

# Gas Dehydration (Dehidrasi Gas)

Teknologi Pemrosesan Gas (TKK 564)

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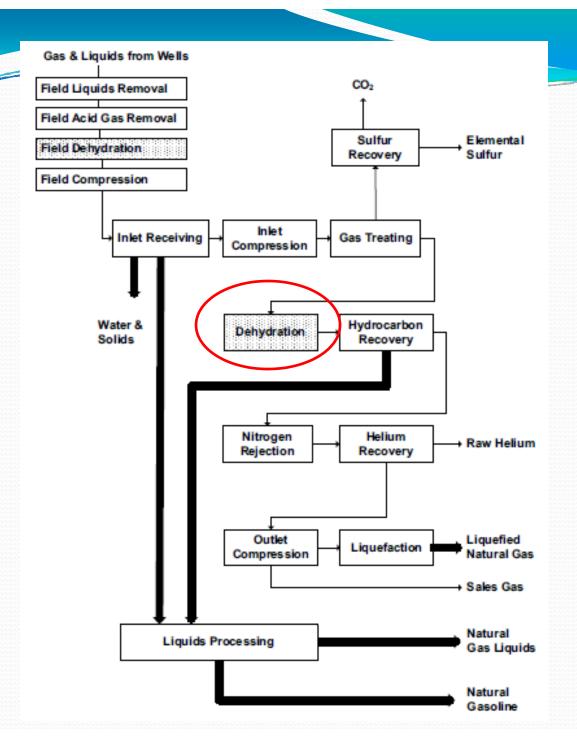
#### Instructor's Background

- BEng. (1995): Universitas Diponegoro
- Meng. (2000): Institut Teknologi Bandung
- PhD. (2006): Universiti Teknologi Malaysia
- Specialization:
  - Catalyst Design for Energy Conversion
  - Process Design for Energy Conversion
  - Combustion Engineering
  - Computational Fluid Dynamic (CFD)



#### Course Syllabus: (Part 1)

- 1. Definitions of Natural Gas, Gas Reservoir, Gas Drilling, and Gas production (*Pengertian gas alam, gas reservoir, gas drilling, dan produksi gas*)
- 2. Overview of Gas Plant Processing (Overview Sistem Pemrosesan Gas)
- 3. Gas Field Operations and Inlet Receiving (Operasi Lapangan Gas dan Penerimaan Inlet)
- 4. Gas Treating: Chemical Treatment (*Pengolahan Gas: Secara Kimia*)
- 5. Gas Treating: Physical Treatment (Pengolahan Gas: Secara Kimia)
- **6.** Gas Dehydration (*Dehidrasi Gas*)
- 7. Gas Compression System (Sistem Kompresi Gas)
- 8. Ujian Tengah Semester



#### mportance of Dehydration

#### Gas Gathering:

- to reduce pipeline corrosion
- eliminate line blockage caused by hydrate formation
- water dew point < the lowest pipeline temperature → no water formation</li>

#### Product Dehydration:

- Sales gas is usually dry if cryogenic hydrocarbon liquid recovery is used
- Liquid and gas streams may be water saturated after amine treatment or coming from underground storage
- Most product specifications, except for propane, require that no free water be present

#### Hydrocarbon Recovery:

- If acid gases are removed by use of amine processes, → the exit gas leaves water saturated
- To prevent hydrate formation in the cryogenic section of hydrocarbon recovery → water <= 0.1 ppmv</li>

# WATER CONTENT OF HYDROCARBONS

- Water content is stated in a number of ways:
  - Mass of water per volume of gas, lb/MMscf (mg/Sm3)
  - Dew point temperature, °F (°C
  - Concentration, parts per million by volume (ppmv)
  - Concentration, parts per million by mass (ppmw)
- Frst assume: ideal behavior
- In any mixture, where both the gas and liquid phases are in equilibrium → non ideal

$$x_i \gamma_i P_i^{Sat} = y_i \varphi_i P$$

- The **vapor pressure** is temperature dependent,
- the activity and fugacity coefficients are temperature, pressure, and composition dependent
- The activity and fugacity coefficients can be calculated by use of equations of state and empirical equations
- If we make the good assumption of **negligible hydrocarbon in the liquid water ph**ase, which, thus makes both  $x_i$  and  $y_i$  unity for water and assume the gas phase to be ideal, which makes  $j_i$  unity.

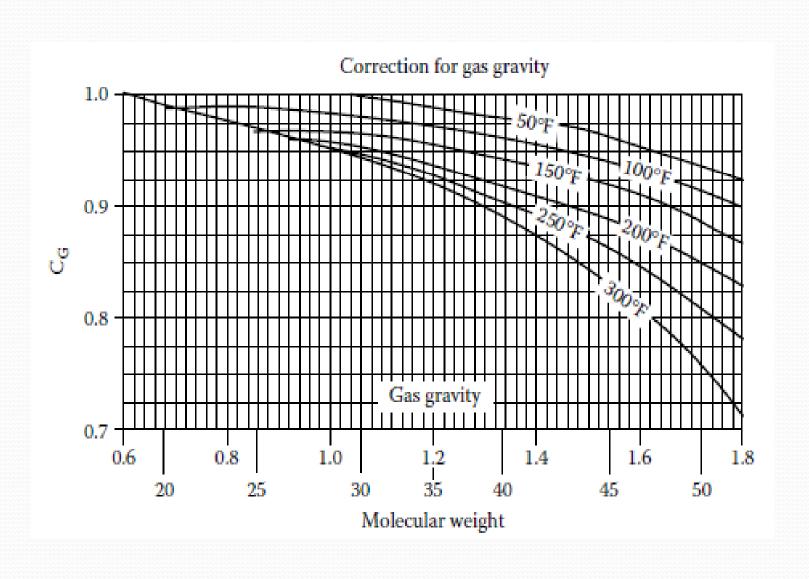
$$y_{H_2O} = \frac{P_{H_2O}^{Sat}}{P}$$

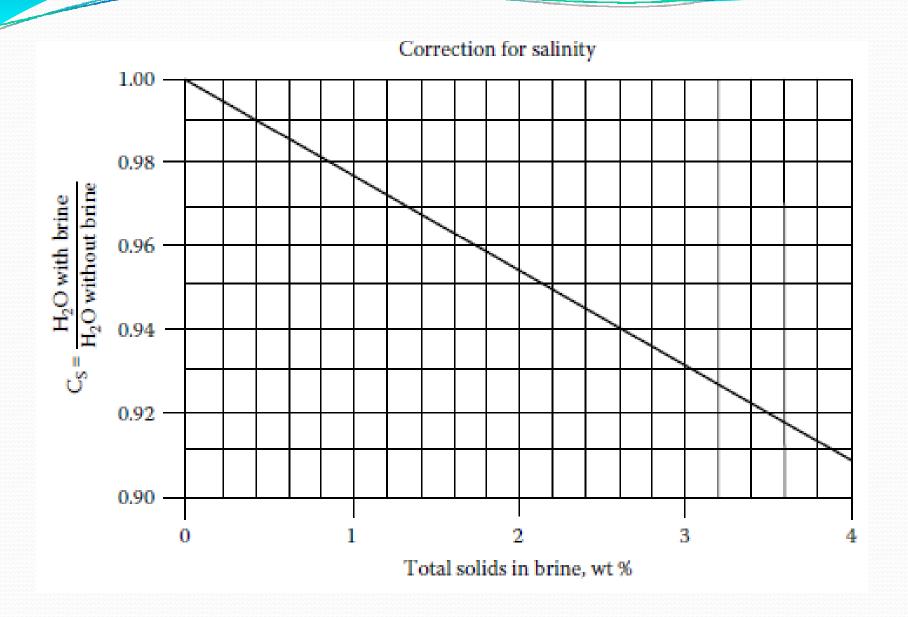
#### 60,000 40,000 20,000 20,00 10,000 8,000 8,000 6,000 4,000 2,000 2,000 1,000 Lb water/MMscf of wet gas 800 600 400 200 100 80 60 Dashed lines denote metastable region. Slope of lines is composition dependent and water content may be lower than Temperature, °F

Water content of hydrocarbon gases as a function of temperature and pressure (P<500 psia(34 bar))

$$y_{H_2O} = \frac{P_{H_2O}^{Sat}}{P}$$

## Gas gravity and salinity corrections to water content in hydrocarbon gases





#### Example 6.1

• Problem: Calculate the water content of the sweet natural gas shown in Table 6.1 at 300 psia (20.7 bar) and 80°F (26.7°C) by use of Equation 6.2 and Figure 6.1.

TABLE 6.1 Gas Composition Data for Example 6.1						
Component	Mole Fraction	Molar Mass	$\textbf{Mol Fraction} \times \textbf{Molar Mass}$			
$CH_4$	0.90	16.043	14.44			
$C_2H_6$	0.04	30.070	1.20			
$C_3H_8$	0.03	44.097	1.32			
$n-C_4H_{10}$	0.02	58.123	1.16			
$N_2$	0.01	28.013	0.28			
Totals	1.00		18.41			

• Equation 6.2 using vapor-pressure data from Appendix B gives:

$$y_{H_2O} = \frac{P_{H_2O}^{Sat}}{P} = \frac{0.507 \, psia}{300 \, psia} = 0.0017 \, \text{mol fraction}$$

convert to lb Water/MMscf:

$$W = \left(0.0017 \frac{\text{mol H}_2\text{O}}{\text{mol gas}}\right) \left(18 \frac{\text{lb H}_2\text{O}}{\text{lb-mol}}\right) \left(\frac{11\text{b-mol}}{379.5 \text{scf}}\right) (10)^6 = 81 \frac{\text{lb H}_2\text{O}}{\text{MMscf}}$$
$$= \left(1,300 \frac{\text{mg}}{\text{m}^3}\right)$$

• From Table 6.1, the MW of the gas mixture is 18.41 and the specific gravity is:

$$SpGr = \rho_{gas}/\rho_{air} = 18.41/28.96 = 0.636$$

- From Figure 6.1(a). W<sup>sa</sup>t= 85 lb/MMscf (1,400 mg/Sm<sup>3</sup>).
- Correct for specific gravity: by obtaining Cg from Figure 6.19b) (Cg = 0.99), and multiplication gives:

 $W^{Sat} = (0.99)(85) = 84 \text{ lb/MMscf} (1,400 \text{ mg/Sm}^3)$ 

#### Main Process of Gas Dehydration

- Gas Absorption → Solvent
- Gas Adsorption → Adsorbent
- Dessicant → dessicant
- Membran Separation → membran material

#### 1. ABSORPTION PROCESSES

- Water levels in natural gas can be reduced to the 10 pmmv range in a physical absorption process
- Solvent Properties used:
  - A high affinity for water and a low affinity for hydrocarbons
  - A *low volatility* at the absorption temperature to reduce vaporization losses
  - A *low viscosity* for ease of pumping and good contact between the gas and liquid phases
  - A *good thermal stability* to prevent decomposition during regeneration
  - A low potential for corrosion

#### **Absorbents Commonly Used:**

- The glycols:
  - ethylene glycol (EG),
  - diethylene glycol (DEG),
  - Triethylene glycol (TEG),
  - tetraethylene glycol (TREG)
  - and propylene glycol (PG)

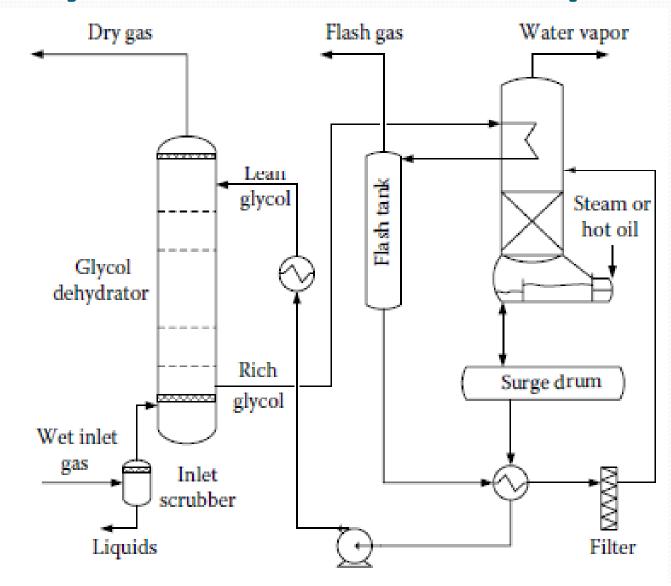
#### Glycols Used in Dehydration

TABLE 6.2 Glycols Used in Dehydration

Name	Formula		Recommended Regeneration Temperature, °F (°C) <sup>a</sup>		
Ethylene glycol (EG)	HO—(CH <sub>2</sub> ) <sub>2</sub> —OH	$C_2H_6O_2$			
Diethylene glycol (DEG)	HO—((CH <sub>2</sub> ) <sub>2</sub> —O)—(CH <sub>2</sub> ) <sub>2</sub> —OH	$C_4H_{10}O_3$	325 (160)		
Triethylene glycol (TEG)	HO—((CH <sub>2</sub> ) <sub>2</sub> —O) <sub>2</sub> —(CH <sub>2</sub> ) <sub>2</sub> — OH	$C_6H_{14}O_4$	360 (180)		
Tetraethylene glycol (TREG)	HO—((CH <sub>2</sub> ) <sub>2</sub> —O) <sub>3</sub> —(CH <sub>2</sub> ) <sub>2</sub> — OH	$C_8H_{18}O_5$	400 (200)		
Propylene glycol	HO—(CH <sub>2</sub> ) <sub>3</sub> —OH	$\mathrm{C_3H_8O_2}$			
<sup>a</sup> Source: Kohl and Nielsen (1997).					

Maximum

# Schematic of typical glycol dehydrator unit -- Absorption



#### TABLE 6.3 Typical Operating Conditions of TEG Dehydrators

Contactor

Inlet pressures <2000 psig (139 bar)

Inlet temperatures 60°F to 100°F (16°C to 38°C)

(Lower temperatures enhance absorption capacity but

can lead to hydrate formation at high pressure.)

Pressure drop 5 to 10 psi (34 to 69 kPa)

Glycol circulation rate 2 to 5 gal/lb H<sub>2</sub>O removed, with 3 common.

(17 to 42 L/kg)

Tray efficiencies 25 to 30%.

Dew points > -25°F (-32°C) (Enhanced regeneration required for lower dew

point temperatures.)

Glycol losses

Vaporization ~ 0.012 gal/MMscf (1.6 L/MM Sm<sup>3</sup>) Total 0.025 gal/MMscf (3.3 L/MM Sm<sup>3</sup>)

Regenerator

(reboiler and still)

Column internals Packed equivalent to 3 or 4 trays Reboiler temperatures 375°F to 400°F (191°C to 204°C)

Flash tank

Pressure 50 to 75 psig (446 to 618 kPa)

Temperature 150°F (66°C)

Retention times<sup>a</sup>

C4+ Lean Gas ~10 minutes.

C4+ Rich Gas<sup>a</sup> ~20 minutes (Use three-phase separator.) TEG absorbs about 1 scf

gas/gal TEG at 1,000 psig and 100°F (0.0076 Sm3/L at 70 barg

and 38°C)

<sup>a</sup> For treatment of gas streams that contain high concentrations of C4+, adequate time needs to be allowed for removal of the less-volatile components from the glycol to minimize hydrocarbon losses in the still overhead.

# Typical Operating Conditions of TEG Dehydrators

#### **Operating Conditions**

- Operating conditions for glycol units are governed principally by:
  - the degree of dehydration required,
  - the *physical properties of the glycol* solutions,
  - and the *inlet pressure of the gas* to the processing unit.

#### Other Factors That Affect Glycol Dehydrator Performance

- Oxygen reacts with the glycols to form corrosive acidic compounds.
- The products also increase the potential for foaming and glycol carryover
- A dry natural gas blanket is often put over the storage and surge tanks → to *minimize air intrusion*.
- low pH accelerates glycol decomposition
   →suggestion: addition of trace amounts of basic hydrocarbons

#### 2. ADSORPTION PROCESSES

- The two types of adsorption are:
  - physical adsorption
  - Chemisorption
- Physical adsorption: the bonding between the adsorbed species and the solid phase is called van der Waals forces, the attractive and repulsive forces that hold liquids and solids together and give them their structure.
- Chemisorption: a much stronger chemical bonding occurs between the surface and the adsorbed molecules.

- Physical adsorption is an equilibrium process like vapor-liquid equilibria and
- equations analogous to *Equation 6.1* apply.
- Thus, for a given vapor-phase concentration (partial pressure) and temperature, *an equilibrium* concentration exists on the adsorbent surface
- that is the *maximum concentration of the* condensed component (adsorbate) on the surface

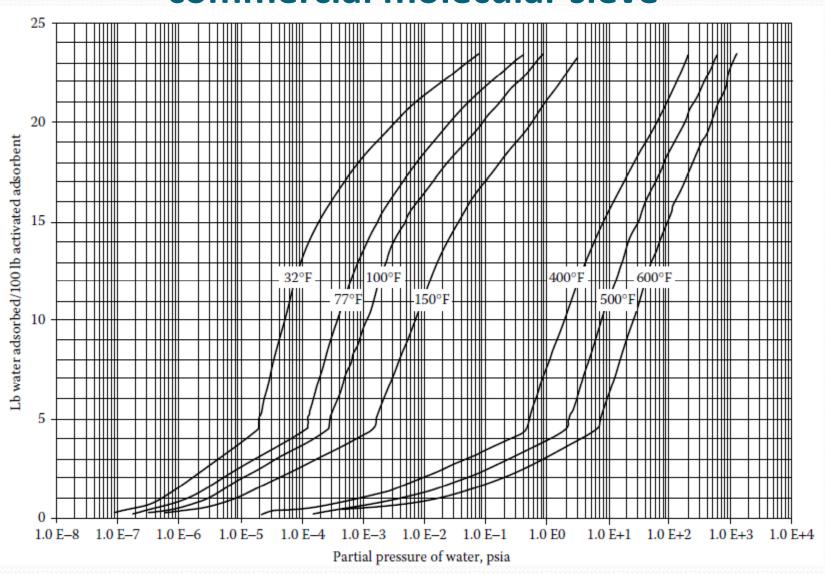
#### Physical Adsorption

- Adsorbate concentrations are usually low → only a few layers of molecules will build up on the surface.
- Thus, adsorption processes use solids with extremely high surface-to-volume ratios. (synthetic zeolites (i.e, molecular sieves) have surface-to-volume ratios: 750 cm<sup>2</sup>/cm<sup>3</sup>.
- **Molecular sieves** → the adsorbent consists of extremely fine zeolite particles held together by a binder.
- Therefore, adsorbing species travel through the macropores of the binder into the micropores of the zeolite.
- Adsorbents such as **silica gel and alumina** are formed in larger particles and require no binder.
- **Pore openings** that lead to the inside of commercial adsorbents are of molecular size (4 Å (1 Å = 10–8 cm) to 100 Å).

- Molecular sieves have an extremely narrow pore distribution, whereas silica gel and alumina have wide distributions.
- However, a molecular sieve binder (about 20% of the total adsorbent) has large pores capable of adsorbing heavier components.
- Two steps are involved in adsorbing a trace gas component:
  - The first step is to have the component contact the surface and
  - the second step is to have it travel through the pathways inside the adsorbent.
- Because this process is a two-step process and the second step is relatively slow, solid adsorbents take longer to come to equilibrium with the gas phase than in absorption processes.

- In addition to concentration (i.e., partial pressure for gases), two properties of the adsorbate dictate its concentration on the absorbent surface: *polarity* and *size*.
- Unless the **adsorbent is nonpolar**, which is not the case for those used in gas plants, polar molecules, like water, will be more strongly adsorbed than weakly polar or nonpolar compounds.
- Thus, *methane* is *displaced* by the weakly polar acid gases that are displaced by the strongly polar water

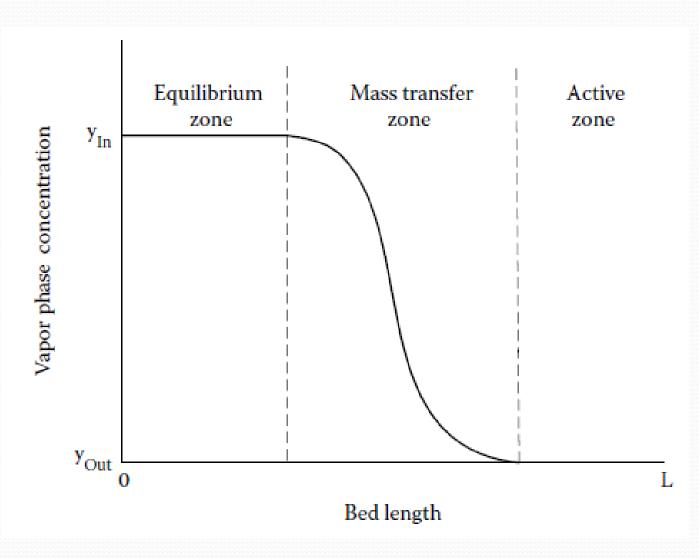
## Equilibrium Conditions for water on a commercial molecular sieve



#### **Commercial Adsorption**

- Commercial practice → adsorption is carried out in a vertical, fixed bed of adsorbent, with the feed gas flowing down through the bed.
- **\rightarrow** the formation of a *mass transfer zone (MTZ)* in the bed.
- Figure 6.7 shows the three zones in an adsorbent bed:
  - The equilibrium zone, where the adsorbate on the adsorbent is in equilibrium with the adsorbate in the inlet gas phase and no additional adsorption occurs
  - The mass transfer zone (MTZ), the volume where mass transfer and adsorption take place
  - The active zone, where no adsorption has yet taken place

## Vapor-phase concentration profile of an adsorbate in the three zones of an adsorption bed.



- In the mass transfer zone (MTZ), the concentration drops from the inlet value, y<sub>in</sub>, to the outlet value, y<sub>out</sub>, in a smooth S-shaped curve.
- If the mass transfer rate were infinite, the MTZ would have zero thickness.
- The MTZ is usually assumed to form quickly in the adsorption bed and to have a constant length as it moves through the bed, unless particle size or shape is changed.
- The value of y<sub>in</sub> is dictated by upstream processes; the y<sub>out</sub> value is determined by the regeneration gas adsorbate content.

- When used as a purification process, adsorption has two major disadvantages:
  - It is a fixed-bed process that *requires two or more adsorption beds* for continuous operation.
  - It has *limited capacity* and is usually *impractical* for removing large amounts of impurity.
- However, adsorption is very effective in the dehydration of natural gas, because water is much more strongly adsorbed than any of the alkanes, carbon dioxide, or hydrogen sulfide.
- Generally, a higher degree of dehydration can be achieved with adsorbents than with absorption processes.

### Industrial Adsorbents for Dehydration

- Three types of **commercial adsorbents** are in common use in gas processing plants:
  - Silica gel, which is made of pure SiO2
  - Activated alumina, which is made of Al<sub>2</sub>O<sub>3</sub>
  - Molecular sieves, which are made of alkali aluminosilicates and can be altered to affect adsorption characteristics

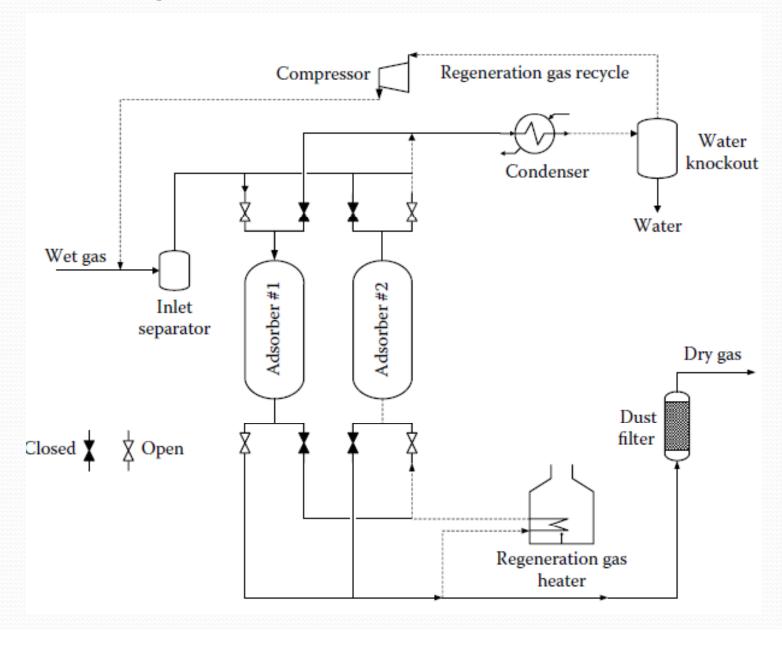
## Properties of Commercial Silica Gels, Activated Alumina, and Molecular Sieve 4A

TABLE 6.4
Representative Properties of Commercial Silica Gels, Activated Alumina, and Molecular Sieve 4A

	Silica Gel	Activated Alumina	Molecular Sieve 4A
	Silica Gei	Activated Alumina	Molecular Sieve 4A
Shape	Spherical	Spherical	Pellets (extruded cylinders) and beads
Bulk density lb/ft <sup>3</sup> (kg/m <sup>3</sup> )	49 (785)	48 (769)	40 –45 (640 – 720)
Particle size	4 – 8 mesh 5 –2 mm	7–14 mesh, 1/8-inch, 3/16-inch, 1/4-inch diameter (3-mm, 5-mm, 6-mm)	1/16-inch,1/8-inch,1/4-inch diameter cylinders (1.6-mm, 3.2-mm, 6-mm)
Packed bed % voids	35	35	35
Specific heat Btu/lb-°F (kJ/kg-K)	0.25 (1.05)	0.24 (1.00)	0.24 (1.00)
Surface area m <sup>2</sup> /g	650 - 750	325 - 360	600 - 800
Pore volume cm <sup>3</sup> /g	0.36	0.5	0.28
Regeneration temperature, °F (°C)	375 (190)	320 to 430 (160 to 220)	400 to 600 (200 to 315)
Average pore diameter (Å)	22	NA	3,4,5,10
Minimum dew point temperature of effluent, °F (°C) <sup>a</sup>	-80 (-60)	-100 (-75)	-150 (-100)
Average minimum moisture content of effluent gas, ppmv	5 –10	10 – 20	0.1

- Silica gels are used:
  - where a high concentration of water (>1 mol%) vapor is present in the feed,
  - and low levels of water in the dehydrated gas are not needed.
  - noncatalytic compounds.
- Aluminas are very polar and strongly attract water and acid gases.
  - They are used for moderate levels of water in the feed when low levels of water in the product are not required.
  - They have the highest mechanical strength of the adsorbents considered here.
- molecular sieve: for gas going into cryogenic processing
  - Of these, 4A is the most common, but the smaller pore 3A is sometimes used

#### Adsorption Process: Molecular Sieve



# Typical Operating Conditions for Molecular Sieve Dehydration Units

TABLE 6.5

Typical Operating Conditions for Molecular Sieve Dehydration Units

Feed rate 10 to 1500 MMscfd (0.3 to 42 MMSm<sup>3</sup>/d)

Superficial velocity Approximately 30 to 35 ft/min (9 to 11 m/min)

Pressure drop Approximately 5 psi (35 kPa), not to exceed 10 psi (69 kPa)

Cycle time Four to 24 hours; 8 or a multiple thereof is common

Temperatures and pressures

Adsorption

Temperatures: 50 to 115°F (10 to 45°C)

Pressures: to 1500 psig (100 barg),

Regeneration

Temperatures: 400 to 600°F (200 to 315°C)

Pressures: Adsorption pressure or lower.

#### 3. DESICCANT PROCESSES

- In some situations, such as remote gas wells, use of a consumable salt desiccant, such as CaCl2, may be economically feasible.
- The system can reduce the water content down to 20 ppmv.
- Typical salt capacities are 0.3 lb CaCl2 per lb H2O.

#### 4. MEMBRANE PROCESSES

- Membranes offer an attractive option for cases in which drying is required to meet pipeline specifications.
- Their modular nature, light weight, large turndown ratio, and low maintenance make them competitive with glycol units in some situations
- The inlet gas must be free of solids and droplets larger than 3 microns
- Inlet gas temperature should be at least 20°F (10°C) above the dew point of water to avoid condensation in the membrane.
- membranes used for natural gas dehydration are economically viable only when dehydration is combined with acid-gas removal

#### Membrane Operation

- Units operate at pressures up to 700 to 1,000 psig (50 – 70 barg) with feed gases containing 500 to 2,000 ppmv of water.
- They produce a **product gas stream of 20 to 100 ppmv** and 700 to 990 psig (48 to 68 barg).
- The low-pressure (7 to 60 psig [0.5 to 4 barg]) permeate gas volume is about 3 to 5% of the feed gas volume

### THANK YOU

