11)       | (12)      | (13)    | (14)           | (15)     | (16)                | (17)  | (18)   | (19)  | (20)     | (21)       |
| Ν         |              | Ρ    |      | 0.21     | 0.21    | 8           | 4800       | 1.00 | 0.95     | 1.00       | 1.00      | 1.054   | 0.966          | 4646     | 968                 | 0.208 | 0.257  | 35    | 1070     | 0.9        |
| S         |              | Ρ    |      | 0.26     | 0.23    | 8           | 4800       | 1.00 | 0.98     | 1.00       | 1.00      | 1.059   | 0.958          | 4778     | 715                 | 0.149 | 0.185  | 25    | 786      | 0.91       |
| Е         |              | Р    |      | 0.24     | 0.26    | 9           | 5400       | 1.00 | 0.95     | 1.00       | 1.00      | 1.067   | 0.962          | 5267     | 1284                | 0.24  | 0.297  | 41    | 1421     | 0.90       |
| W         |              | р    |      | 0.23     | 0.23    | 9           | 5400       | 1.00 | 0.95     | 1.00       | 1.00      | 1.058   | 0.963          | 5232     | 1101                | 0.21  | 0.26   | 35    | 1205     | 0.91       |
| Tot       | al lost      | 16   |      | Unadju   | stment  | cycle tin   | ne Cus (se | ec)  | 151      |            |           |         |                |          | IFR=                |       |        |       |          |            |
| ti<br>LTI | ime<br>(sec) | Sec  |      | Adjus    | tment c | cycle time  | e C (seo   | C)   | 153      |            |           |         |                |          | ∑FR <sub>CRIT</sub> | 0.808 |        |       |          |            |

| Approach             | Traffic | Capacity | Degree of  | Green | No              | . of queuir     | ng vehicles | (pcu) | Queue       | Stop        | No. of | Delay         |                    |                       |         |
|----------------------|---------|----------|------------|-------|-----------------|-----------------|-------------|-------|-------------|-------------|--------|---------------|--------------------|-----------------------|---------|
| Code                 | flow    | pcu/h    | Saturation | Ratio |                 |                 |             |       | length      | rate        | Stops  | Average       | Average            | Average delay         | Total   |
|                      | pcu/h   |          | DS         | GR    | NQ <sub>1</sub> | NQ <sub>2</sub> | Total       | NQMAX | (m)         | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delay | sec/pcu               | Delay   |
|                      |         |          | =          | =     |                 |                 | NQ1+NQ2     |       |             |             |        | sec/pcu       | sec/pcu            | D =                   | Pcu.sec |
|                      | Q       | С        | Q/C        | g/c   |                 |                 | NQ          |       | QL          | NS          | Nsv    | DT            | DĠ                 | DT+DG                 | DxQ     |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6)             | (7)             | (8)         | (9)   | (10)        | (11)        | (12)   | (13)          | (14)               | (15)                  | (16)    |
| N                    | 968     | 1070     | 0.90       | 0.23  | 3.74            | 39.68           | 43.42       | 60    | 150         | 0.96        | 929    | 69.40         | 3.89               | 73.29                 | 70945   |
| S                    | 715     | 786      | 0.91       | 0.16  | 4.10            | 29.68           | 33.78       | 48    | 120         | 1.00        | 715    | 81.50         | 4.00               | 85.5                  | 61133   |
| E                    | 1284    | 1421     | 0.90       | 0.27  | 3.80            | 52.3            | 56.10       | 78    | 173         | 0.93        | 1194   | 63.13         | 3.83               | 66.96                 | 85977   |
| W                    | 1101    | 1205     | 0.91       | 0.23  | 4.23            | 45.3            | 49.53       | 69    | 153         | 0.93        | 1024   | 57.70         | 3.82               | 61.52                 | 67734   |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
|                      |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
| ROTR (all)           |         |          |            |       |                 |                 |             |       |             |             |        |               |                    |                       |         |
| Flow adj. Qadj :     |         | ]        |            |       |                 |                 |             |       |             | Total:      | 3862   |               |                    | Total                 | 285789  |
| Total flow Qtot<br>: | 4068    |          |            |       |                 |                 |             | Ave   | erage no. o | f stops/pcu | 0.95   | Avera         | ge interse<br>(seo | ction delay<br>c/pcu) | 70.25   |

## 2. High Traffic Flow

| App. code | Dir.    | Total<br>Motor vehicles<br>MV |                 | Ratio<br>of<br>turning |
|-----------|---------|-------------------------------|-----------------|------------------------|
|           |         | pcu/h                         | р <sub>LT</sub> | р <sub>кт</sub>        |
|           |         | Орр                           | Eq.(13)         | Eq.(14)                |
| (1)       | (2)     | (9)                           | (10)            | (11)                   |
| N         | LT/LTOR | 149                           | 0.21            |                        |
|           | ST      | 425                           |                 |                        |
|           | RT      | 152                           |                 | 0.21                   |
|           | TOTAL   | 726                           |                 |                        |
| S         | LT/LTOR | 140                           | 0.26            |                        |
|           | ST      | 275                           |                 |                        |
|           | RT      | 121                           |                 | 0.23                   |
|           | TOTAL   | 536                           |                 |                        |
| Ε         | LT/LTOR | 235                           | 0.24            |                        |
|           | ST      | 480                           |                 |                        |
|           | RT      | 248                           |                 | 0.26                   |
|           | TOTAL   | 963                           |                 |                        |
| W         | LT/LTOR | 194                           | 0.23            |                        |
|           | ST      | 440                           |                 |                        |
|           | RT      | 192                           |                 | 0.23                   |
|           | TOTAL   | 826                           |                 |                        |



| Appr | Green | Appr |      | Ratio    | )    | Eff      |       |      |          | Sat        | uration f | low pci | u/h    |          | Traffic | Flow                | Phase  | Green | Capacity | Degree     |
|------|-------|------|------|----------|------|----------|-------|------|----------|------------|-----------|---------|--------|----------|---------|---------------------|--------|-------|----------|------------|
| Code | e In  | type | C    | of turni | ng   | width    | Base  |      |          | Adjustment | factors   |         |        | Adjusted | Flow    | ratio               | Ratio  | Time  | pcu/h    | Of         |
|      | Phase |      |      | vehicle  | es   | (m)      | Value |      | All a    | ippr type  |           | Only    | type p | Value    | pcu/h   | FR                  | PR =   | Sec   | S x g/c  | Saturation |
|      | no    |      |      |          |      |          | pcu/h | City | Side     | Gradient   | Parking   | Right   | Lift   | pcu/h    |         |                     | FRcrit |       |          |            |
|      |       |      |      |          |      |          |       | size | Friction |            |           | Turns   | Turns  |          |         |                     |        |       |          |            |
|      |       |      | Ρ    | D        | D    | \٨/      | c     | Faa  | E        | E.         | E-        | F       | E      | S        | 0       | 2/0                 | IED    | 0     | C        | OIC        |
|      |       |      | LTOR | ' LI     | I RI | vve      | 0.    | I CS | I SF     | IG         | IР        | I RI    | ' L I  | 3        | Q       | Q/0                 |        | y     | U        | QIU        |
|      |       |      |      |          |      |          |       |      |          |            |           |         |        |          |         |                     |        |       |          |            |
|      |       |      |      |          |      |          |       |      |          |            |           |         |        |          |         |                     |        |       |          |            |
|      | (.)   |      |      |          |      | <i>—</i> | 6.5   |      |          |            |           |         |        |          |         | <i>.</i> _ <b>.</b> |        |       | 6.0      | 6.3        |
| (1)  | (2)   | (3)  | (4)  | (5)      | (6)  | (7)      | (8)   | (9)  | (10)     | (11)       | (12)      | (13)    | (14)   | (15)     | (16)    | (17)                | (18)   | (19)  | (20)     | (21)       |
| Ν    |       | Ρ    |      | 0.21     | 0.21 | 8        | 4800  | 1.00 | 0.95     | 1.00       | 1.00      | 1.054   | 0.966  | 4646     | 726     | 0.16                | 0.26   | 16    | 965      | 0.75       |
| S    |       | Ρ    |      | 0.26     | 0.23 | 8        | 4800  | 1.00 | 0.98     | 1.00       | 1.00      | 1.059   | 0.958  | 4778     | 536     | 0.11                | 0.18   | 11    | 683      | 0.78       |
| E    |       | Ρ    |      | 0.24     | 0.26 | 9        | 5400  | 1.00 | 0.95     | 1.00       | 1.00      | 1.067   | 0.962  | 5267     | 961     | 0.19                | 0.30   | 18    | 1231     | 0.78       |
| W    |       | р    |      | 0.23     | 0.23 | 9        | 5400  | 1.00 | 0.95     | 1.00       | 1.00      | 1.058   | 0.963  | 5232     | 823     | 0.16                | 0.26   | 16    | 1087     | 0.76       |

| Total lost    | 16    | Ur      | nadjustmen                 | t cycle time | Cus (sec) | )    | 76     |                 |               |       |              |           | IFR=   |        |               |              |             |               |          |
|---------------|-------|---------|----------------------------|--------------|-----------|------|--------|-----------------|---------------|-------|--------------|-----------|--------|--------|---------------|--------------|-------------|---------------|----------|
| LTI (sec)     | Sec   | ŀ       | Adjustment                 | cycle time ( | C (sec)   |      | 77     |                 |               |       |              | Σ         | FRCRIT | 0.62   |               |              |             |               |          |
| Approach      |       | Traffic | Capacity                   | Degree of    | Green     | ١    | lo. of | queuing         | g vehicles (p | ocu)  | Queue        | Stop      | N      | o. of  | Delay         |              |             |               |          |
| Code          |       | flow    | pcu/h                      | Saturation   | Ratio     |      |        |                 |               |       | length       | rate      | S      | tops   | Average       | Avera        | age         | Average delay | Total    |
|               |       | pcu/h   |                            | DS           | GR        | NQ1  |        | NQ <sub>2</sub> | Total         | NQMAX | (m)          | stops/p   | ocu p  | cu/h   | Traffic delay | Geom<br>dela | etric<br>av | sec/pcu       | Delay    |
|               |       |         |                            | =            | =         |      |        |                 | $NQ_1+NQ_2$   |       |              |           |        |        | sec/pcu       | sec/p        | ocu         | D =           | Pcu.sec  |
|               |       | Q       | С                          | Q/C          | g/c       |      |        |                 | NQ            |       | QL           | NS        | 1      | Nsv    | DT            | DC           | 3           | DT+DG         | DxQ      |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             | (13)+(14)     | (2)+(15) |
| (1)           |       | (2)     | (3)                        | (4)          | (5)       | (6)  |        | (7)             | (8)           | (9)   | (10)         | (11)      | (      | 12)    | (13)          | (14          | I)          | (15)          | (16)     |
| N             |       | 726     | 965                        | 0.75         | 0.21      | 1.61 | 1      | 14.63           | 16.24         | 24    | 60           | 0.94      | 6      | 682    | 34.78         | 3.8          | 4           | 38.62         | 28038    |
| S             |       | 536     | 683                        | 0.78         | 0.14      | 1.47 | 1      | 11.10           | 12.57         | 20    | 50           | 0.99      | Ę      | 531    | 39.94         | 3.9          | 7           | 43.91         | 23536    |
| E             |       | 961     | 1231                       | 0.78         | 0.23      | 1.48 | 1      | 19.40           | 20.88         | 30    | 67           | 0.91      | 8      | 375    | 33.52         | 3.7          | 8           | 37.30         | 35845    |
| W             |       | 823     | 1087                       | 0.76         | 0.21      | 1.16 | 1      | 16.60           | 17.76         | 26    | 58           | 0.91      | 7      | 749    | 32.58         | 3.7          | 6           | 36.34         | 29908    |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       |         |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
|               |       | 2014    |                            |              |           |      |        |                 |               |       |              |           |        |        |               |              |             |               |          |
| Flow adi Oa   | di ·  | 3040    |                            |              |           |      |        |                 |               |       |              | Tot       | tal: 2 | 837    |               |              |             | Total         | 117307   |
| i iuw auj. Qa | iuj.  |         | Average intersection delay |              |           |      |        |                 |               |       |              |           |        | 11/32/ |               |              |             |               |          |
| Total flow Q  | tot : | 3046    |                            |              |           |      |        |                 |               | A     | verage no. o | f stops/p | ocu C  | .93    | AV            | erage in     | (sec/j      | pcu)          | 38.52    |

### 3. Low Traffic Flow

|           |         | Total<br>Motor vehicles | R       | atio<br>of             |
|-----------|---------|-------------------------|---------|------------------------|
| Appr code | Dir.    | MV                      | tur     | ning                   |
|           |         | pcu/h                   | рьт     | <b>р</b> <sub>RT</sub> |
|           |         | Орр                     | Eq.(13) | Eq.(14)                |
|           | (2)     | (9)                     | (10)    | (11)                   |
| Ν         | LT/LTOR | 100                     | 0.21    |                        |
|           | ST      | 284                     |         |                        |
|           | RT      | 101                     |         | 0.21                   |
|           | TOTAL   | 485                     |         |                        |
| S         | LT/LTOR | 94                      | 0.26    |                        |
|           | ST      | 184                     |         |                        |
|           | RT      | 81                      |         | 0.23                   |
|           | TOTAL   | 359                     |         |                        |
| E         | LT/LTOR | 157                     | 0.24    |                        |
|           | ST      | 320                     |         |                        |
|           | RT      | 166                     |         | 0.26                   |
|           | TOTAL   | 643                     |         |                        |
| W         | LT/LTOR | 129                     | 0.23    |                        |
|           | ST      | 294                     |         |                        |
|           | RT      | 128                     |         | 0.23                   |
|           | TOTAL   | 551                     |         |                        |



| А | ppr ( | Green | Appr |      | Ratic    | )    | Eff   |       |          |          | Sat        | uration f | low pci | ı/h    |          | Traffic | Flow  | Phase  | Green    | Capacity | Degree     |
|---|-------|-------|------|------|----------|------|-------|-------|----------|----------|------------|-----------|---------|--------|----------|---------|-------|--------|----------|----------|------------|
| С | ode   | In    | type | 0    | of turni | ng   | width | Base  |          |          | Adjustment | t factors |         |        | Adjusted | Flow    | ratio | Ratio  | Time     | pcu/h    | Of         |
|   | F     | Phase |      |      | vehicle  | es   | (m)   | Value |          | All a    | ippr type  |           | Only    | type p | Value    | pcu/h   | FR    | PR =   | Sec      | S x g/c  | Saturation |
|   |       | no    |      |      |          |      |       | pcu/h | City     | Side     | Gradient   | Parking   | Right   | Lift   | pcu/h    |         |       | FRcrit |          |          |            |
|   |       |       |      |      |          |      |       |       | size     | Friction |            |           | Turns   | Turns  |          |         |       |        |          |          |            |
|   |       |       |      | Р    | D        | D    | ۱۸/   | c     | <b>E</b> | E        | E.         | E-        | E       | E      | c        | 0       | 0/9   |        | <b>a</b> | C        | 0/0        |
|   |       |       |      | LTOR | FLT      | F RT | ۷Ve   | 30    | ГCS      | ΓSF      | ГG         | ГР        | FRT     | FLT    | 3        | Q       | Q/3   | IFK    | y        | U        |            |
|   |       |       |      |      |          |      |       |       |          |          |            |           |         |        |          |         |       |        |          |          |            |
|   |       |       |      |      |          |      |       |       |          |          |            |           |         |        |          |         |       |        |          |          |            |
|   |       |       |      |      |          |      |       |       |          |          |            |           |         |        |          |         |       |        |          |          |            |
| ( | (1)   | (2)   | (3)  | (4)  | (5)      | (6)  | (7)   | (8)   | (9)      | (10)     | (11)       | (12)      | (13)    | (14)   | (15)     | (16)    | (17)  | (18)   | (19)     | (20)     | (21)       |
|   | Ν     |       | Ρ    |      | 0.21     | 0.21 | 8     | 4800  | 1.00     | 0.95     | 1.00       | 1.00      | 1.054   | 0.966  | 4646     | 485     | 0.11  | 0.261  | 9        | 805      | 0.6        |
|   | S     |       | Ρ    |      | 0.26     | 0.23 | 8     | 4800  | 1.00     | 0.98     | 1.00       | 1.00      | 1.059   | 0.958  | 4778     | 359     | 0.082 | 0.195  | 7        | 646      | 0.56       |
|   | E     |       | Ρ    |      | 0.24     | 0.26 | 9     | 5400  | 1.00     | 0.95     | 1.00       | 1.00      | 1.067   | 0.962  | 5267     | 643     | 0.125 | 0.30   | 10       | 1006     | 0.64       |
| 1 | W     |       | р    |      | 0.23     | 0.23 | 9     | 5400  | 1.00     | 0.95     | 1.00       | 1.00      | 1.058   | 0.963  | 5232     | 551     | 0.11  | 0.261  | 9        | 905      | 0.61       |

| Total lost        | 16  | Unadjustment cycle time Cus (sec) | 50 |  |  | IFR=                |       |  |  |
|-------------------|-----|-----------------------------------|----|--|--|---------------------|-------|--|--|
| time<br>LTI (sec) | Sec | Adjustment cycle time C (sec)     | 51 |  |  | ∑FR <sub>CRIT</sub> | 0.421 |  |  |

| Approach             | Traffic | Capacity | Degree of                | Green | N               | o. of queuir    | ng vehicles (p | ocu)  | Queue      | Stop        | No. of | Delay         |   |               |          |  |  |  |  |  |
|----------------------|---------|----------|--------------------------|-------|-----------------|-----------------|----------------|-------|------------|-------------|--------|---------------|---|---------------|----------|--|--|--|--|--|
| Code                 | Flow    | pcu/h    | Saturation               | Ratio |                 |                 |                |       | length     | rate        | Stops  | Average       | Average   | Average delay | Total    |  |  |  |  |  |
|                      | pcu/h   |          | DS                       | GR    | NQ <sub>1</sub> | NQ <sub>2</sub> | Total          | NQMAX | (m)        | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delay  | sec/pcu       | Delay    |  |  |  |  |  |
|                      |         |          | =                        | =     |                 |                 | $NQ_1 + NQ_2$  |       |            |             |        | sec/pcu       | sec/pcu   | D =           | Pcu.sec  |  |  |  |  |  |
|                      | Q       | С        | Q/C                      | g/c   |                 |                 | NQ             |       | QL         | NS          | Nsv    | DT            | DG  | DT+DG         | DxQ      |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   | (13)+(14)     | (2)+(15) |  |  |  |  |  |
| (1)                  | (2)     | (3)      | (4)                      | (5)   | (6)             | (7)             | (8)            | (9)   | (10)       | (11)        | (12)   | (13)          | (14)  | (15)          | (16)     |  |  |  |  |  |
| N                    | 485     | 805      | 0.6                      | 0.18  | 0.25            | 6.32            | 6.57           | 12    | 20         | 0.86        | 417    | 20.34         | 3.62  | 23.96         | 11621    |  |  |  |  |  |
| S                    | 359     | 646      | 0.56                     | 0.14  | 0.14            | 4.80            | 4.94           | 9     | 23         | 0.87        | 314    | 21.24         | 3.67  | 24.91         | 8943     |  |  |  |  |  |
| E                    | 643     | 1006     | 0.64                     | 0.20  | 0.40            | 8.36            | 8.76           | 14    | 31         | 0.867       | 556    | 20.15         | 3.67  | 23.82         | 15316    |  |  |  |  |  |
| W                    | 551     | 905      | 0.61                     | 0.18  | 0.28            | 7.19            | 7.47           | 13    | 29         | 0.86        | 474    | 20.37         | 3.63  | 24            | 13224    |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
|                      |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
| ROTR (all)           |         |          |                          |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
| Flow adj. Qadj :     |         |          | Total: 1761 Total: 49104 |       |                 |                 |                |       |            |             |        |               |   |               |          |  |  |  |  |  |
| Total flow Qtot<br>: | 2038    |          |                          |       |                 |                 |                | Ave   | rage no. o | f stops/pcu | 0.864  | Ave           | Total: 49104<br>Average intersection delay<br>(sec/pcu) 24.10 |               |          |  |  |  |  |  |

### 4. Very Low Traffic Flow

|           |         | Total<br>Motor |         | Ratio   |
|-----------|---------|----------------|---------|---------|
| Appr code | Dir     | vehicles       |         | of      |
| Appi couc | Dir.    | MV             |         | turning |
|           |         | ncu/h          |         | tarning |
|           |         | poun           | ріт     | D PT    |
|           |         | Opp            | Eq.(13) | Eq.(14) |
| (1)       | (2)     | (9)            | (10)    | (11)    |
| N         | LT/LTOR | 50             | 0.21    |         |
|           | ST      | 142            |         |         |
|           | RT      | 51             |         | 0.21    |
|           | TOTAL   | 243            |         |         |
| S         | LT/LTOR | 47             | 0.26    |         |
|           | ST      | 92             |         |         |
|           | RT      | 40             |         | 0.23    |
|           | TOTAL   | 179            |         |         |
| E         | LT/LTOR | 78             | 0.24    |         |
|           | ST      | 160            |         |         |
|           | RT      | 83             |         | 0.26    |
|           | TOTAL   | 321            |         |         |
| W         | LT/LTOR | 65             | 0.23    |         |
|           | ST      | 147            |         |         |
| Ν         | RT      | 64             |         | 0.23    |
|           | TOTAL   | 276            |         |         |



| Α | Appr | Green | Appr |      | Ratic    | )        | Eff   |       |      |          | Sat        | uration f | flow pcu | ı/h    |          | Traffic | Flow  | Phase  | Green | Capacity | Degree     |
|---|------|-------|------|------|----------|----------|-------|-------|------|----------|------------|-----------|----------|--------|----------|---------|-------|--------|-------|----------|------------|
| С | code | In    | type | C    | of turni | ng       | width | Base  |      |          | Adjustment | t factors |          |        | Adjusted | Flow    | ratio | Ratio  | Time  | pcu/h    | Of         |
|   |      | Phase |      |      | vehicle  | es       | (m)   | Value |      | All a    | ippr type  |           | Only     | type p | Value    | pcu/h   | FR    | PR =   | Sec   | S x g/c  | Saturation |
|   |      | no    |      |      |          |          |       | pcu/h | City | Side     | Gradient   | Parking   | Right    | Lift   | pcu/h    |         |       | FRcrit |       |          |            |
|   |      |       |      |      |          |          |       |       | size | Friction |            |           | Turns    | Turns  |          |         |       |        |       |          |            |
|   |      |       |      | Р    | P.T      | Рат      | W.    | S     | Foo  | For      | Fa         | Fa        | For      | F      | S        | 0       | 0/5   | IFR    | a     | C        | 0/0        |
|   |      |       |      | LTOR | • LI     | I RI     | vve   | 0.    | 1.05 | · 5F     | I G        | 1 P       | I RI     | • []   | 0        | Q       | Q/O   |        | 9     | Ŭ        | QIU        |
|   |      |       |      |      |          |          |       |       |      |          |            |           |          |        |          |         |       |        |       |          |            |
|   |      |       |      |      |          |          |       |       |      |          |            |           |          |        |          |         |       |        |       |          |            |
|   | (1)  | (2)   | (2)  |      | /F)      | <i>w</i> | (7)   | (0)   | (0)  | (10)     | (11)       | (10)      | (10)     | (1 1)  | (45)     | (1)     | (17)  | (10)   | (10)  | (20)     | (01)       |
|   | (1)  | (2)   | (3)  | (4)  | (5)      | (6)      | (/)   | (8)   | (9)  | (10)     | (11)       | (12)      | (13)     | (14)   | (15)     | (16)    | (17)  | (18)   | (19)  | (20)     | (21)       |
|   | Ν    |       | Ρ    |      | 0.21     | 0.21     | 8     | 4800  | 1.00 | 0.95     | 1.00       | 1.00      | 1.054    | 0.966  | 4646     | 243     | 0.052 | 0.26   | 5     | 645      | 0.38       |
|   | S    |       | Р    |      | 0.26     | 0.23     | 8     | 4800  | 1.00 | 0.98     | 1.00       | 1.00      | 1.059    | 0.958  | 4778     | 179     | 0.037 | 0.18   | 4     | 531      | 0.24       |
|   | Ε    |       | Ρ    |      | 0.24     | 0.26     | 9     | 5400  | 1.00 | 0.95     | 1.00       | 1.00      | 1.067    | 0.962  | 5267     | 321     | 0.061 | 0.30   | 6     | 1024     | 0.38       |

| W          | р   | 0.23 0.23 9            | 5400 1.00    | 0.95 | 1.00 | 1.00 | 1.058 | 0.963 | 5232 | 275                 | 0.053 | 0.26 | 5 | 727 | 0.33 |
|------------|-----|------------------------|--------------|------|------|------|-------|-------|------|---------------------|-------|------|---|-----|------|
| Total lost | 16  | Unadjustment cycle tim | ne Cus (sec) | 36   |      |      |       |       |      | IFR=                |       |      |   |     |      |
| LTI (sec)  | Sec | Adjustment cycle time  | e C (sec)    | 36   |      |      |       |       |      | ∑FR <sub>CRIT</sub> | 0.203 |      |   |     |      |

| Approach             | Traffic | Capacity | Degree of  | Green | No              | . of queuing    | g vehicles ( | ocu)  | Queue       | Stop        | No. of | Delay         |                       |                      |          |
|----------------------|---------|----------|------------|-------|-----------------|-----------------|--------------|-------|-------------|-------------|--------|---------------|-----------------------|----------------------|----------|
| Code                 | Flow    | pcu/h    | Saturation | Ratio |                 |                 |              |       | length      | rate        | Stops  | Average       | Average               | Average delay        | Total    |
|                      | pcu/h   |          | DS         | GR    | NQ <sub>1</sub> | NQ <sub>2</sub> | Total        | NQMAX | (m)         | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delay    | sec/pcu              | Delay    |
|                      |         |          | =          | =     |                 |                 | $NQ_1+NQ_2$  |       |             |             |        | sec/pcu       | sec/pcu               | D =                  | Pcu.sec  |
|                      | Q       | С        | Q/C        | g/c   |                 |                 | NQ           |       | QL          | NS          | Nsv    | DT            | DG                    | DT+DG                | DxQ      |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       | (13)+(14)            | (2)+(15) |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6)             | (7)             | (8)          | (9)   | (10)        | (11)        | (12)   | (13)          | (14)                  | (15)                 | (16)     |
| N                    | 243     | 645      | 0.38       | 0.14  | 0               | 2.21            | 2.21         | 5.5   | 14          | 0.82        | 199    | 14.10         | 3.51                  | 17.61                | 4279     |
| S                    | 179     | 531      | 0.24       | 0.11  | 0               | 1.65            | 1.65         | 4     | 10          | 0.83        | 149    | 14.80         | 3.55                  | 18.35                | 3285     |
| E                    | 321     | 1024     | 0.38       | 0.17  | 0               | 2.81            | 2.81         | 7     | 16          | 0.79        | 254    | 13.10         | 3.49                  | 16.59                | 5325     |
| W                    | 275     | 727      | 0.33       | 0.14  | 0               | 2.50            | 2.50         | 6     | 13          | 0.82        | 226    | 14.10         | 3.53                  | 17.63                | 4848     |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
|                      |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
| ROTR (all)           |         |          |            |       |                 |                 |              |       |             |             |        |               |                       |                      |          |
| Flow adj. Qadj :     |         | ļ        |            |       |                 |                 |              |       |             | Total:      | 828    | ļ             |                       | Total:               | 17737    |
| Total flow Qtot<br>: | 1018    |          |            |       |                 |                 |              | Ave   | erage no. o | f stops/pcu | 0.81   | Ave           | rage interse<br>/sec/ | ction delay<br>/pcu) | 17.42    |

# The Calculations Of Four Phase (Type 2)

### 1. Very High Traffic Flow

|           |         |           |             |           | TRAFFIC     | FLOW MOT   | ORISED VEH | IICLES (MV)    |                 |                 |
|-----------|---------|-----------|-------------|-----------|-------------|------------|------------|----------------|-----------------|-----------------|
|           |         | Light Veh | nicles (LV) | Heavy Ve  | hicles (HV) | Motorcycle | es (MC)    | Total          |                 | Datio           |
|           |         | pce prote | ected = 1.0 | pce prote | cted = 1.3  | pce protec | ted = 0.2  | Motor          |                 | of              |
| Appr code | Dir.    | рсе орро  | sed = 1.0   | pce oppo  | sed = 1.3   | pce oppos  | ed = 0.4   | vehicles<br>MV | t               | urning          |
|           |         | veh/h     | pcu/h       | veh/h     | pcu/h       | veh/h      | pcu/h      | pcu/h          | р <sub>LT</sub> | р <sub>кт</sub> |
|           |         |           | Орр         |           | Орр         |            | Орр        | Орр            | Eq.(13)         | Eq.(14)         |
| (1)       | (2)     | (3)       | (4)         | (5)       | (6)         | (7)        | (8)        | (9)            | (10)            | (11)            |
| N         | LT/LTOR | 109       | 109         | 68        | 88          | 5          | 2          | 199            | 0.21            |                 |
|           | ST      | 465       | 465         | 78        | 101         | 3          | 1          | 567            |                 |                 |
|           | RT      | 140       | 140         | 47        | 61          | 3          | 1          | 202            |                 | 0.21            |
|           | TOTAL   |           |             |           |             |            |            | 968            |                 |                 |
| S         | LT/LTOR | 104       | 104         | 62        | 81          | 4          | 2          | 187            | 0.26            |                 |
|           | ST      | 236       | 236         | 99        | 129         | 4          | 2          | 367            |                 |                 |
|           | RT      | 88        | 88          | 55        | 72          | 3          | 1          | 161            |                 | 0.23            |
|           | TOTAL   |           |             |           |             |            |            | 715            |                 |                 |
| E         | LT/LTOR | 164       | 164         | 113       | 147         | 5          | 2          | 313            | 0.24            |                 |
|           | ST      | 443       | 443         | 150       | 195         | 5          | 2          | 640            |                 |                 |
|           | RT      | 202       | 202         | 98        | 127         | 4          | 2          | 331            |                 | 0.26            |
|           | TOTAL   |           |             |           |             |            |            | 1284           |                 |                 |
| W         | LT/LTOR | 145       | 145         | 84        | 109         | 10         | 4          | 258            | 0.23            |                 |
|           | ST      | 413       | 413         | 132       | 172         | 6          | 2          | 587            |                 |                 |
|           | RT      | 137       | 137         | 90        | 117         | 6          | 2          | 256            |                 | 0.23            |
|           | TOTAL   |           |             |           |             |            |            | 1101           |                 |                 |



| Арр  | r Green | Appr |        | Ratic    | )    | Eff   |       |      |          | S        | Saturation | n flow pc | u/h    |          | Traffic | Flow  | Phase  | Green | Capacity | Degree     |
|------|---------|------|--------|----------|------|-------|-------|------|----------|----------|------------|-----------|--------|----------|---------|-------|--------|-------|----------|------------|
| Code | e In    | type | 0      | of turni | ng   | width | Base  |      |          | Adjustme | ent factor | S         |        | Adjusted | Flow    | ratio | Ratio  | Time  | pcu/h    | Ōf         |
|      | Phase   |      | ۱<br>۱ | vehicle  | es   | (m)   | Value |      | All a    | ppr type |            | Only      | type p | Value    | pcu/h   | FR    | PR =   | Sec   | S x g/c  | Saturation |
|      | no      |      |        |          |      |       | pcu/h | City | Side     | Gradient | Parking    | Right     | Lift   | pcu/h    |         |       | FRcrit |       |          |            |
|      |         |      |        |          |      |       |       | Size | Friction |          |            | Turns     | Turns  |          |         |       | [      |       |          |            |
|      |         |      | Р      | D        | D    | \M/   | c     | Faa  | For      | Ea       | E.         | Ear       | E      | S        | 0       | 0/9   | IED    | 0     | C        | OIC        |
|      |         |      | LTOR   | ' LI     | I RI | vve   | 0.    | TCS  | I SF     | ΙG       | ΙP         | I RI      | I []   | 5        | Q       | Q/3   |        | y     | U        | Q/C        |
|      |         |      |        |          |      |       |       |      |          |          |            |           |        |          |         |       |        |       |          |            |
|      |         |      |        |          |      |       |       |      |          |          |            |           |        |          |         |       |        |       |          |            |
|      | (0)     | (0)  |        | (=)      |      | ()    | (0)   | (0)  | (10)     | (1.1)    | (10)       | (10)      | (4.1)  | (45)     | (4.1)   | (47)  | (10)   | (10)  | (0.0)    | (04)       |
| (1)  | (2)     | (3)  | (4)    | (5)      | (6)  | (/)   | (8)   | (9)  | (10)     | (11)     | (12)       | (13)      | (14)   | (15)     | (16)    | (17)  | (18)   | (19)  | (20)     | (21)       |
| Ν    | 1       | Ρ    |        |          |      | 5     | 3000  | 1.00 | 0.95     | 1.00     | 1.00       | 1.054     | 0.9664 | 2903     | 769     | 0.265 | 0.32   | 51    | 846      | 0.91       |
| S    | 1       | р    |        |          |      | 5     | 3000  | 1.00 | 0.98     | 1.00     | 1.00       | 1.0598    | 0.9584 | 2986     | 528     | 0.177 |        | 51    | 870      | 0.61       |
| Ν    | 2       | Р    |        |          |      | 3     | 1800  | 1.00 | 0.95     | 1.00     | 1.00       | 1.054     | 0.9664 | 1741     | 199     | 0.114 | 0.14   | 22    | 219      | 0.91       |
| S    | 2       | р    |        |          |      | 3     | 1800  | 1.00 | 0.98     | 1.00     | 1.00       | 1.0598    | 0.9584 | 1792     | 187     | 0.104 |        | 22    | 225      | 0.83       |
| Е    | 2       | р    |        |          |      | 5.5   | 3300  | 1.00 | 0.95     | 1.00     | 1.00       | 1.0676    | 0.9616 | 3218     | 971     | 0.302 | 0.36   | 57    | 1048     | 0.926      |
| W    | 3       | Ρ    |        |          |      | 5.5   | 3300  | 1.00 | 0.95     | 1.00     | 1.00       | 1.0589    | 0.9632 | 3197     | 843     | 0.264 |        | 57    | 1041     | 0.81       |
| Е    | 1       | р    |        |          |      | 3.5   | 2100  | 1.00 | 0.95     | 1.00     | 1.00       | 1.0676    | 0.9616 | 2048     | 313     | 0.153 | 0.18   | 29    | 339      | 0.92       |
| W    | 4       | р    |        |          |      | 3.5   | 2100  | 1.00 | 0.95     | 1.00     | 1.00       | 1.0589    | 0.9632 | 2035     | 258     | 0.126 |        | 29    | 337      | 0.77       |

| Total lost        | 16  | Unadjustment cycle time Cus (sec) | 175 |  |  | IFR=                |       |  |  |
|-------------------|-----|-----------------------------------|-----|--|--|---------------------|-------|--|--|
| time<br>LTI (sec) | Sec | Adjustment cycle time C (sec)     | 175 |  |  | ∑FR <sub>CRIT</sub> | 0.834 |  |  |

| Approach             | Traffic | Capacity | Degree of  | Green | No              | . of queuin     | ig vehicles ( | pcu)  | Queue      | Stop        | No. of | Delay         |                    |                       |         |
|----------------------|---------|----------|------------|-------|-----------------|-----------------|---------------|-------|------------|-------------|--------|---------------|--------------------|-----------------------|---------|
| Code                 | flow    | pcu/h    | Saturation | Ratio |                 |                 |               |       | length     | rate        | Stops  | Average       | Average            | Average delay         | Total   |
|                      | pcu/h   |          | DS         | GR    | NQ <sub>1</sub> | NQ <sub>2</sub> | Total         | NQMAX | (m)        | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delay | sec/pcu               | Delay   |
|                      |         |          | =          | =     |                 |                 | NQ1+NQ2       |       |            |             |        | sec/pcu       | sec/pcu            | D =                   | Pcu.sec |
|                      | Q       | С        | Q/C        | g/c   |                 |                 | NQ            |       | QL         | NS          | Nsv    | DT            | DG                 | DT+DG                 | DxQ     |
|                      |         |          |            |       |                 |                 |               |       |            |             |        |               |                    |                       |         |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6)             | (7)             | (8)           | (9)   | (10)       | (11)        | (12)   | (13)          | (14)               | (15)                  | (16)    |
| N                    | 769     | 846      | 0.91       | 0.29  | 4.11            | 36.1            | 40.21         | 66    | 264        | 0.97        | 746    | 77.41         | 3.92               | 81.33                 | 62543   |
| S                    | 528     | 870      | 0.61       | 0.29  | 0.28            | 22.14           | 22.42         | 32    | 128        | 0.79        | 417    | 54.75         | 3.45               | 58.2                  | 30730   |
| N                    | 199     | 219      | 0.91       | 0.13  | 3.39            | 9.54            | 12.93         | 20    | 133        | 1.20        | 239    | 130.8         | 4.55               | 135.35                | 26935   |
| S                    | 187     | 225      | 0.83       | 0.13  | 1.78            | 8.87            | 10.65         | 17    | 113        | 1.05        | 196    | 102.72        | 4.13               | 106.85                | 19981   |
| E                    | 971     | 1048     | 0.926      | 0.32  | 5.03            | 45.61           | 50.64         | 70    | 255        | 0.965       | 937    | 74.78         | 3.91               | 78.69                 | 76408   |
| W                    | 843     | 1041     | 0.81       | 0.32  | 1.61            | 37.62           | 39.23         | 54    | 196        | 0.86        | 725    | 60.18         | 3.63               | 63.81                 | 53792   |
| E                    | 313     | 339      | 0.92       | 0.17  | 4.04            | 14.97           | 19.01         | 28    | 160        | 1.12        | 351    | 114.36        | 4.29               | 118.65                | 37137   |
| W                    | 258     | 337      | 0.77       | 0.17  | 1.14            | 11.98           | 13.12         | 20    | 114        | 0.94        | 243    | 81.54         | 3.84               | 85.38                 | 22028   |
| ROTR (all)           |         |          |            |       |                 |                 |               |       |            |             |        |               |                    |                       |         |
| Flow adj. Qadj :     |         |          |            |       |                 |                 |               |       |            | Total:      | 3854   |               |                    | Total                 | 329554  |
| Total flow Qtot<br>: | 4068    |          |            |       |                 |                 |               | Ave   | rage no. o | f stops/pcu | 0.95   | Avera         | ge interse<br>(sec | ction delay<br>c/pcu) | 81      |

## 2. High Traffic Flow

| App. code | Dir.    | Total<br>Motor vehicles<br>MV |                 | Ratio<br>of<br>turning |
|-----------|---------|-------------------------------|-----------------|------------------------|
|           |         | pcu/h                         | р <sub>LT</sub> | р <sub> RT</sub>       |
|           |         | Орр                           | Eq.(13)         | Eq.(14)                |
| (1)       | (2)     | (9)                           | (10)            | (11)                   |
| N         | LT/LTOR | 149                           | 0.21            |                        |
|           | ST      | 425                           |                 |                        |
|           | RT      | 152                           |                 | 0.21                   |
|           | TOTAL   | 726                           |                 |                        |
| S         | LT/LTOR | 140                           | 0.26            |                        |
|           | ST      | 275                           |                 |                        |
|           | RT      | 121                           |                 | 0.23                   |
|           | TOTAL   | 536                           |                 |                        |
| Ε         | LT/LTOR | 235                           | 0.24            |                        |
|           | ST      | 480                           |                 |                        |
|           | RT      | 248                           |                 | 0.26                   |
|           | TOTAL   | 963                           |                 |                        |
| W         | LT/LTOR | 194                           | 0.23            |                        |
|           | ST      | 440                           |                 |                        |
|           | RT      | 192                           |                 | 0.23                   |
|           | TOTAL   | 826                           |                 |                        |



| A | ppr ( | Green | Appr |      | Ratio   | )    | Eff   |       |      |                  | S         | Saturation | n flow pc | u/h    |          | Traffic | Flow  | Phase  | Green   | Capacity | Degree     |
|---|-------|-------|------|------|---------|------|-------|-------|------|------------------|-----------|------------|-----------|--------|----------|---------|-------|--------|---------|----------|------------|
| С | ode   | In    | type | 0    | f turni | ng   | width | Base  |      |                  | Adjustme  | ent factor | S         |        | Adjusted | Flow    | ratio | Ratio  | Time    | pcu/h    | Of         |
|   | F     | Phase |      | ١    | vehicle | es   | (m)   | Value |      | All a            | appr type |            | Only      | type p | Value    | pcu/h   | FR    | PR =   | Sec     | S x g/c  | Saturation |
|   |       | no    |      |      |         |      |       | pcu/h | City | Side             | Gradient  | Parking    | Right     | Lift   | pcu/h    |         |       | FRcrit |         |          |            |
|   |       |       |      |      |         |      |       |       | Size | Friction         |           |            | Turns     | Turns  |          |         |       | [      |         |          |            |
|   |       |       |      | Р    | D       | D    | \M/   | c     | Faa  | Far              | E.        | E-         | E         | E      | S        | 0       | 0/9   | IED    | 0       | C        | OIC        |
|   |       |       |      | LTOR | ' LI    | I RI | ۷Ve   | 0.    | T CS | I S⊦             | IG        | īР         | I KI      | 1 L I  | 0        | Q       | Q/3   |        | y       | U        | QIU        |
|   |       |       |      |      |         |      |       |       |      |                  |           |            |           |        |          |         |       |        |         |          |            |
|   |       |       |      |      |         |      |       |       |      |                  |           |            |           |        |          |         |       |        |         |          |            |
|   |       | (-)   | (-)  |      | ()      |      | ()    | (-)   | (1)  | <i>(</i> , , , ) | ()        | (1.2)      | ( ) = )   | (      | (        | ( )     |       | (      | ( ) = ) | (2.2)    | (5.1)      |
| ( | 1)    | (2)   | (3)  | (4)  | (5)     | (6)  | (7)   | (8)   | (9)  | (10)             | (11)      | (12)       | (13)      | (14)   | (15)     | (16)    | (17)  | (18)   | (19)    | (20)     | (21)       |
|   | Ν     | 1     | Ρ    |      |         |      | 5     | 3000  | 1.00 | 0.95             | 1.00      | 1.00       | 1.054     | 0.9664 | 2903     | 577     | 0.199 | 0.32   | 20      | 744      | 0.78       |
|   | S     | I     | р    |      |         |      | 5     | 3000  | 1.00 | 0.98             | 1.00      | 1.00       | 1.0598    | 0.9584 | 2986     | 396     | 0.133 |        | 20      | 766      | 0.52       |
|   | Ν     | 0     | Ρ    |      |         |      | 3     | 1800  | 1.00 | 0.95             | 1.00      | 1.00       | 1.054     | 0.9664 | 1741     | 149     | 0.086 | 0.14   | 9       | 201      | 0.74       |
|   | S     | 2     | р    |      |         |      | 3     | 1800  | 1.00 | 0.98             | 1.00      | 1.00       | 1.0598    | 0.9584 | 1792     | 140     | 0.071 |        | 9       | 207      | 0.68       |
|   | E     | c     | р    |      |         |      | 5.5   | 3300  | 1.00 | 0.95             | 1.00      | 1.00       | 1.0676    | 0.9616 | 3218     | 728     | 0.226 | 0.361  | 22      | 908      | 0.80       |
| ١ | N     | 3     | Ρ    |      |         |      | 5.5   | 3300  | 1.00 | 0.95             | 1.00      | 1.00       | 1.0589    | 0.9632 | 3197     | 632     | 0.198 |        | 22      | 902      | 0.70       |
|   | E     | 4     | р    |      |         |      | 3.5   | 2100  | 1.00 | 0.95             | 1.00      | 1.00       | 1.0676    | 0.9616 | 2048     | 235     | 0.115 | 0.184  | 11      | 289      | 0.81       |

| W               |      | р   |         |        | 3.5       | 2100      | 1.00 | 0.95 | 1.00 | 1.00 | 1.0589 | 0.9632 | 2035 | 194                 | 0.095 | 11 | 287 | 0.68 |
|-----------------|------|-----|---------|--------|-----------|-----------|------|------|------|------|--------|--------|------|---------------------|-------|----|-----|------|
| Total lo        | st   | 16  | Unadjus | stment | cycle tin | ne Cus (s | sec) | 78   |      |      |        |        |      | IFR=                |       |    |     |      |
| time<br>LTI (se | c) ( | Sec | Adjust  | ment c | ycle time | e C (se   | ec)  | 78   |      |      |        |        |      | ∑FR <sub>CRIT</sub> | 0.626 |    |     |      |

| Approach             | Traffic | Capacity | Degree of  | Green | No              | . of queuin | ig vehicles ( | (pcu)             | Queue       | Stop      | No. of | Delay         |                    |                       |         |
|----------------------|---------|----------|------------|-------|-----------------|-------------|---------------|-------------------|-------------|-----------|--------|---------------|--------------------|-----------------------|---------|
| Code                 | flow    | pcu/h    | Saturation | Ratio |                 |             |               |                   | length      | rate      | Stops  | Average       | Average            | Average delay         | Total   |
|                      | pcu/h   |          | DS         | GR    | NQ <sub>1</sub> | $NQ_2$      | Total         | NQ <sub>MAX</sub> | (m)         | stops/pcu | pcu/h  | Traffic delay | Geometric<br>delay | sec/pcu               | Delay   |
|                      |         |          | =          | =     |                 |             | $NQ_1 + NQ_2$ |                   |             |           |        | sec/pcu       | sec/pcu            | D =                   | Pcu.sec |
|                      | Q       | С        | Q/C        | g/c   |                 |             | NQ            |                   | QL          | NS        | Nsv    | DT            | DG                 | DT+DG                 | D x Q   |
|                      |         |          |            |       |                 |             |               |                   |             |           |        |               |                    |                       |         |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6)             | (7)         | (8)           | (9)               | (10)        | (11)      | (12)   | (13)          | (14)               | (15)                  | (16)    |
| N                    | 577     | 744      | 0.78       | 0.26  | 1.25            | 11.60       | 12.85         | 20                | 80          | 0.925     | 534    | 32.84         | 3.79               | 36.63                 | 21136   |
| S                    | 396     | 766      | 0.52       | 0.26  | 0.042           | 7.34        | 7.38          | 12                | 48          | 0.77      | 305    | 24.89         | 3.40               | 28.29                 | 11203   |
| N                    | 149     | 201      | 0.74       | 0.11  | 0.89            | 3.13        | 4.02          | 8                 | 53          | 1.12      | 167    | 49.57         | 4.33               | 53.90                 | 8031    |
| S                    | 140     | 207      | 0.68       | 0.11  | 0.55            | 2.92        | 3.47          | 7                 | 47          | 1.03      | 144    | 42.95         | 4.08               | 47.03                 | 6584    |
| E                    | 728     | 908      | 0.80       | 0.28  | 1.48            | 14.64       | 16.12         | 24                | 87          | 0.92      | 670    | 31.92         | 3.80               | 35.72                 | 26004   |
| W                    | 632     | 902      | 0.70       | 0.28  | 0.66            | 12.26       | 12.92         | 20                | 73          | 0.85      | 537    | 27.78         | 3.61               | 31.39                 | 19838   |
| E                    | 235     | 289      | 0.81       | 0.14  | 1.54            | 4.94        | 6.48          | 11                | 63          | 1.15      | 270    | 51.72         | 4.37               | 56.09                 | 13181   |
| W                    | 194     | 287      | 0.68       | 0.14  | 0.56            | 4.00        | 4.56          | 8.5               | 49          | 0.98      | 190    | 38.90         | 3.95               | 42.85                 | 8313    |
| ROTR (all)           |         |          |            |       |                 |             |               |                   |             |           |        |               |                    |                       |         |
| Flow adj. Qadj :     |         |          |            |       |                 |             |               |                   |             | Total:    | 2817   |               |                    | Total                 | 114290  |
| Total flow Qtot<br>: | 3051    |          |            |       |                 |             |               | Ave               | rage no. of | stops/pcu | 0.92   | Avera         | ge interse<br>(sec | ction delay<br>c/pcu) | 37.46   |

### 3. Low Traffic Flow

|           |         | Total<br>Motor vehicles | R       | atio<br>of      |
|-----------|---------|-------------------------|---------|-----------------|
| Appr code | Dir.    | MV                      | tur     | ning            |
|           |         | pcu/h                   | рьт     | р <sub>RT</sub> |
|           |         | Орр                     | Eq.(13) | Eq.(14)         |
|           | (2)     | (9)                     | (10)    | (11)            |
| Ν         | LT/LTOR | 100                     | 0.21    |                 |
|           | ST      | 284                     |         |                 |
|           | RT      | 101                     |         | 0.21            |
|           | TOTAL   | 485                     |         |                 |
| S         | LT/LTOR | 94                      | 0.26    |                 |
|           | ST      | 184                     |         |                 |
|           | RT      | 81                      |         | 0.23            |
|           | TOTAL   | 359                     |         |                 |
| E         | LT/LTOR | 157                     | 0.24    |                 |
|           | ST      | 320                     |         |                 |
|           | RT      | 166                     |         | 0.26            |
|           | TOTAL   | 643                     |         |                 |
| W         | LT/LTOR | 129                     | 0.23    |                 |
|           | ST      | 294                     |         |                 |
|           | RT      | 128                     |         | 0.23            |
|           | TOTAL   | 551                     |         |                 |



| Appr | Green | Appr |      | Ratic    | )    | Eff   |       |      |          | S         | Saturation | n flow po | u/h    |          | Traffic | Flow  | Phase  | Green | Capacity | Degree     |
|------|-------|------|------|----------|------|-------|-------|------|----------|-----------|------------|-----------|--------|----------|---------|-------|--------|-------|----------|------------|
| Code | In    | type | 0    | of turni | ng   | width | Base  |      |          | Adjustme  | ent factor | S         |        | Adjusted | Flow    | ratio | Ratio  | Time  | pcu/h    | Of         |
|      | Phase |      | ١    | vehicle  | es   | (m)   | Value |      | All a    | appr type |            | Only      | type p | Value    | pcu/h   | FR    | PR =   | Sec   | S x g/c  | Saturation |
|      | no    |      |      |          |      |       | pcu/h | City | Side     | Gradient  | Parking    | Right     | Lift   | pcu/h    |         |       | FRcrit |       |          |            |
|      |       |      |      |          |      |       |       | Size | Friction |           |            | Turns     | Turns  |          |         |       |        |       |          |            |
|      |       |      | Ρ    | P.T      | P    | W.    | S     | Foo  | For      | Fa        | Fn         | For       | F      | S        | 0       | 0/5   | IFR    | a     | C        | 0/0        |
|      |       |      | LTOR | ' ''     | ' RI | ••e   |       | 105  | • SF     | 16        | ١P         | I RI      | • []   | U        | Q       | Q/O   |        | 9     | Ŭ        | Q, O       |
|      |       |      |      |          |      |       |       |      |          |           |            |           |        |          |         |       |        |       |          |            |
|      |       |      |      |          |      |       |       |      |          |           |            |           |        |          |         |       |        |       |          |            |
| (1)  | (2)   | (2)  | (1)  | (5)      | in   | (7)   | (0)   | (0)  | (10)     | (11)      | (10)       | (10)      | (1.4)  | (15)     | (1/)    | (17)  | (10)   | (10)  | (20)     | (01)       |
| (1)  | (2)   | (3)  | (4)  | (5)      | (6)  | (/)   | (8)   | (9)  | (10)     | (11)      | (12)       | (13)      | (14)   | (15)     | (16)    | (17)  | (18)   | (19)  | (20)     | (21)       |
| Ν    | 1     | Р    |      |          |      | 5     | 3000  | 1.00 | 0.95     | 1.00      | 1.00       | 1.054     | 0.9664 | 2903     | 385     | 0.133 | 0.32   | 11    | 603      | 0.64       |
| S    | I     | р    |      |          |      | 5     | 3000  | 1.00 | 0.98     | 1.00      | 1.00       | 1.0598    | 0.9584 | 2986     | 265     | 0.089 |        | 11    | 620      | 0.43       |
| Ν    | 2     | Ρ    |      |          |      | 3     | 1800  | 1.00 | 0.95     | 1.00      | 1.00       | 1.054     | 0.9664 | 1741     | 100     | 0.057 | 0.14   | 7     | 230      | 0.43       |
| S    | 2     | р    |      |          |      | 3     | 1800  | 1.00 | 0.98     | 1.00      | 1.00       | 1.0598    | 0.9584 | 1792     | 94      | 0.052 |        | 7     | 237      | 0.40       |
| Е    | 2     | р    |      |          |      | 5.5   | 3300  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0676    | 0.9616 | 3218     | 486     | 0.151 | 0.36   | 12    | 729      | 0.67       |
| W    | 5     | Ρ    |      |          |      | 5.5   | 3300  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0589    | 0.9632 | 3197     | 422     | 0.132 |        | 12    | 724      | 0.58       |
| Е    | 1     | р    |      |          |      | 3.5   | 2100  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0676    | 0.9616 | 2048     | 157     | 0.077 | 0.18   | 7     | 270      | 0.58       |
| W    | 4     | р    |      |          |      | 3.5   | 2100  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0589    | 0.9632 | 2035     | 129     | 0.065 |        | 7     | 269      | 0.48       |

| Total lost        | 16  | Unadjustment cycle time Cus (sec) | 50 |  |  | IFR=                |       |  |  |
|-------------------|-----|-----------------------------------|----|--|--|---------------------|-------|--|--|
| time<br>LTI (sec) | Sec | Adjustment cycle time C (sec)     | 53 |  |  | ∑FR <sub>CRIT</sub> | 0.418 |  |  |

| Approach             | Traffic | Capacity | Degree of  | Green | No   | . of queuin     | ng vehicles ( | (pcu) | Queue      | Stop        | No. of | Delay         |                    |                       |         |
|----------------------|---------|----------|------------|-------|------|-----------------|---------------|-------|------------|-------------|--------|---------------|--------------------|-----------------------|---------|
| Code                 | flow    | pcu/h    | Saturation | Ratio |      |                 |               |       | length     | rate        | Stops  | Average       | Average            | Average delay         | Total   |
|                      | pcu/h   |          | DS         | GR    | NQ1  | NQ <sub>2</sub> | Total         | NQMAX | (m)        | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delay | sec/pcu               | Delay   |
|                      |         |          | =          | =     |      |                 | $NQ_1 + NQ_2$ |       |            |             |        | sec/pcu       | sec/pcu            | D =                   | Pcu.sec |
|                      | Q       | С        | Q/C        | g/c   |      |                 | NQ            |       | QL         | NS          | Nsv    | DT            | DG                 | DT+DG                 | DxQ     |
|                      |         |          |            |       |      |                 |               |       |            |             |        |               |                    |                       |         |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6)  | (7)             | (8)           | (9)   | (10)       | (11)        | (12)   | (13)          | (14)               | (15)                  | (16)    |
| N                    | 385     | 603      | 0.64       | 0.21  | 0.39 | 5.17            | 5.56          | 10    | 40         | 0.88        | 339    | 21.26         | 3.67               | 24.93                 | 9598    |
| S                    | 265     | 620      | 0.43       | 0.21  | 0    | 3.39            | 3.39          | 7     | 28         | 0.78        | 207    | 18.18         | 3.42               | 21.6                  | 5724    |
| N                    | 100     | 230      | 0.43       | 0.13  | 0    | 1.36            | 1.36          | 3.8   | 25         | 0.83        | 83     | 21.25         | 3.53               | 24.78                 | 2478    |
| S                    | 94      | 237      | 0.40       | 0.13  | 0    | 1.27            | 1.27          | 3.2   | 21         | 0.826       | 78     | 21.16         | 3.54               | 24.7                  | 2322    |
| E                    | 486     | 729      | 0.67       | 0.23  | 0.51 | 6.51            | 7.02          | 12    | 44         | 0.88        | 428    | 21.09         | 3.71               | 24.8                  | 12053   |
| W                    | 422     | 724      | 0.58       | 0.23  | 0.19 | 5.52            | 5.71          | 10    | 36         | 0.83        | 350    | 19.08         | 3.55               | 22.63                 | 9550    |
| E                    | 157     | 270      | 0.58       | 0.13  | 0.19 | 2.17            | 2.36          | 6     | 34         | 0.92        | 144    | 24.22         | 3.80               | 28.02                 | 4399    |
| W                    | 129     | 269      | 0.48       | 0.13  | 0    | 1.76            | 1.76          | 4.3   | 25         | 0.83        | 107    | 21.39         | 3.55               | 24.94                 | 3217    |
| ROTR (all)           |         |          |            |       |      |                 |               |       |            |             |        |               |                    |                       |         |
| Flow adj. Qadj :     |         |          |            |       |      |                 |               |       |            | Total:      | 1736   |               |                    | Total                 | 49341   |
| Total flow Qtot<br>: | 2038    |          |            |       |      |                 |               | Ave   | rage no. o | f stops/pcu | 0.85   | Avera         | ge interse<br>(sec | ction delay<br>c/pcu) | 24.2    |

### 4. Very Low Traffic Flow

| -         |         |          |         |             |
|-----------|---------|----------|---------|-------------|
|           |         | Total    |         |             |
|           |         | Motor    |         | Ratio       |
| Appr code | Dir.    | vehicles |         | of          |
|           |         | MV       |         | turning     |
|           |         | pcu/h    |         | -           |
|           |         |          | р∟т     | <b>р</b> кт |
|           |         | Орр      | Eq.(13) | Eq.(14)     |
| (1)       | (2)     | (9)      | (10)    | (11)        |
| N         | LT/LTOR | 50       | 0.21    |             |
|           | ST      | 142      |         |             |
|           | RT      | 51       |         | 0.21        |
|           | TOTAL   | 243      |         |             |
| S         | LT/LTOR | 47       | 0.26    |             |
|           | ST      | 92       |         |             |
|           | RT      | 40       |         | 0.23        |
|           | TOTAL   | 179      |         |             |
| E         | LT/LTOR | 78       | 0.24    |             |
|           | ST      | 160      |         |             |
|           | RT      | 83       |         | 0.26        |
|           | TOTAL   | 321      |         |             |
| W         | LT/LTOR | 65       | 0.23    |             |
|           | ST      | 147      |         |             |
| N         | RT      | 64       |         | 0.23        |
|           | TOTAL   | 276      |         |             |



| Ap | pr Gr | reen | Appr |                   | Ratio   | )    | Eff                 |       |      |          | S         | aturation  | n flow pc | u/h    |          | Traffic | Flow  | Phase  | Green | Capacity | Degree     |
|----|-------|------|------|-------------------|---------|------|---------------------|-------|------|----------|-----------|------------|-----------|--------|----------|---------|-------|--------|-------|----------|------------|
| Со | de    | In   | type | 0                 | f turni | ng   | width               | Base  |      |          | Adjustme  | ent factor | S         |        | Adjusted | Flow    | ratio | Ratio  | Time  | pcu/h    | Of         |
|    | Ph    | nase |      | ١                 | vehicle | es   | (m)                 | Value |      | All a    | ippr type |            | Only      | type p | Value    | pcu/h   | FR    | PR =   | Sec   | S x g/c  | Saturation |
|    | r     | no   |      |                   |         |      |                     | pcu/h | City | Side     | Gradient  | Parking    | Right     | Lift   | pcu/h    |         |       | FRcrit |       |          |            |
|    |       |      |      |                   |         |      |                     |       | Size | Friction |           |            | Turns     | Turns  |          |         |       |        |       |          |            |
|    |       |      |      | Р                 | P.T     | P    | W.                  | S     | Foo  | For      | Fo        | Fa         | For       | E      | S        | 0       | 0/5   | IFR    | a     | C        | 0/0        |
|    |       |      |      | LTOR              | • LI    | ' RI | ••e                 | 0.0   | 105  | • SF     | IG        | īР         | I RI      | ' L I  | 0        | G       | Q/O   |        | 9     | Ŭ        | QIU        |
|    |       |      |      |                   |         |      |                     |       |      |          |           |            |           |        |          |         |       |        |       |          |            |
|    |       |      |      |                   |         |      |                     |       |      |          |           |            |           |        |          |         |       |        |       |          |            |
|    |       | (0)  | (0)  | <i>(</i> <b>)</b> | ()      |      | <i>(</i> <b>_</b> ) |       | (0)  | (10)     | (1.1)     | (10)       | (10)      | (4.1)  | (1-)     | (4.1)   |       | (10)   | (10)  | (0.0)    | (0.1)      |
| (1 | ) (   | (2)  | (3)  | (4)               | (5)     | (6)  | (/)                 | (8)   | (9)  | (10)     | (11)      | (12)       | (13)      | (14)   | (15)     | (16)    | (17)  | (18)   | (19)  | (20)     | (21)       |
| Ν  |       | 1    | Ρ    |                   |         |      | 5                   | 3000  | 1.00 | 0.95     | 1.00      | 1.00       | 1.054     | 0.9664 | 2903     | 193     | 0.066 | 0.32   | 7     | 452      | 0.43       |
| S  | 5     | I    | р    |                   |         |      | 5                   | 3000  | 1.00 | 0.98     | 1.00      | 1.00       | 1.0598    | 0.9584 | 2986     | 132     | 0.044 |        | 7     | 464      | 0.28       |
| Ν  |       | 2    | Ρ    |                   |         |      | 3                   | 1800  | 1.00 | 0.95     | 1.00      | 1.00       | 1.054     | 0.9664 | 1741     | 51      | 0.029 | 0.14   | 7     | 271      | 0.19       |
| 9  | 5     | 2    | р    |                   |         |      | 3                   | 1800  | 1.00 | 0.98     | 1.00      | 1.00       | 1.0598    | 0.9584 | 1792     | 47      | 0.026 |        | 7     | 279      | 0.17       |
| E  |       | 2    | р    |                   |         |      | 5.5                 | 3300  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0676    | 0.9616 | 3218     | 243     | 0.076 | 0.36   | 8     | 572      | 0.42       |
| ۷  | /     | 3    | Ρ    |                   |         |      | 5.5                 | 3300  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0589    | 0.9632 | 3197     | 211     | 0.066 |        | 8     | 568      | 0.37       |
| E  |       | 4    | р    |                   |         |      | 3.5                 | 2100  | 1.00 | 0.95     | 1.00      | 1.00       | 1.0676    | 0.9616 | 2048     | 78      | 0.038 | 0.18   | 7     | 319      | 0.24       |

| W                 | р   |                 | 3.5       | 2100      | 1.00 | 0.95 | 1.00 | 1.00 | 1.0589 | 0.9632 | 2035 | 64                  | 0.031 | 7 | 317 | 0.20 |
|-------------------|-----|-----------------|-----------|-----------|------|------|------|------|--------|--------|------|---------------------|-------|---|-----|------|
| Total los         | 16  | Unadjustment of | cycle tin | ne Cus (s | sec) | 37   |      |      |        |        |      | IFR=                |       |   |     |      |
| time<br>LTI (sec) | Sec | Adjustment cy   | ycle time | eC (se    | ec)  | 45   |      |      |        |        |      | ∑FR <sub>CRIT</sub> | 0.209 |   |     |      |

| Approach             | Traffic | Capacity | Degree of  | Green | No  | . of queuin     | g vehicles (  | (pcu) | Queue       | Stop        | No. of | Delay         |   |               |         |  |  |  |  |  |
|----------------------|---------|----------|------------|-------|-----|-----------------|---------------|-------|-------------|-------------|--------|---------------|---|---------------|---------|--|--|--|--|--|
| Code                 | flow    | pcu/h    | Saturation | Ratio |     |                 |               |       | length      | rate        | Stops  | Average       | Average                                 | Average delay | Total   |  |  |  |  |  |
|                      | pcu/h   |          | DS         | GR    | NQ1 | NQ <sub>2</sub> | Total         | NQMAX | (m)         | stops/pcu   | pcu/h  | Traffic delay | Geometric<br>delav                      | sec/pcu       | Delay   |  |  |  |  |  |
|                      |         |          | =          | =     |     |                 | $NQ_1 + NQ_2$ |       |             |             |        | sec/pcu       | sec/pcu                                 | D =           | Pcu.sec |  |  |  |  |  |
|                      | Q       | С        | Q/C        | g/c   |     |                 | NQ            |       | QL          | NS          | Nsv    | DT            | DG                                      | DT+DG         | DxQ     |  |  |  |  |  |
|                      |         |          |            |       |     |                 |               |       |             |             |        |               |   |               |         |  |  |  |  |  |
| (1)                  | (2)     | (3)      | (4)        | (5)   | (6) | (7)             | (8)           | (9)   | (10)        | (11)        | (12)   | (13)          | (14)                                    | (15)          | (16)    |  |  |  |  |  |
| N                    | 193     | 452      | 0.43       | 0.16  | 0   | 2.18            | 2.18          | 5     | 20          | 0.81        | 156    | 5.91          | 3.48                                    | 9.39          | 1812    |  |  |  |  |  |
| S                    | 132     | 464      | 0.28       | 0.16  | 0   | 1.45            | 1.45          | 3     | 12          | 0.79        | 104    | 16.62         | 3.45                                    | 20.07         | 2649    |  |  |  |  |  |
| N                    | 51      | 271      | 0.19       | 0.16  | 0   | 0.55            | 0.55          | 2     | 13          | 0.776       | 40     | 16.37         | 3.39                                    | 19.76         | 1008    |  |  |  |  |  |
| S                    | 47      | 279      | 0.17       | 0.16  | 0   | 0.51            | 0.51          | 1.9   | 13          | 0.78        | 37     | 16.31         | 3.42                                    | 19.73         | 927     |  |  |  |  |  |
| E                    | 243     | 572      | 0.42       | 0.18  | 0   | 2.69            | 2.69          | 6.3   | 23          | 0.80        | 194    | 16.37         | 3.51                                    | 19.88         | 4831    |  |  |  |  |  |
| W                    | 211     | 568      | 0.37       | 0.18  | 0   | 2.32            | 2.32          | 5     | 18          | 0.79        | 167    | 16.21         | 3.42                                    | 19.63         | 4142    |  |  |  |  |  |
| E                    | 78      | 319      | 0.24       | 0.16  | 0   | 0.85            | 0.85          | 2.3   | 13          | 0.78        | 61     | 16.51         | 3.46                                    | 19.97         | 1558    |  |  |  |  |  |
| W                    | 64      | 317      | 0.20       | 0.16  | 0   | 0.69            | 0.69          | 2.1   | 12          | 0.776       | 50     | 16.40         | 3.41                                    | 19.81         | 1268    |  |  |  |  |  |
| ROTR (all)           |         |          |            |       |     |                 |               |       |             |             |        |               |   |               |         |  |  |  |  |  |
| Flow adj. Qadj :     |         |          |            |       |     |                 |               |       |             | Total:      | 809    |               |   | Total         | 18195   |  |  |  |  |  |
| Total flow Qtot<br>: | 948     |          |            |       |     |                 |               | Ave   | erage no. o | f stops/pcu | 0.85   | Avera         | Average intersection delay<br>(sec/pcu) |               |         |  |  |  |  |  |
|                      |         | -        |            |       |     |                 |               |       |             | L           |        |               | ,                                       |               |         |  |  |  |  |  |