

BAB II**PERHITUNGAN RENCANA GARIS****(LINES PLAN)****A. PERHITUNGAN DASAR**

1. Panjang Garis Air Muat (Lwl)

$$\begin{aligned}Lwl &= Lpp + 2 \% \times Lpp \\ &= 99,15 + 1,983 \\ &= 101,133 \text{ m}\end{aligned}$$

2. Panjang Displacement (L Displ)

$$\begin{aligned}L \text{ Displ} &= 0,5 \times (Lwl + Lpp) \\ &= 0,5 \times (101,133 + 99,15) \\ &= 100,1415 \text{ m}\end{aligned}$$

3. Coefisien Midship (Cm) Formula Arkent Bont Shocker

$$\begin{aligned}Cm &= 0,90 + 0,1 + \sqrt{Cb} \\ &= 0,90 + 0,1 + \sqrt{0,76} \\ &= 0,99 \rightarrow \text{Memenuhi Syarat} \quad (0,95 - 0,99)\end{aligned}$$

4. Coefisien Prismatic (Cp) Formula Troast

$$\begin{aligned}Cp &= Cb / Cm \\ &= 0,76 / 0,99 \\ &= 0,770 \rightarrow \text{Memenuhi Syarat} \quad (0,68 - 0,80)\end{aligned}$$

5. Coefisien Garis Air (Cw) Formula Troast

$$\begin{aligned}Cw &= \sqrt{cb - 0.025} \\ &= \sqrt{0.71 - 0.025} \\ &= 0,86 \rightarrow \text{Memenuhi Syarat} \quad (0,80 - 0,87)\end{aligned}$$

6. Luas Garis Air (Awl)

$$\begin{aligned}Awl &= Lwl \times B \times Cw \\ &= 101,133 \times 15,41 \times 0,847\end{aligned}$$

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$$= 1336,101 \text{ m}^2$$

7. Luas Midship (A_m)

$$A_m = B \times T \times C_m$$

$$= 15,41 \times 6,86 \times 0,99$$

$$= 104,36 \text{ m}^2$$

8. Volume Displacement (C Displ)

$$V \text{ Displ} = L_{pp} \times B \times T \times C_b$$

$$= 99,15 \times 15,41 \times 6,86 \times 0,76$$

$$= 7965,867 \text{ m}^3$$

9. Coefisien Prismatic Displacement (C_p Displ)

$$C_p \text{ Displ} = L_{pp} / L \text{ Displ} \times C_p$$

$$= 99,15 / 100,1415 \times 0,77$$

$$= 0,762$$

10. Displacement (D)

$$D = V \text{ Displ} \times \rho \times c$$

$$= 7965,967 \times 1,025 \times 1,004$$

$$= 8197,67 \text{ Ton}$$

B. MENENTUKAN LETAK LCB

B.1. Dengan menggunakan Cp Displacement pada grafik NSP pada Cp

Displacement = 0,70 Didapat letak titik LCB (Longitudinal Centre

Bouyancy = 0,8 % x L Displ, dimana L Displ = 101,404 m

$$\begin{aligned} \text{Cp Displ} &= \text{Lpp} / \text{L Displ} \times \text{Cp} \\ &= 99,15 / 100,1415 \times 0,770 \\ &= 0,7622 \end{aligned}$$

B.1.1. Letak LCB Displ menurut grafik NSP

$$\begin{aligned} \text{LCB Displ} &= 1,8 \% \times \text{L Displ} \\ &= 1,8 \times 100,1415 \\ &= 1,803 \text{ m} \quad (\text{Di depan midship Lpp}) \end{aligned}$$

B.1.2. Jarak midship (O) L Displ ke FP

$$\begin{aligned} \text{O Displ} &= 0,5 \times \text{L Displ} \\ &= 0,5 \times 100,1415 \\ &= 50,07075 \text{ m} \end{aligned}$$

B.1.3. Jarak midship (O) Lpp ke FP

$$\begin{aligned} \text{O Lpp} &= 0,5 \times \text{Lpp} \\ &= 0,5 \times 99,15 \\ &= 49,58 \text{ m} \end{aligned}$$

B.1.4. Jarak antara midship (O) L Displ dengan midship (O) Lpp

$$\begin{aligned} &= \text{O Displ} - \text{O Lpp} \\ &= 50,07075 - 49,575 \\ &= 0,50 \text{ m} \end{aligned}$$

B.1.5. Jarak antara LCB terhadap midship (O) Lpp

$$\begin{aligned} &= 1,803 - 0,50 \\ &= 1,303 \text{ m} \quad (\text{Di belakang O Lpp}) \end{aligned}$$

B.2. Menurut diagram NSP dengan luas tiap section (A_m) = 104,36 m²

No. Ord	%	% thdp AM	FS	Hasil	FM	Hasil
0	0	0,0000	1	0,000	-10	-0,00
1	0,120	12,5229	4	50,091	-9	-450,82
2	0,365	38,0904	2	76,181	-8	-609,45

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3	0,575	60,0054	4	240,021	-7	-1680,15	
4	0,760	79,3114	2	158,623	-6	-951,74	
5	0,895	93,3996	4	373,599	-5	-1867,99	
6	0,950	99,1393	2	198,279	-4	-793,11	
7	0,980	102,2700	4	409,080	-3	-1227,24	
8	0,990	103,3136	2	206,627	-2	-413,25	
9	1	104,3572	4	417,429	-1	-417,43	
10	1	104,3572	2	208,714	0	-0	
					Σ_2	-8411,19	
11	1	104,3572	4	417,429	1	417,43	
12	1	104,3572	2	208,714	2	417,43	
13	1	104,3572	4	417,429	3	1252,29	
14	1	104,3572	2	208,714	4	834,86	
15	1	104,3572	4	417,429	5	2087,14	
16	0,940	98,0957	2	196,191	6	1177,15	
17	0,770	80,3550	4	321,420	7	2249,94	
18	0,545	56,8746	2	113,749	8	909,99	
19	0,240	25,0457	4	100,183	9	901,65	
20	0	0,0000	1	0,000	0	0	
				Σ_1	4739,900	Σ_3	10247,87

$$\begin{aligned}
 \text{B.2.1. } h &= L \text{ Displ} / 20 \\
 &= 100,1415 / 20 \\
 &= 5,007 \text{ m}
 \end{aligned}$$

B.2.2. Volume Displacement

$$\begin{aligned}
 V \text{ Displ} &= 1/3 \times h \times E1 \\
 &= 1/3 \times 5,007 \times 4623,2352 \\
 &= 7911,01 \text{ m}^3
 \end{aligned}$$

B.2.3. Letak LCB NSP

$$\text{LCB NSP} = \frac{\Sigma_2 + \Sigma_3}{\Sigma_1} \times \frac{L \text{ Displ}}{20}$$

$$\begin{aligned}
&= \frac{-8411,19 + 10247,87}{4739,902} \times \frac{100,1415}{20} \\
&= \frac{1836,69}{4739,902} \times 5,007 \\
&= 1,940 \text{ m}
\end{aligned}$$

B.2.4. Koreksi prosentase penyimpangan LCB

$$\begin{aligned}
&= \frac{\text{LCB Displ} - \text{LCB NSP}}{\text{L Displ}} \times 100 \% \\
&= \frac{1,803 - 1,940}{100,1415} \times 100 \% \\
&= -0,00137472 \times 100 \% \\
&= -0,1375 \% < 0,1 \% \quad (\text{Memenuhi})
\end{aligned}$$

B.2.5. Koreksi prosentase penyimpangan untuk vol. Displ

$$\begin{aligned}
&= \frac{\text{Vol Displ Awal} - \text{Vol Displ NSP}}{\text{Vol Displ Awal}} \times 100 \% \\
&= \frac{7965,87 - 7911,01}{7965,87} \times 100 \% \\
&= 54,85 / 7965,87 \times 100 \% \\
&= -0,7 \% < 0,5 \% \quad (\text{Memenuhi})
\end{aligned}$$

B.3. Perhitungan prismatic depan (Qf) dan koefisien prismatic belakang (Qa) berdasarkan tabel "Van Lamerent"

Dimana :

$$\begin{aligned}
Q_f &= \text{Koefisien prismatic bagian depan midship Lpp} \\
Q_a &= \text{Koefisien prismatic bagian belakang midship Lpp} \\
e &= \text{Perbandingan jarak LCB terhadap Lpp} \\
e &= (\text{LCB Lpp} / \text{Lpp}) \times 100 \% \\
&= (1,303 / 99,15) \times 100 \% \\
&= 1,3142 \%
\end{aligned}$$

Dengan rumus tersebut diatas dapat dihitung harga Qa dan Qf dengan rumus berikut :

$$Q_a = Q_f = \pm (1,4 + Q) \times e$$

Dimana :

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$$\begin{aligned}
 Q_f &= C_p + (1,4 + Q) \times e \\
 &= 0,770 + (1,4 + 0,770) \times 0,0131 \\
 &= 0,798
 \end{aligned}$$

$$\begin{aligned}
 Q_a &= C_p - (1,4 + Q) \times e \\
 &= 0,770 - (1,4 + 0,770) \times 0,0131 \\
 &= 0,742
 \end{aligned}$$

Tabel luas tiap section terhadap Am menurut Van Lamerent

$$A_m = 104,36 \text{ m}^2$$

No Ord	% Luas Station	Luas Station Thd Am	FS	Hasil	FM	Hasil
AP	0,000	1,800	0,25	0.450	- 5	-2,25
0,25	0,100	10,400	1	10,400	- 4,75	-49,4
0,5	0,207	21,600	0,5	10,800	- 4,5	-48,6
0,75	0,318	33,200	1	33,200	- 4,25	-141,4
1	0,429	44,800	0,75	33,600	- 4	-134,4
1,5	0,632	66,000	2	132,000	- 3,5	-462
2	0,792	82,600	1	82,600	- 3	-247,8
2,5	0,907	94,600	2	189,200	- 2,5	-473
3	0,972	101,400	1,5	152,100	- 2	-304,2
4	1,000	104,400	4	417,600	- 1	-417,6
5	1,000	104,400	2	208,800	- 0	-0
					Σ_2	- 2280,35
6	1,000	104,400	4	417,600	1	417,6
7	0,998	104,100	1,5	156,150	2	312,3
7,5	0,972	101,400	2	202,800	2,5	507
8	0,901	94,000	1	94,000	3	282
8,5	0,753	78,600	2	157,200	3,5	550,2
9	0,558	58,200	0,75	43,650	4	174,6
9,25	0,427	44,600	1	44,600	4,25	189,55
9,5	0,287	30,000	0,5	15,000	4,5	67,5
9,75	0,095	14,800	1	14,800	4,75	70,3

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FP	0,142	0	0,25	0	0	0
			Σ_1	2416,55	Σ_3	2571,05

$$\begin{aligned} 1. h &= L_{pp} / 10 \\ &= 99,15 / 10 \\ &= 9,915 \text{ m} \end{aligned}$$

2. Volume Displacement pada Main Part

$$\begin{aligned} V_{\text{Displ}} &= 1/3 \times L_{pp} / 10 \times \Sigma_1 \\ &= 1/3 \times 99,15 / 10 \times 2416,55 \\ &= 7986,698 \text{ m}^3 \end{aligned}$$

3. Letak LCB pada Main Part

$$\begin{aligned} &= \frac{\Sigma_2 + \Sigma_3}{\Sigma_1} \times \frac{L_{pp}}{10} \\ &= \frac{-2280,35 + 2571,05}{2416,550} \times 9,915 \\ &= 1,193 \text{ m} \end{aligned}$$

4. Perhitungan pada Cant Part

No. Ord	Luas Station	FS	Hasil	FM	Hasil
X	1,8	1	1,8	0	0
Y	0,9	4	3,6	1	3,6
A	0	1	0	2	0
		Σ_1	5,4	Σ_2	3,6

$$\begin{aligned} e &= \frac{L_{wl} - L_{pp}}{2} \\ &= \frac{101,133 - 99,15}{2} \\ &= 0,9915 \text{ m} \end{aligned}$$

5. Volume Cant Part

$$\begin{aligned} &= 1/3 \times e \times \Sigma_1 \\ &= 1/3 \times 0,9915 \times 5,4 \\ &= 1,785 \text{ m}^3 \end{aligned}$$

6. LCB Cant Part terhadap AP

$$\begin{aligned}
 &= \frac{\sum_2}{\sum_1} \times e \\
 &= \frac{3,6}{5,4} \times 0,9915 \\
 &= 0,661 \text{ m}
 \end{aligned}$$

7. Jarak LCB Cant Part terhadap O Lpp

$$\begin{aligned}
 &= 1/2 \times Lpp + \text{LCB Cant Part} \\
 &= 1/2 \times 99,15 + 0,661 \\
 &= 50,236 \text{ m}
 \end{aligned}$$

8. Volume Displacement total

$$\begin{aligned}
 &= V \text{ Displ MP} + V \text{ Displ Cp} \\
 &= 7986,698 + 1,785 \\
 &= 7988,482 \text{ m}^3
 \end{aligned}$$

9. LCB total terhadap O Lpp

$$\frac{(\text{LCB Main Part} \times \text{Vol Main Part}) + (\text{LCB Cant Part} \times \text{Vol Cant Part})}{\text{Volume Displacement}}$$

$$\begin{aligned}
 &= \frac{(1,193 \times 7986,70) + (50,236 \times 1,785)}{7988,482} \\
 &= \frac{9615,626292}{7988,482} \\
 &= 1,20 \text{ m}
 \end{aligned}$$

B.4. Koreksi Hasil Perhitungan

a. Koreksi untuk Volume Displacement

$$\begin{aligned}
 &= \frac{\text{Vol. Total} + \text{Vol Displacement Perhitungan}}{\text{Vol. Displacement Perhitungan}} \times 100 \% \\
 &= \frac{7988,48 - 7986,698}{7988,48} \times 100 \% \\
 &= 0,000223400 \times 100 \% \\
 &= 0,0223409 \% < 0,5 \% \text{ (Memenuhi)}
 \end{aligned}$$

b. Koreksi untuk prosentase penyimpangan LCB

$$= \frac{\text{LCB terhadap midship Lpp} + \text{LCB Total}}{\text{Lpp}} \times 100 \%$$

$$= \frac{1,20 - 1,303}{99,15} \times 100 \%$$

$$= 0,000997083 \times 100 \%$$

$$= 0,09970 \% < 0,1 \% \quad (\text{Memenuhi})$$



C. RENCANA BENTUK GARIS AIR

C.1. Perhitungan Besarnya Sudut Masuk (a)

Untuk menghitung besarnya sudut masuk garis air berdasarkan Coefisien Prismatic Depan (Qf). Dimana :

Pada perhitungan penentuan letak LCB, $C_p = 0,723$

Dari grafik Latsiun sudut masuk $= 18^\circ$

Penyimpangan $= 3$

Maka besarnya sudut masuk yang diperoleh $= 27^\circ$

C.2. Perhitungan Luas Bidang Garis Air

No Ord	Y = ½ B	FS	Hasil
Ap	4,300	0.25	1,075
0.25	4,900	1	4,900
0.50	5,500	0.5	2,750
0.75	5,900	1	5,900
1	6,350	0.75	4,7625
1.5	6,800	2	13,600
2	7,200	1	7,200
2.5	7,600	2	15,200
3	7,705	1.5	11,5575
4	7,705	4	30,820
5	7,705	2	15,410
6	7,705	4	30,820
7	7,650	1.5	11,475
7.5	7,500	2	15,000
8	7,000	1	7,000
8.5	5,900	2	11,800
9	4,300	0.75	3,225
9.25	3,300	1	3,300
9.5	2,500	0.5	1,250
9.75	1,300	1	1,300

FP	0,000	0.5	0
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$$\sum = 198,345$$

a. Luas garis air pada Main Part

$$\begin{aligned} Aw_{mp} &= 2 \times \frac{1}{3} \times \frac{L_{pp}}{10} \times \sum \\ &= 2 \times \frac{1}{3} \times \frac{99,15}{10} \times 198,345 \\ &= 1311,060 \end{aligned}$$

b. Rencana bentuk garis air pada Cant Part

$$\begin{aligned} AP &= X = 4,300 \\ \frac{1}{2} AP &= Y \\ e &= \frac{1}{2} \times (LWL - L_{pp}) \\ &= \frac{1}{2} \times (101,133 - 99,15) \\ &= \frac{1}{2} \times 1,983 \\ &= 0,992 \end{aligned}$$

No Ord	Tinggi Ord (Y =1/2 B)	FS	HASIL
0	0	1	0
1/2 AP	2,150	4	8,6
AP	4,300	1	4,3

$$\sum = 12,9$$

d. Luas garis air pada Cant Part (Awl Cp)

$$\begin{aligned} Awl_{Cp} &= 2 \times e \times \sum \\ &= 2 \times 0,992 \times 12,9 \\ &= 25,581 \end{aligned}$$

e. Luas total garis air (Awl Total)

$$\begin{aligned} Awl_{tot} &= \text{Luas Main Part} + \text{Luas Cant Part} \\ &= 1311,060 + 25,581 \\ &= 1336,641 \text{ m}^2 \end{aligned}$$

f. Koreksi luas garis air

$$= \frac{\text{Awl Perhitungan} - \text{Awl Total}}{\text{Awl Perhitungan}} \times 100 \%$$

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$$= \frac{1336,641 - 1336,101}{1336,641} \times 100 \%$$

$$= \frac{0,540}{1336,641} \times 100 \%$$

$$= 0,0404 \% < 0,5 \% \quad (\text{Memenuhi Syarat})$$



D. PERHITUNGAN RADIUS BILGA

Dimana :

$$B = 15,41 \text{ m}$$

$$H = 7,705 \text{ m}$$

$$T = 6,86 \text{ m}$$

$$A = \text{Rise Of Floor}$$

$$= 0,01 \times B$$

$$= 0,01 \times 15,41 = 0,1541 \text{ m}$$

$$R = \text{Jari - jari Bilga}$$

$$M = \text{Titik pusat kelelengkungan bilga}$$

D.1. Dalam Segitiga ABC

$$\text{Tg } \alpha = \frac{AB}{BC} = \frac{7,705}{0,1541}$$

$$\text{Tg } \alpha = 50$$

$$\alpha = 88,854^\circ$$

$$\beta = 180^\circ - 88,854^\circ$$

$$\beta = 91,146^\circ$$

$$\theta = 91,146 / 2$$

$$= 45,573^\circ$$

$$\angle \alpha = 0,5 \times \alpha$$

$$= 0,5 \times 88,854$$

$$= 44,427^\circ$$

D.2. Perhitungan**D.2.1. Luas Trapesium ACED**

$$= \frac{1}{2} B \times \left(\frac{B}{2} \right) \times (T+T-a) = \frac{B}{4} \times (2T-a)$$

$$= 0,5 \times 7,705 \times (2 \times 6,86 - 0,1541)$$

$$= 52,263 \text{ m}^2$$

D.2.2. Luas AFHEDA

$$= \frac{1}{2} \text{ Luas Midship}$$

$$= \frac{1}{2} \times B \times T \times C_m \quad (\text{m}^2)$$

$$= \frac{1}{2} \times 15,41 \times 6,86 \times 0,99$$

$$= 52,179 \text{ m}^2$$

D.2.3. Luas FGHC

$$\begin{aligned} &= \text{Luas trapesium ACED} - \text{Luas AFHEDA} \\ &= 52,263 - 52,179 \\ &= 0,084 \text{ m}^2 \end{aligned}$$

D.2.4. Luas FCG

$$\begin{aligned} \text{Luas juring MFG} &= a1 / 360 \times MR^2 \\ \text{Luas juring FCG} &= \text{Luas MFC} - \text{Luas juring MFG} \\ &= 0,5 R^2 \text{Tg } \alpha - (\alpha / 360) \times \pi R^2 \end{aligned}$$

Jadi Luas ACED-Luas AFHEDA=LuasMFC-Luas juring MFG

$$52,263 - 52,179 = 0,5 R^2 \text{Tg } 45,573^\circ - (45,573^\circ / 360) \times 3,14$$

R

$$0,084 = 1/2 R^2 1,02 - 0,397 R^2$$

$$0,084 = 0,51 R^2 - 0,397 R^2$$

$$R^2 = 0,743$$

$$R = 0,862 \text{ m}$$

E. MERENCANAKAN BENTUK BODY PLAN

1. Merencanakan bentuk body plan adalah
Merencanakan atau membuat bentuk garis air lengkung padapotongan ordinat
2. Langkah – langkah
 - Membuat empat persegi panjang dengan sisi $\frac{1}{2}$ B dan T
 - Pada garis air T diukurkan garis b yang besarnya = $\frac{1}{2}$ luas station dibagi T
 - Dibuat persegi panjang ABCD
 - Diukurkan pada garis air T garis air Y = $\frac{1}{2}$ lebar garis air pada station yang bersangkutan
 - Dari titik E kita merencanakan bentuk station sedemikian sehingga luas ODE = luas OAB letak titik O dari station – station harus merupakan garis lengkung yang stream line
 - Setelah bentuk station selesai dibuat, dilakukan pengecekan volume displacement dari bentuk-bentuk station
 - Kebenaran dari lengkung – lengkung dapat dicek dengan menggunakan Planimeter

E.1. Rencana Bentuk Body Plan

$$T = 6,86 \text{ m}$$

$$2 T = 13,72 \text{ m}$$

No Ord	Y = $\frac{1}{2}$ B	b = Lb / 2 T	Luas Station
Ap	4,300	0,131	1,800
0.25	4,900	0,758	10,400
0.5	5,500	1,574	21,600
0.75	5,900	2,420	33,200
1	6,350	3,265	44,800
1.5	6,800	4,810	66,000
2	7,200	6,020	82,600
2.5	7,600	6,895	94,600
3	7,705	7,391	101,400

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4	7,705	7,638	104,400
5	7,705	7,638	104,400
6	7,705	7,638	104,400
7	7,650	7,609	104,100
7.5	7,500	7,391	101,400
8	7,000	6,851	94,000
8.5	5,900	5,729	78,600
9	4,300	4,242	58,200
9.25	3,300	3,251	44,600
9.50	2,500	2,187	30,000
9.75	1,300	1,079	14,800
Fp	0	0	0

.2. Perhitungan Koreksi Volume Displacement Rencana Body Plan

No Ord	Luas Station	FS	Hasil
Ap	1,800	0.25	0,450
0.25	10,400	1	10,400
0.5	21,600	0.5	10,800
0.75	33,200	1	33,200
1	44,800	0.75	33,600
1.5	66,000	2	132,000
2	82,600	1	82,600
2.5	94,600	2	189,200
3	101,400	1.5	152,100
4	104,400	4	417,600
5	104,400	2	208,800
6	104,400	4	417,600
7	104,100	1.5	156,150
7.5	101,400	2	202,800
8	94,000	1	94,000

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8.5	78,600	2	157,200
9	58,200	0.75	43,650
9.25	44,600	1	44,600
9.50	30,000	0.5	15,000
9.75	14,800	1	14,800
Fp	0	0,25	0
		ΣA	2416,55

E.2.1. Volume Displacement Perhitungan

$$\begin{aligned} &= L_{pp} \times B \times T \times C_b \\ &= 99,15 \times 15,41 \times 6,86 \times 0,76 \\ &= 7965,867 \text{ m}^3 \end{aligned}$$

E.2.2. Volume Displacement Perencanaan

$$\begin{aligned} &= \frac{1}{3} \times (L_{pp} / 10) \times \Sigma_1 \\ &= \frac{1}{3} \times (99,15 / 10) \times 2416,55 \\ &= 7986,69775 \text{ m}^3 \end{aligned}$$

E.2.3. Koreksi penyimpangan volume displacement body plan

$$\begin{aligned} &= \frac{\text{Vol. Displ Perencanaan} + \text{Vol Displ. Perhitungan}}{\text{Vol. Displ. Perencanaan}} \times 100 \% \\ &= \frac{7986,698 - 7965,867}{7986,698} \times 100 \% \\ &= \frac{20,830}{7986,698} \times 100 \% \\ &= 0,2608 \% < 0,5 \% \quad (\text{Memenuhi Syarat}) \end{aligned}$$

F. PERHITUNGAN CHAMBER, SHEER DAN BANGUNAN ATAS

F.1. Perhitungan Chamber

$$\begin{aligned}\text{Chamber} &= 1/50 \times B \\ &= 1/50 \times 15,41 \\ &= 0,308 \\ &= 308 \text{ mm}\end{aligned}$$

F.1.1 Tinggi Bulwark = 1,0 m

F.2. Perhitungan Sheer

F.2.1. Bagian Buritan (Belakang)

$$\begin{aligned}\text{F.2.1.1. AP} &= 25 (\text{Lpp} / 3 + 10) \\ &= 25 (99,15 / 3 + 10) \\ &= 1076,25 \text{ mm}\end{aligned}$$

$$\begin{aligned}\text{F.2.1.2. } 1/6 \text{ Lpp dari AP} &= 11,1 (\text{Lpp} / 3 + 10) \\ &= 11,1 (99,15 / 3 + 10) \\ &= 477,855 \text{ mm}\end{aligned}$$

$$\begin{aligned}\text{F.2.1.3. } 1/3 \text{ Lpp dari AP} &= 2,8 (\text{Lpp} / 3 + 10) \\ &= 2,8 (99,15 / 3 + 10) \\ &= 120,54 \text{ mm}\end{aligned}$$

F.2.2. Bagian Midship (Tengan) = 0 m

F.2.3. Bagian Haluan (Depan)

$$\begin{aligned}\text{F.2.3.1. FP} &= 50 (\text{Lpp} / 3 + 10) \\ &= 50 (99,15 / 3 + 10) \\ &= 2152,5 \text{ mm}\end{aligned}$$

$$\begin{aligned}\text{F.2.3.2. } 1/6 \text{ Lpp dari FP} &= 22,2 (\text{Lpp} / 3 + 10) \\ &= 22,2 (99,15 / 3 + 10) \\ &= 955,71 \text{ mm}\end{aligned}$$

$$\begin{aligned}\text{F.2.3.3. } 1/3 \text{ Lpp dari FP} &= 5,6 (\text{Lpp} / 3 + 10) \\ &= 5,6 (99,15 / 3 + 10) \\ &= 241,08 \text{ mm}\end{aligned}$$

F.3. Bangunan Atas (Menurut Methode Varian)

F.3.1. Perhitungan Jumlah Gading

Jarak gading (a)

$$\begin{aligned} a &= L_{pp} / 500 + 0,48 \\ &= 99,15 / 150 + 0,48 \\ &= 0,678 \text{ m} \end{aligned}$$

$$\begin{aligned} \text{Jarak yang diambil} &= 0,6 \text{ m} \\ \text{Untuk } L_{pp} &= 99,15 \text{ m} \\ \text{Maka } 0,60 \times 156 \text{ gading} &= 93,6 \text{ m} \\ \text{Maka } 0,55 \times 5 \text{ gading} &= 2,75 \text{ m} \\ \text{Maka } 0,56 \times 5 \text{ gading} &= 2,8 \text{ m} \\ \hline 166 \text{ gading} &= 99,15 \text{ m} \end{aligned}$$

F.3.2. Poop Deck (Geladak Kimbul)

Panjang Poop Deck (20 % - 30 %) L_{pp}

$$\begin{aligned} \text{Panjang} &= 25 \% \times L_{pp} \\ &= 0,25 \times 99,15 \\ &= 24,7875 = 24,6 \text{ m} \end{aligned}$$

Sedang tinggi poop deck 2,0 s/d 2,4 m diambil 2,2 m dari main deck bentuk disesuaikan dengan bentuk buttock line.

Jarak gading pada poop deck

$$\begin{aligned} \text{Panjang poop deck} &= 24,6 \text{ m} \\ 0,60 \times 41 \text{ gading} &= 24,6 \text{ m} \end{aligned}$$

F.3.3. Fore Castle Deck (Deck Akil)

Panjang fore castle deck (8 % - 15 %) L_{pp}

$$\begin{aligned} \text{Panjang} &= 15 \% \times L_{pp} \\ &= 0,15 \times 99,15 \\ &= 14,873 = 14,55 \text{ m} \end{aligned}$$

Tinggi deck akil (1,9 – 2,2) diambil dari 2,2 dari main deck

Jarak gading pada fore castle dengan panjang = 11 m

$$\begin{aligned} 0,60 \times 15 \text{ gading} &= 9 \text{ m} \\ 0,53 \times 5 \text{ gading} &= 2,75 \text{ m} \\ 0,50 \times 5 \text{ gading} &= 2,8 \text{ m} \\ \hline &14,55 \text{ m} \end{aligned}$$

F.3.4. Jarak Sekat Tubrukan

$$\text{Jarak minimum} = 0,05 \times L_{pp} \times 3,05$$

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$$\begin{aligned} &= 0,05 \times 99,15 \times 3,05 \\ &= 8,0075 \text{ m} \\ \text{Jarak maximum} &= 0,08 \times L_{pp} \times 3,05 \\ &= 0,08 \times 99,15 \times 3,05 \\ &= 10,982 \text{ m} \\ \text{Jarak sekat tubrukan} &= \frac{8,0075 + 10,982}{2} \\ &= 9,49475 \text{ m} \\ &= 9,5 \text{ m} \end{aligned}$$



Menurut ketentuan perlengkapan kapal ITS halaman 53 harga

$$\text{perbandingan } h / b = 0,8 - 3$$

$$\text{Diambil } 2 \text{ sehingga } 2 = h / b \rightarrow h = 2 \times b$$

$$A = h \times b$$

$$A = 2 \times b \times b$$

$$9,500 = 2 \times b^2$$

$$b^2 = \sqrt{\frac{9,500}{2}}$$

$$= 2,18 \text{ m}$$

$$h = A / b \quad \text{Maka } b = 2,18 \text{ m}$$

$$= 9,500 / 2,18 \quad h = 4,359 \text{ m}$$

$$= 4,359 \text{ m}$$

Luas bagian yang dibalansir dianjurkan < 23 % dari luas daun kemudi

$$A' = 23 \% \times A$$

$$= 0,23 \times 9,500$$

$$= 2,1850 \text{ m}^2$$

Lebar bagian yang dibalansir pada potongan sembarang horizontal

$$b' = 23 \% \times b$$

$$= 0,23 \times 2,18$$

$$= 0,501 \text{ m}$$

Dari ukuran diatas dapat diambil ukuran daun kemudi :

$$\rightarrow \text{Luas daun kemudi (A)} = 9,500 \text{ m}^2$$

$$\rightarrow \text{Luas bagian bahan air (A')} = 2,185 \text{ m}^2$$

$$\rightarrow \text{Tinggi daun kemudi (h')} = 4,359 \text{ m}$$

$$\rightarrow \text{Lebar daun kemudi (b)} = 2,180 \text{ m}$$

$$\rightarrow \text{Lebar bagian balansir (b')} = 0,501 \text{ m}$$

G.2. Perhitungan Gaya Kemudi

G.2.1. Menurut BKI 2001 Vol II (hal 14-3 Sec B.1.1) tentang gaya kemudi adalah :

$$CR = 132 \times A \times V^2 \times k_1 \times k_2 \times k_3 \times k_t \text{ (N)}$$

Dimana :

$$A = \text{Aspek Ratio } h^2 / A$$

$$= 4,359^2 / 9,500 = 2$$

$$V = \text{Kecepatan dinas kapal} = 13,5 \text{ knot}$$

$$K1 = \frac{A + 2}{3}$$

$$= \frac{2 + 2}{3}$$

$$= 1,3333$$

$$k2 = \text{Koefisien yang tergantung dari kapal} = 1,1$$

$$k3 = 1,15 \text{ untuk kemudi dibelakang propeller}$$

$$kt = 1,0 \text{ (normal)}$$

Jadi :

$$\begin{aligned} CR &= 132 \times 9,500 \times (13,5)^2 \times 1,333 \times 1,1 \times 1,15 \times 1,0 \\ &= 385473,330 \text{ N} \end{aligned}$$



H. PERHITUNGAN SEPATU KEMUDI

Modulus penampang dari sepatu kemudi terhadap sumbu Z, menurut BKI 2001 Vol II hal 13 - 3

Dimana :

Bl = Gaya kemudi dalam resultan

BL = CR / 2

CR = Gaya Kemudi

CR = 385473,330 N

BL = 385473,330 / 2
= 192736,665 N

x = Jarak masing - masing irisan penampang yang bersangkutan terhadap sumbu kemudi

x = 0,5 x L50 (x maximum)

x = L50 (x maximum), dimana :

$$L50 = \frac{C_R}{Pr \times 10^3}$$

Dimana :

$$Pr = \frac{C_R}{L_{10} \times 10^3}; \quad L_{10} = \text{Tinggi daun kemudi } h = 4,359$$

$$= \frac{385473,330}{4,359 \times 10^3}$$
$$= 88,434 \text{ N/m}$$

$$L50 = \frac{C_R}{Pr \times 10^3}$$

$$L50 = \frac{385473,330}{88,434 \times 10^3}$$
$$= 4,359 \text{ m} \quad \text{diambil } 2,4 \text{ m (4 jarak gading)}$$

$$X \text{ min} = 0,5 \times L50$$

$$= 0,5 \times 2,4$$

$$= 1,2 \text{ m}$$

$$k = \text{Faktor bahan} = 1,0$$

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$$\begin{aligned}WZ &= \frac{BL \times X \times k}{80} \\ &= \frac{192736,665 \times 1,2 \times 1,0}{80} \\ &= 2891,050 \text{ cm}^3 \\ WY &= 1/3 \times WZ \\ &= 1/3 \times 2891,050 \\ &= 963,68 \text{ cm}^3\end{aligned}$$

Perencanaan profil sepatu kemudi dengan plat dengan ukuran sebagai berikut :

$$\begin{aligned}\text{Tinggi (h)} &= 280 \text{ mm} \\ \text{Tebal (s)} &= 50 \text{ mm} \\ \text{Lebar (b)} &= 300 \text{ mm}\end{aligned}$$

No.	b	h	F = b x h	a	F x a ²	I=1/12xbxh ³
I	30	5	150	0	0	313
II	5	18	90	12,5	14062,5	2430
III	5	18	90	0	0	2430
IV	5	18	90	12,5	14062,5	2430
V	30	5	150	0	0	313
				a= 25	Σ₂ = 28125	Σ₂ = 7915

$$\begin{aligned}I_y &= \Sigma_1 + \Sigma_2 \\ &= 28125 + 7915 \\ &= 36040 \text{ cm}^3 \\ W_{z'} &= I_y / a \\ &= 36040 / 12,5 \\ &= 2883,20 \text{ cm}^3\end{aligned}$$

$$\begin{aligned}W_{y'} &= W_{z'} / 3 \\ &= 2883,20 / 3 \\ &= 961,07\end{aligned}$$

$$\begin{aligned}W_{y'} \text{ Rencana} &< W_{y'} \text{ Perhitungan} \\ 961,07 &< 963,68 \text{ cm}^3 \quad (\text{Memenuhi})\end{aligned}$$

Koreksi hasil perhitungan

$$\begin{aligned}W_y &= \frac{W_y^1(\text{rencana}) - W_y(\text{hitungan})}{W_y(\text{hitungan})} \times 100 \% \\&= \frac{963,683 - 961,07}{961,07} \times 100 \% \\&= \frac{-2,617}{961,07} \times 100\% \\&= 0,272 \% < 0,5 \% \text{ (MEMENUHI)}\end{aligned}$$

$$\begin{aligned}W_z &= \frac{W_z^1(\text{rencana}) - W_z(\text{hitungan})}{W_z(\text{hitungan})} \times 100 \% \\&= \frac{2883,20 - 2891,050}{2891,050} \times 100 \% \\&= \frac{-7,850}{2891,050} \times 100 \% \\&= 0,272 \% < 0,5 \% \text{ (MEMENUHI)}\end{aligned}$$

I. STERN CLEARANCE

Ukuran diameter propeller ideal adalah $(0,6 - 0,7) T$, dimana T = Sarat kapal

Diambil $0,65 \times T$

$$\begin{aligned} D \text{ Propeller Ideal} & \text{ adalah} \\ & = 0,6 \times T \\ & = 0,6 \times 6,86 \\ & = 4,116 \text{ m} \end{aligned}$$

R (Jari – jari Propeller)

$$\begin{aligned} & = 0,5 \times D \text{ Propeller} \\ & = 0,5 \times 4,116 \\ & = 2,058 \text{ m} \end{aligned}$$

Diameter Boss Propeller

$$\begin{aligned} & = 1/6 \times D \\ & = 1/6 \times 4,116 \\ & = 0,686 \text{ m} \end{aligned}$$

Menurut konstruksi lambung BKI, untuk kapal baling - baling tunggal jarak minimal antara baling – baling dengan linggi buritan menurut aturan konstruksi BKI 2001 Vol II Sec 13 – 1 adalah sebagai berikut :

- a. $0,1 \times D = 0,1 \times 4,116$
 $= 0,4116 \text{ m}$
- b. $0,009 \times D = 0,09 \times 4,116$
 $= 0,37044 \text{ m}$
- c. $0,17 \times D = 0,17 \times 4,116$
 $= 0,6997 \text{ m}$
- d. $0,15 \times D = 0,15 \times 4,116$
 $= 0,6174 \text{ m}$
- e. $0,18 \times D = 0,18 \times 4,116$
 $= 0,7309 \text{ m}$
- f. $0,04 \times D = 0,04 \times 4,116$
 $= 0,1646 \text{ m}$
- g. 2 “ – 3 “ Diambil 2 “

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TUGAS AKHIR

$$\begin{aligned} \text{h. } 0,35 \quad \times \quad D &= 0,35 \times 4,116 \\ &= 1,4406 \text{ m} \end{aligned}$$

Jarak poros propeller dengan Base Line adalah

R Propeller + f + Tinggi sepatu kemudi

$$= 2,058 + 0,1646 + 0,28$$

$$= 2,503 \text{ m}$$

